

# **Qulliq Energy Corporation**



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Qulliq Energy Corporation  
Société d'énergie Qulliq  
Qulliq Alruyaktuqtunik Ikumatjutiit

## **Application for Major Project Permits**

### **MAJOR PROJECT FOR CAMBRIDGE BAY DISTRIBUTION SYSTEM UPGRADE**

**February 2026**

## Executive Summary

Qulliq Energy Corporation (QEC) hereby applies to the Minister Responsible for Qulliq Energy Corporation pursuant to section 18.1 of the *Qulliq Energy Corporation Act*, R.S.N.W.T. 1988, c.N-2 for a major project permit to upgrade the feeder distribution system interconnecting the new power plant to the community of Cambridge Bay.

QEC is in the process of building a new power plant in Cambridge Bay with the approval of a major project permit (MPP) by the Minister responsible for QEC in August 2021 replacing the existing power plant which was constructed in 1958. The plant is expected to come in-service in 2029.

The current Cambridge Bay distribution system is fed from the existing generation plant that consists of three 1100kW and one 550kW generators with an output voltage of 4.16kV. All generators are connected to a common switchgear bus and are used to provide power to four community feeders. The switchgear is also used to provide power to other service loads. In order to improve customer power supply reliability, feeders are interconnected via a set of normally open switches. Any of these switches may be closed in the case when one of the feeder breakers is out of duty due to failure or maintenance purposes.

In the 2021 MPP application, QEC discussed that a single supply line without any alternative means of transmission would create a high risk of power interruption to the community, especially in areas with high winds and extreme cold temperatures. Accordingly, the new power plant construction scope included installation of a second line that increases reliability of the power supply and provides an alternative for electricity transmission from the plant to the community.

The proposed distribution upgrade will interconnect the new power plant to the existing community feeders via the new distribution line. The project scope has been developed with consideration of future load growth and meeting other system requirements in the community and includes the following:

- Install 4.16 kV switchgear and two 4.16/25 kV, 5 MVA, step-up transformers in the new power plant
- Construct a new substation at the North yard on the north side of Cambridge Bay comprising of one 25 kV switchgear, two 25/4.16 kV 5 MVA step-down transformers, and one 4.16KV switchgears. Existing two 25/4.16 kV 5 MVA step-down transformers from the existing power plant location shall to relocated and re-used at this new substation.
- Run two 4/0 3-phase overhead feeder lines at 25KV from the new power plant on different pole lines, interconnecting closer to town to the new substation at the North Yard on the northside of Cambridge Bay.





- Connect the existing town distribution feeders to the new power plant and substations per below:
  - Feeder 1: Will be connected to the 4.16kV switchgear in the new substation using approximately 130m of underground cables
  - Feeder 2: Will be connected to the 4.16kV switchgear in the new power plant using approximately 60m of underground cables
  - Feeder 3: Will be connected to the 4.16kV switchgear in the new substation using approximately 650m of overhead lines
  - Feeder 4: Will be connected to the 4.16kV switchgear in the new substation using approximately 1300m of overhead lines
- Perform load switching to balance loads around the feeders.

QEC's estimated cost to complete this project is \$11.6 million. This would result in an estimated 0.46 cents/kWh increase in revenue requirement by the time the project is fully in service. The project will have no impact on rates until the time of QEC's first General Rate Application following the project in-service date.

The project is anticipated to be completed by the 2029/30 fiscal year.



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## Application for Major Project Permit | Cambridge Bay Distribution System

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## 1.0 Application

Qulliq Energy Corporation (QEC) hereby applies to the Minister Responsible for Qulliq Energy Corporation pursuant to Section 18.1 of the *Qulliq Energy Corporation Act*, R.S.N.W.T. 1988, cN-2 for a major project permit to upgrade the feeder distribution system interconnecting the new power plant to the community of Cambridge Bay. QEC is requesting permission to proceed with this project. Details in support of the requested project permit are set out below.

## 2.0 Background

### 2.1 Project Background

Cambridge Bay is a hamlet located on Victoria Island in the Kitikmeot Region of Nunavut. The community had a population of 1,760 in the 2021 census. Access is mainly by air through the Cambridge Bay Airport and by sealift during the summer shipping season.

The location of the community is shown in Figure 2.1.

**Figure 2.1 – Cambridge Bay Location**



QEC is in the process of building a new power plant in Cambridge Bay, which was granted a major project permit by the Minister responsible for QEC in August 2021, replacing the existing power plant which was constructed in 1958. The plant is expected to come in-service in 2029.



The current Cambridge Bay distribution system is fed from the existing generation plant that consists of three 1100 kW and one 550 kW generators with an output voltage of 4.16kV. All generators are connected to a common switchgear bus and are used to provide power to four community feeders. The switchgear is also used to provide power to other service loads. In order to improve customer power supply reliability, feeders are interconnected via a set of normally open switches. Any of these switches may be closed in the case when one of the feeder breakers is out of duty due to failure or maintenance purposes.

In the 2021 MPP application, QEC discussed that a single supply line without any alternative means of transmission would create a high risk of power interruption to the community, especially in areas with high winds and extreme cold temperatures. Accordingly, the new power plant construction scope included installation of a second line that increases reliability of the power supply and provides an alternative for electricity transmission from the plant to the community.

In 2024, QEC engaged an independent engineering consulting company (Asher Engineering) to undertake a review of options to interconnect the new power plant to the existing community feeders via the new distribution line.

### 3.0 Assessment of Project Options

In accordance with QEC's request, the consultant performed technical analysis of various tie-in options of the new power plant to the existing community feeders, including:

- **Option 1:** Run two 5 kV feeder circuit lines from the new power plant to the existing distribution system. Tie in to the nearest feeder point and reduce the four feeders to two feeders within the existing distribution system.
- **Option 2:** The four existing community feeders are connected to the new power plant via new 5 kV transmission lines, which includes changing all the single-phase power lines between Feeder 2 poles to be three-phase.
- **Option 3:** Run two 25 kV feeder circuit lines from the new power plant (with two 5 MVA step-up transformers) to the existing distribution system (with two 5 MVA step-down transformers).
- **Option 4:** Run two 25 kV feeder circuit lines from the new power plant (with two 5 MVA step-up transformers) to the North Yard location (with two 5 MVA step-down transformers and 5 kV switchgear).
- **Option 5:** Upgrade all customers' transformers to have 25 kV primary voltage.

Since the new power plant is located in a considerably remote location that is far from the existing power plant location, the analysis of options focused on optimizing the following criteria:



- Minimizing the voltage drop across the lines. The voltage drop should not exceed 3% from the generators to each individual consumer.
- Minimizing the network active power losses.

Network model and simulation parameters were set based on the following inputs:

- **Electrical Transient Analyzer Program (ETAP) Model:** The ETAP model used was based on the model developed by Asher Engineering for the QEC Penetration Study. The model of the power plant was updated to reflect the topology of the new plant.
- **One-line Diagrams:** The network model was built using the one-line diagrams provided by QEC, which were also used to obtain the connected load and phase connection of each customer.
- **Generation Forecast:** Generation estimates for 2026-2066 period were used for feeder sizing, voltage drop, and network losses calculations.

The study used generation forecast for the years from 2026 to 2066 to calculate the demand load and demand factor for each feeder. These demand factors were applied to calculate the minimum feeder size that is required to achieve a maximum voltage drop of 3% at the customer transformer under each option.

The initial study by Asher Engineering, included in Appendix A, concluded that the option 4 preferred by QEC as presented did not accommodate the load forecast up to the year 2066, and that the off-line tap changers of both step up and step down transformers needed to be adjusted to mitigate the voltage drop due to future load increase.

Upon reviewing the initial study by Asher Engineering, QEC requested the consultant to investigate the feasibility to implement an alternative approach for voltage drop mitigation. The alternative approach involves the use of Automatic Voltage Regulators (AVRs) that are strategically placed at different parts of the network in order to maintain the voltage drop within the  $\pm 3\%$  voltage limits while keeping the network losses at a minimum. In addition, alternatives for tie-in of Feeder 2 were considered. The alternative approach study is included in Appendix B.

The proposed distribution upgrade project will interconnect the new power plant to the existing community feeders via the new distribution line. The project scope has been developed with consideration of future load growth and meeting other system requirements in the community and includes the following:

- Install 4.16 kV switchgear and two 4.16/25 kV, 5 MVA, step-up transformers in the new power plant
- Construct a new substation at the North yard on the north side of Cambridge Bay comprising of one 25 kV switchgear, two 25/4.16 kV 5 MVA step-down transformers, and one 4.16KV switchgears. Existing two 25/4.16 kV 5 MVA step-down



transformers from the existing power plant location shall to relocated and re-used at this new substation.

- Run two 4/0 3-phase overhead feeder lines at 25KV from the new power plant on different pole lines, interconnecting closer to town to the new substation at the North Yard on the northside of Cambridge Bay.
- Connect the existing town distribution feeders to the new power plant and substations per below:
  - Feeder 1: Will be connected to the 4.16kV switchgear in the new substation using approximately 130m of underground cables
  - Feeder 2: Will be connected to the 4.16kV switchgear in the new power plant using approximately 60m of underground cables
  - Feeder 3: Will be connected to the 4.16kV switchgear in the new substation using approximately 650m of overhead lines
  - Feeder 4: Will be connected to the 4.16kV switchgear in the new substation using approximately 1300m of overhead lines
- Perform load switching to balance loads around the feeders.

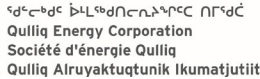
The estimated cost to complete this project is \$11.567 million. The project is anticipated to be completed by the 2029/30 fiscal year.

## 4.0 Impact of the Project on Ratepayers

QEC conducted an analysis of the impact of the project on ratepayers. It should be noted that the project will have no impact on rates until the time of QEC's General Rate Application following the project coming in-service. QEC conducted the rate impact analysis based on a territorial rate design assuming the project is completed by the 2029/30 fiscal year.

The rate impact analysis is based on QEC's estimated cost for this project of \$11.567 million.

Table 4.1 summarizes the estimated incremental revenue requirement increase due to the project of \$11.567 million. The estimated rate increase under territory-wide rates is 0.46 cents/kWh.



2	Average Territorial Rate Increase (c/kWh)	0.46
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3 It is important to note that this analysis has been provided for illustrative purposes only.  
4 Actual rate impacts will depend on the overall revenue requirements and rate designs  
5 approved in subsequent General Rate Applications.

## 6 5.0 Grounds in Support of the Application

7 The implementation of the proposed project is very important to QEC's customers. The  
8 project will provide a stable, cost effective, safe, and reliable service to the community of  
9 Cambridge Bay and support the new power plant operation.

0 Power is an essential service in Nunavut, and QEC must plan to be able to deliver reliable  
1 electricity.

## 2 6.0 Project Timelines

3 Based on QEC's experience with procurement, delivery of materials and construction  
4 windows, this project is anticipated to be completed by the 2029/30 fiscal year.



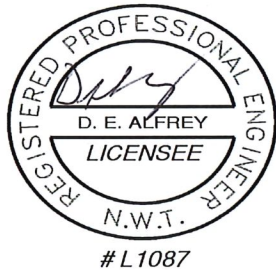


## Engineering Study Final Report

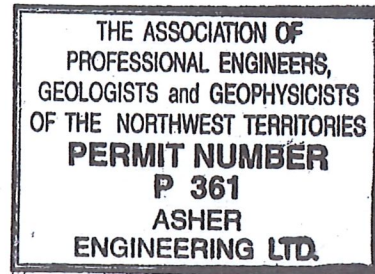
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## Revision History

Rev No.	Date	Description	Asher Engineering Ltd.			Qulliq Energy Corporation
			Created By (Initials)	Checked by (Initials)	Approval (Name and Signature)	Received by (Name and Signature)
C	Nov. 8/24	Issued for Use	AA	SW	Dwight Alfrey P.Eng.	
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					<i>Brent Taylor</i>	



November 8, 2024



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While it is believed that the information contained herein is reliable under the conditions and subject to the limitations set forth in the Document, this Document is based on information not within the control of Asher, nor has said information been verified by Asher, and Asher therefore cannot and does not guarantee its sufficiency and accuracy. The comments in the Document reflect Asher's best judgment in light of the information available to it at the time of preparation.

The results presented in the report are at a conceptual level; no detailed engineering has yet been performed, nor has equipment been selected or an operational plan been defined.

Use of this Document acknowledges acceptance of the foregoing conditions.

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Appendix 2	Cambridge Bay – Estimated Electricity Production

## **Executive Summary**

Qulliq Energy Corporation (QEC) currently delivers electricity to approximately 15,000 customers in 25 communities across Nunavut using 25 standalone diesel power plants with total installed capacity of 76MW. Each community has its own independent generation and distribution system that does not have any backup from the utility grid.

QEC is planning to de-commission the existing Cambridge Bay Community power plant and build a new power plant on the south-west side of the community to provide sufficient energy to this community. Due to the remote location of the new power plant, different approaches for connecting the existing community feeders to the new power plant need to be studied.

QEC proposes five (5) options to tie-in the new power plant to the existing community feeders. Additionally, Asher has proposed rearrangements for some of these options to improve the voltage drop. These options are summarized as below:

**Option 1** involves the following:

- Feeders 1 and 4 and Feeders 2 and 3 are combined into two (2) feeders.
- Two (2) new 5kV power lines are installed from the new power plant to these two feeders to tie in at the nearest locations for Feeders 1 and 2.

**Option 2** involves the following:

- The four existing community feeders are connected to the new power plant using new 5kV power lines to tie in at the nearest location for each feeder.

**Option 3** involves the following:

- Two (2) 4.16/25kV, 5MVA, step-up transformers are installed at the new power plant and connected via cables to the new generator distribution switchgear.
- Two (2) 25/4.16kV, 5MVA, step-down transformers with Main-Tie-Main, 5kV, switchgear are installed at the existing power plant and connected to the step-up transformers via two (2) 25kV power lines.
- The 5kV switchgear at the existing power plant is connected via four (4) new 5kV power lines to tie in at the nearest locations to the existing community feeders such that two feeders are connected to each switchgear section.

**Option 3A**, proposed by Asher, is similar to QEC Option 3 except that feeders are redistributed with one feeder connected to one switchgear section, while the other three feeders are connected to the other switchgear section.

**Option 3B**, proposed by Asher, is an alternative approach for using Option 3 where Feeder 2 is connected directly to the new switchgear in the new power plant.

**Option 4** involves the following:

- Two (2) 4.16/25kV, 5MVA, step-up transformers are installed at the new power plant and connected via cables to the new generator distribution switchgear.

- Two (2) 25/4.16kV, 5MVA, step-down transformers with Main-Tie-Main, 5kV, switchgear are installed at the North Yard and connected to the step-up transformers via two (2) 25kV power lines.
- The 5kV switchgear at the North Yard is connected via four (4) new 5kV power lines to tie in at the nearest locations the existing community feeders.

**Option 5** involves the following:

- Two (2) 4.16/25kV, 5MVA, step-up transformers are installed at the new power plant and connected via cables to the new generator distribution switchgear.
- Upgrade all existing community transformers to have 25kV primary voltage.
- Feeders 1 and 3 and Feeders 2 and 4 are combined into two (2) feeders and connected to the step-up transformers, via an intermediate Main-Tie-Main switchgear, at the nearest location.

The above options are discussed in detail in Section 1.3. The single-line diagrams showing the network topology for each option are included in Appendices 1.A to 1.G.

The scope of the study is to calculate the maximum voltage drop and network active power losses for each community feeder, considering each of the tie-in options and provide the option that will offer the minimum voltage drop and network losses. Additionally, the study will recommend the minimum feeders sizes required to tie-in the new power plant to the existing feeders under each option in order to achieve a maximum voltage drop of 3%.

The study considers the estimated electricity production for the years from 2026 to 2066 as shown in Appendix 2.

Recommendations provided by this study consider technical aspects only. Construction cost estimates associated with each option are presented in a separate report.

Table 3 summarizes the study results.

**Table 3: Study Results Summary**

Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
		Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
1		Failed							
2		Failed							
3	A	Failed							
	B	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
3A	A	Failed							
	B	1/0 AWG	3/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
3B	A	2/0 AWG	1/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	B	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
4	A	Failed							
	B	Failed							
5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-5%	N/A	
	B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	

Scenario A: All feeders are fed from one step-up transformer

Scenario B: Feeders are distributed across both step-up transformers

## **1. Introduction**

### **1.1 Background**

Qulliq Energy Corporation (QEC) currently delivers electricity to approximately 15,000 customers in 25 communities across Nunavut using 25 standalone diesel power plants with total installed capacity of 76MW. Each community has its own independent generation and distribution system that does not have any backup from the utility grid.

QEC is planning to de-commission the existing Cambridge Bay Community power plant and build a new power plant on the south-west side of the community to provide sufficient energy to this community. Due to the remote location of the new power plant, different approaches for connecting the existing community feeders to the new power plant need to be studied.

### **1.2 Scope of Work**

The estimated electricity production for the years from 2026 to 2066, shown in Appendix 2, is used to calculate the maximum voltage drop and network active power losses for each community feeder, when each of the tie-in options is utilized and provide the option that will offer the minimum voltage drop and network losses. Additionally, the study will recommend the minimum feeders sizes required to tie-in the new power plant to the existing feeders under each option in order to achieve a maximum voltage drop of 3%.

### **1.3 Tie-In Options**

In order to connect the new power plant to the existing community feeders, QEC proposed five (5) options to be considered. Additionally, upon further study of the load behavior when connected to the network, Asher proposed two alternative implementations of Option 3. The different options are detailed below.

#### **1.3.1 Option 1**

Run two (2) x 5kV feeder circuit lines from the new power plant to the existing distribution system. Tie in to the nearest feeder point and reduce the four (4) feeders to two (2) feeders within the existing distribution system.

- Feeders 1 and 4 are combined into one feeder by connecting the lines at Poles 50101001 in Feeder 1 and 50104002 in Feeder 4.
- Feeders 2 and 3 are combined into one feeder by connecting the lines at Pole 50102008.
- Connect the new combined feeders to the main 4.16kV switchgear at the new power plant using a new 5kV transmission line.

The nearest tie-in location is at Pole 50104003 in Feeder 4 and Pole 50102268 in Feeder 2. This will require changing all the single-phase power lines between Poles 50102268 and 50102135 to be three-phase.

#### **1.3.2 Option 2**

The four (4) existing community feeders are connected to the new power plant via new 5kV transmission lines. The tie-in location for each feeder is as below:

- For Feeder 1: Pole 50101001.
- For Feeder 2: Pole 50102268. This will require changing all the single-phase power lines between Poles 50102268 and 50102135 to be three-phase.
- For Feeder 3: Pole 50103001.
- For Feeder 4: Pole 50104003.

### 1.3.3 Option 3

Run two (2) x 25kV feeder circuit lines from the new power plant (with two (2) x 5MVA step-up transformers) to the existing distribution system (with two (2) x 5MVA step-down transformers).

- Install two (2) new 4.16/25kV, 5MVA, step-up transformers in the new power plant and connect the primary side of these transformers to the new main 5kV switchgear via cables.
- Install two (2) new 25/4.16kV, 5MVA, step-down transformers and Main-Tie-Main, 5kV, switchgear at the existing power plant and connect the primary side of these transformers to the outgoing breaker of the new switchgear.
- Connect the incoming breakers of the new switchgear to the secondary side of the new step-up transformers via new transmission lines.
- Connect the existing community feeders to the existing 5kV switchgear at the existing power plant using new 5kV transmission lines. The nearest tie-in location for each feeder is as below:
  - For Feeder 1: Pole 50101001
  - For Feeder 2: Pole 50102001
  - For Feeder 3: Pole 50103001
  - For Feeder 4: Pole 50104001

For this option, two operating scenarios are considered:

- All community feeders are fed from one step-up transformer. This is considered the worst-case operating scenario.
- Each two of the community feeders are fed from one step-up transformer. The distribution of the community feeders on each transformer was decided based on the peak demand load of the four feeders such that both transformers are equally loaded.

### 1.3.4 Option 3A

The study of the voltage drop using Option 3 showed that Feeder 1 experiences the highest voltage drop among the other feeders. Therefore, this option suggests rearranging the feeders so that Feeder 1 is connected alone to one step-down transformer, while the other three feeders are connected to the other step-down transformer.

### 1.3.5 Option 3B

The study of the voltage drop using various options showed that Feeder 2 has the least voltage drop among other feeders and it can be connected directly to the 5kV switchgear without violating



the voltage drop limits.

In this option, Feeder 2 is connected directly to the new switchgear in the new power plant in order to reduce the load on the transformers.

#### **1.3.6 Option 4**

Run two (2) x 25kV feeder circuit lines from the new power plant (with two (2) x 5MVA step-up transformers) to the North Yard location (with two (2) x 5MVA step-down transformers and 5kV switchgear).

- Install two (2) new 4.16/25kV, 5MVA, step-up transformers in the new power plant and connect the primary side of these transformers to the new main 5kV switchgear via cables.
- Install two (2) new 25/4.16kV, 5MVA, step-down transformers and Main-Tie-Main, 5kV, switchgear at the North Yard and connect the primary side of these transformers to the outgoing breaker of the new switchgear.
- Connect the incoming breakers of the new switchgear to the secondary side of the new step-up transformers via new transmission lines.
- Connect the existing community feeders to the 5kV switchgear at the North Yard via transmission lines. The tie-in location of each feeder is as below:
  - For Feeder 1: Pole 50101135
  - For Feeder 2: Pole 50102251
  - For Feeder 3: Pole 50103013
  - For Feeder 4: Pole 50104003

For this option, two operating scenarios are considered:

- All community feeders are fed from one step-up transformer. This is considered the worst-case operating scenario.
- Each two of the community feeders are fed from one step-up transformer. The distribution of the community feeders on each transformer was decided based on the peak demand load of the four feeders such that both transformers are equally loaded.

#### **1.3.7 Option 5**

Upgrade all customers' transformers to have 25kV primary voltage.

- Install two (2) new 4.16/25kV, 5MVA, step-up transformers in the new power plant and connect the primary side of these transformers to the new main 5kV switchgear via cables.
- Feeders 1 and 3 are combined into one feeder by connecting the lines at Poles 50101001 in Feeder 1 and 50103001 in Feeder 3.
- The combined feeders are connected to one step-up transformer at Pole 50101001 in Feeder 1.

- Feeders 2 and 4 are combined into one feeder by connecting the lines at Pole 50102003 in Feeder 2 and 50104003 in Feeder 4.
- The combined feeders are connected to the other step-up transformer at Pole 50102268 in Feeder 2.

The single-line diagrams showing the network topology for each option are included under Appendices 1.A to 1.G.

## **2. Discussion**

Since the new power plant is located in a considerably remote location that is far from the existing power plant location, it became crucial to find a proper solution for the connection of the existing community feeders to the new power plant. The recommended solution optimizes the following criteria:

- Minimizing the voltage drop across the lines. The voltage drop should not exceed 3% from the generators to each individual consumer.
- Minimizing the network active power losses.

This study evaluates the five (5) options proposed by QEC and the adjustments made by Asher to determine the most technically feasible option and the provides recommendations for further aspects to be considered.

### **2.1 Sources of Data**

Network model and simulation parameters are set based on the following inputs:

- **ETAP Model:**  
The ETAP model used is based on the model developed for QEC Penetration Study. The model of the power plant is updated to reflect the topology of the new plant.
- **One-line Diagrams:**  
The Network model is built using the provided one-line diagrams. These diagrams are also used to obtain the connected load and phase connection of each customer.
- **Generation Forecast:**  
QEC provided a table showing the estimated electricity produced over the years from 2026 to 2066 (See Appendix 2). These estimates are used for feeder sizing, voltage drop, and network losses calculations.

### **2.2 Assumptions**

- The maximum demand factors of each feeder load in 2019 are calculated based on the load data reading provided by QEC. The estimated electricity production for subsequent years (Appendix 2) is used to calculate the maximum demand factor for these years.

- Normally open switches, interconnecting different feeders and used during the failure or maintenance of any of the feeder breakers, are not included in the model and the penetration study except for the options where each two feeders are combined.
- Since the specified AASC cables are not available in the standard ETAP library, AAC cables are used instead. The electrical and geometric characteristics of the selected cable are modified to match the AASC cable specifications provided by QEC.
- The new power plant main switchgear tie breaker is assumed to be open.
- The boundary conditions for the voltage limits at all networks nodes (buses) are assumed to be  $\pm 3\%$ .
- The maximum transmission line size to be used is 4/0 AWG with a single conductor per phase.
- QEC advised that most of the loads are non-inductive and that the overall power factor for each feeder is in the order of 0.99. For the purpose of this study, all loads are assumed to have a 0.95 power factor for more conservative values of load currents.
- Based on overhead line conductor parameters provided by QEC, resistance, reactance, and susceptance values for overhead lines are calculated using ETAP considering the following conductor configuration on the pole structure:
  - Conductor height: 34 ft (unless otherwise indicated on the single-line diagrams).
  - Spacing between phases: 2 ft.
- Generator plant service loads are not considered in the analysis.

## 2.3 Network Configuration

The new power plant for Cambridge Bay consists of two (2) 1500kW, two (2) 1100kW and one (1) 850kW generators with an output voltage of 4.16kV. Generator outputs are connected to a main 4.16kV switchgear with two (2) bus sections connected together via tie breaker such that one (1) 1500kW and one (1) 1100kW generators are connected to one bus section, and the one (1) 1500kW, one (1) 1100kW, and one (1) 850kW generators are connected to the other bus section.

Existing community feeders are connected to the two bus sections of the main switchgear. The connection scheme depends on the tie-in option to be studied.

In order to improve customer power supply reliability, feeders are interconnected via a set of normally open switches. Any of these switches may be closed in the case when one of the feeder breakers is out of duty due to failure or for maintenance purposes. Since the case where both feeders are connected to one feeder breaker does not represent normal network operation and is used only for maintenance purposes, these configurations are not included in the model except where two feeders are combined into one feeder. For this case, only the tie switch is considered closed.

The network ETAP model for each study option is provided in Appendices 1.A to 1.G.

## 2.4 Calculation Procedures

### 2.4.1 Load Parameters Calculations

The peak demand load for the year 2019 is obtained from the metering readings provided by QEC for this year and is used to calculate the maximum demand factor for the loads of each feeder as shown in Table 1.

**Table 1: Maximum Demand (2019)**

	Connected Load (kVA)	Max. Demand Load (kVA)	Max. Demand Factor (%)
Feeder 1	2537.5	989.625	39.00%
Feeder 2	3017.5	754.375	25.00%
Feeder 3	642.5	334.1	52.00%
Feeder 4	450	234	52.00%
<b>Total</b>	6647.5	2312.1	

The estimated electricity production (Appendix 2) is used to calculate the percentage growth of electricity demand which is, in turn, used to calculate the maximum demand for the successive years as shown in Table 2.

**Table 2: Estimated Growth in Demand Load**

Year	Population Demand Load Change (%)	Maximum Demand Factors			
		Feeder 1	Feeder 2	Feeder 3	Feeder 4
2019	-	39.00%	25.00%	52.00%	52.00%
2026	55.00%	60.45%	38.75%	80.60%	80.60%
2027	57.00%	61.23%	39.25%	81.64%	81.64%
2028	58.00%	61.62%	39.50%	82.16%	82.16%
2029	59.00%	62.01%	39.75%	82.68%	82.68%
2030	61.00%	62.79%	40.25%	83.72%	83.72%
2031	62.00%	63.18%	40.50%	84.24%	84.24%
2032	64.00%	63.96%	41.00%	85.28%	85.28%
2033	65.00%	64.35%	41.25%	85.80%	85.80%
2034	66.00%	64.74%	41.50%	86.32%	86.32%
2035	68.00%	65.52%	42.00%	87.36%	87.36%
2036	70.00%	66.30%	42.50%	88.40%	88.40%
2041	78.00%	69.42%	44.50%	92.56%	92.56%

Year	Population Demand Load Change (%)	Maximum Demand Factors			
		Feeder 1	Feeder 2	Feeder 3	Feeder 4
2046	87.00%	72.93%	46.75%	97.24%	97.24%
2051	98.00%	77.22%	49.50%	102.96%	102.96%
2056	110.00%	81.90%	52.50%	109.20%	109.20%
2061	123.00%	86.97%	55.75%	115.96%	115.96%
2066	138.00%	92.82%	59.50%	123.76%	123.76%

As agreed with QEC, the study considers the load demand of the first 10 years (2026 to 2036) in one-year steps, and the following 30 years (2037 to 2066) in 5-year steps.

The above demand factors are used in the ETAP model.

The maximum demand load analysis of the four feeders based on the table above shows that:

- The balanced connection of feeders for the options where two feeders are supposed to be connected, is to connect Feeders 1 and 4 together and Feeders 2 and 3 together.
- The maximum generation capacity for each bus section of the switchgear is 2500 kW. The peak demand load forecast for all the years exceeds 2500kW. Therefore, the switchgear bus-tie breaker needs to be closed such that the total load can be distributed among all the generators.
- Customer transformers connected to Feeders 3 and 4 need to be upgraded to 125% of their current ratings to accommodate the forecasted demand.

## 2.4.2 Design Constraints

The following design constraint are established by QEC:

- The total voltage drop from the generators to each customer load shall not exceed 3%.
- The maximum size of a transmission line is 4/0AWG with no more than one conductor per phase.
- Initial calculations are made with all transformer taps set at the zero-position. However, transformer tap settings can be changed to compensate for excessive voltage drop when needed.

## 2.5 Results

Electricity production estimate for the years from 2026 to 2066 is used to calculate the demand load and demand factor for each feeder. These demand factors were applied to calculate the minimum feeder size that is required to achieve a maximum voltage drop of 3% at the customer transformer using the different options detailed under Section 1.3.

The study concludes that:

- Options 1 and 2 do not satisfy the 3% voltage drop criteria due to the distance between the new power plant and the tie-ins of Feeders 1, 3, and 4. Therefore, these options cannot be utilized.
- Comparing the results of Options 3 and 4, it can be shown that Option 3 provides better results than Option 4 since the North Yard is farther away from the nearest tie-in to the community feeders than the existing power plant.

Both Options 3 and 4 fail to satisfy the 3% voltage drop criteria when all the feeders are fed from one step-up transformer.

- The alternatives proposed for Option 3 provide better results in terms of voltage drop and active power losses. However, unlike Option 3A, Option 3B allows all feeders to be fed from one step-up transformer without violating the voltage drop criteria.

The study, also, concludes that Option 5 is the recommended option since it involves less voltage drop and active power losses along the power lines as shown by Table 4 below.

**Table 3: Study Results Summary**

Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
		Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
1		Failed							
2		Failed							
3	A	Failed							
	B	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
3A	A	Failed							
	B	1/0 AWG	3/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
3B	A	2/0 AWG	1/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	B	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
4	A	Failed							
	B	Failed							
5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-5%	N/A	
	B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	

Scenario A: All feeders are fed from one step-up transformer

Scenario B: Feeders are distributed across both step-up transformers

**Table 4: Study Results Details**

Year	Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2026	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	2/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	
2027	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	3/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	



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			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2028	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	3/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	
2029	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	3/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

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			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2030	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	3/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	4/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	2/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	
2031	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	2/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

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			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2032	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	2/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	
2033	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	2/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

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			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2034	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	3/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	
2035	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	3/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

Engineering Study – Final Report  
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Year	Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2036	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	3/0 AWG	3/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	
2041	1		Failed	2/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

Year	Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2046	1		Failed	2/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	Failed	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	Failed	Failed	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	
2051	1		Failed	3/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	Failed	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	Failed	Failed	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	

Year	Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2056	1		Failed	3/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3A	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	4	A	Failed	1/0 AWG	Failed	Failed	4/0 AWG	Failed	Failed	
		B	Failed	1/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	Failed	Failed	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
2061	1		Failed	4/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3A	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	4	A	Failed	1/0 AWG	Failed	Failed	4/0 AWG	Failed	Failed	
		B	Failed	1/0 AWG	3/0 AWG	4/0 AWG	4/0 AWG	Failed	Failed	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	

Year	Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2066	1		Failed	4/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3A	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3B	A	2/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	4	A	Failed	1/0 AWG	Failed	Failed	4/0 AWG	Failed	Failed	
		B	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	

Scenario A: All feeders are fed from one step-up transformer

Scenario B: Feeders are distributed across both step-up transformers



### **3. Conclusion and Recommendations**

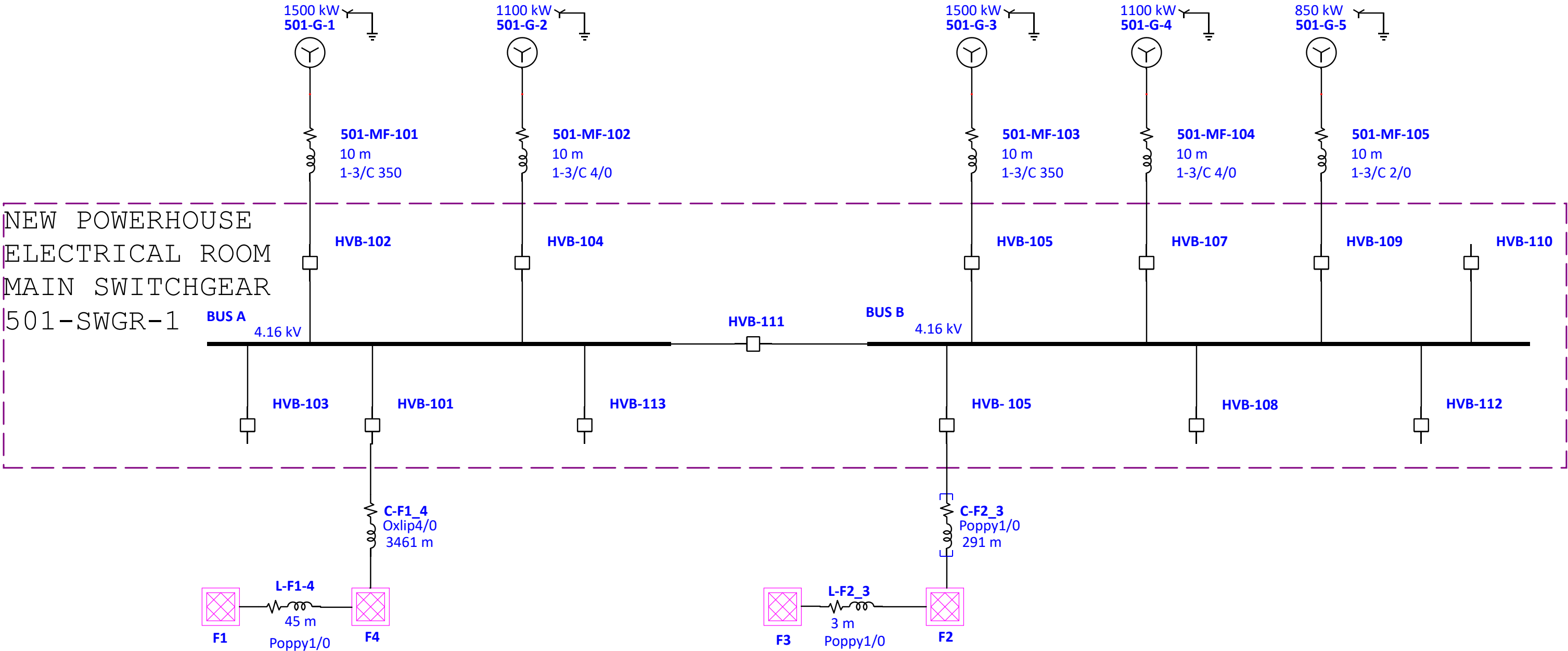
The utilization of Options 1 and 2 was found to be not feasible due to the distance between the new power plant and the tie-in locations of the community feeders particularly for Feeders 1, 3, and 4.

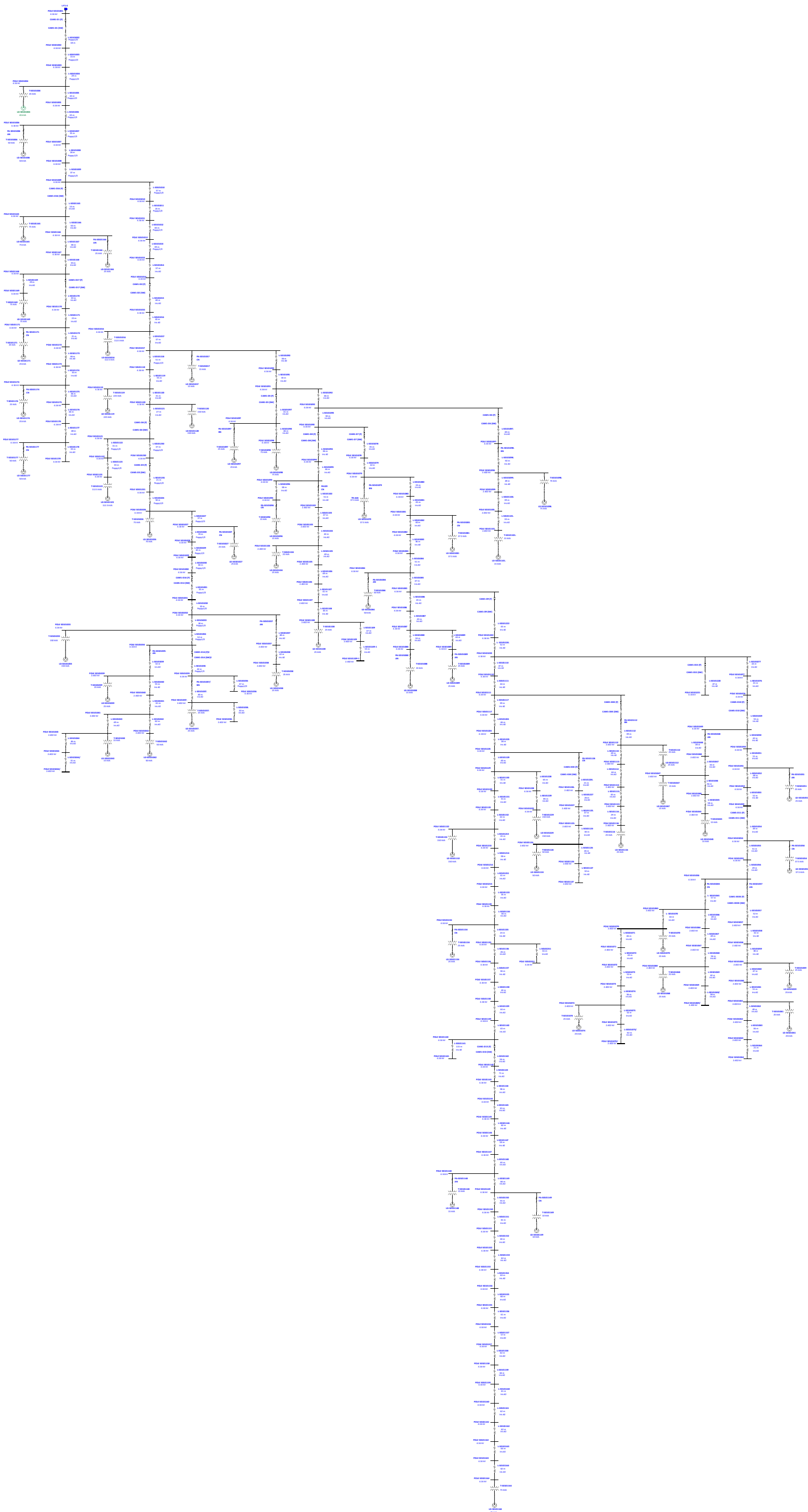
Options 3, 3A, and 4 can be utilized with the exception that all feeders cannot be fed from one step-up transformer. However, Option 3B allows the two scenarios where feeders can either be fed from one transformer or their loads is distributed on both step-up transformers.

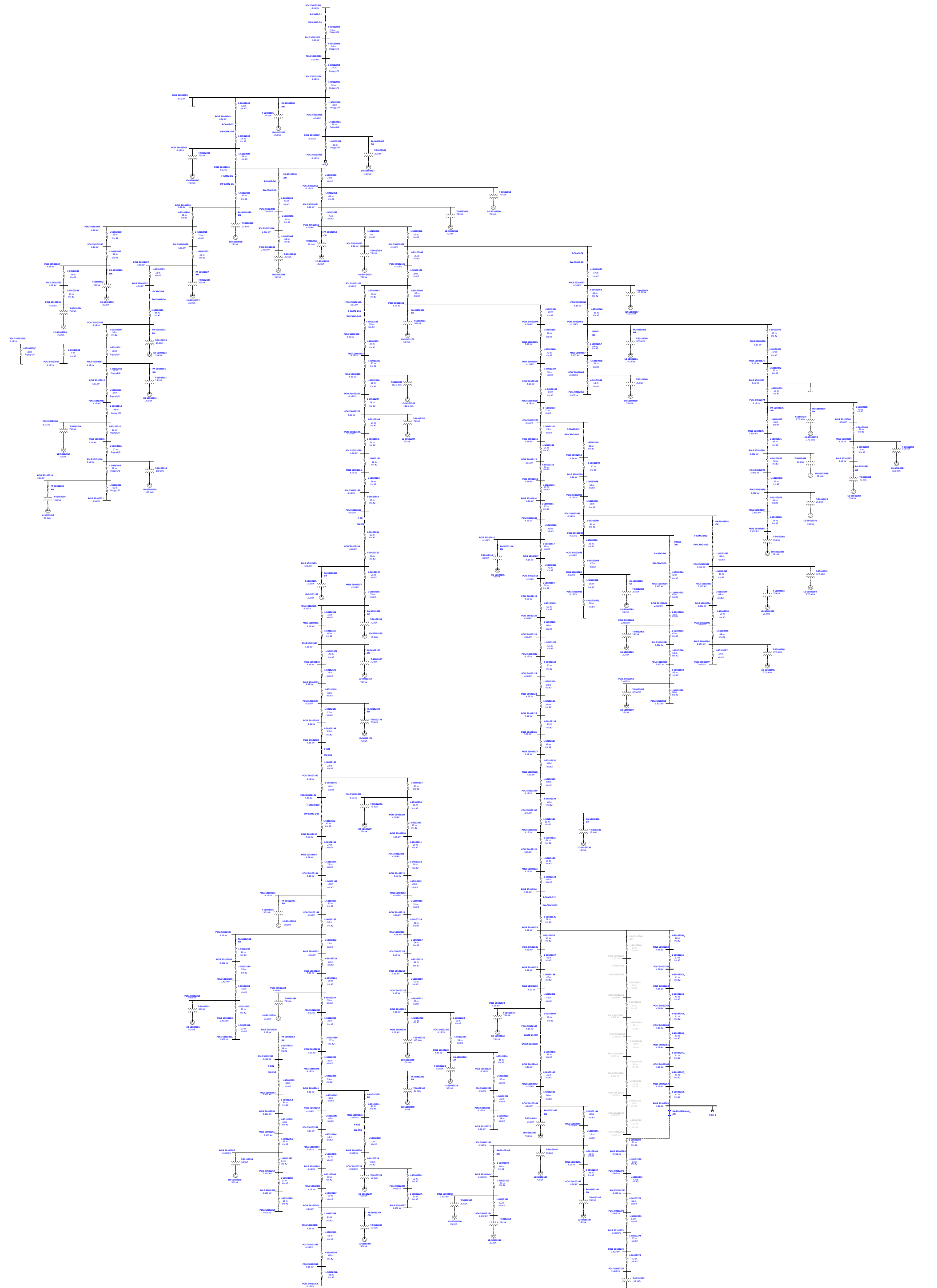
Option 5 was found to be the most technically preferred since it involves less voltage drop and active power losses.

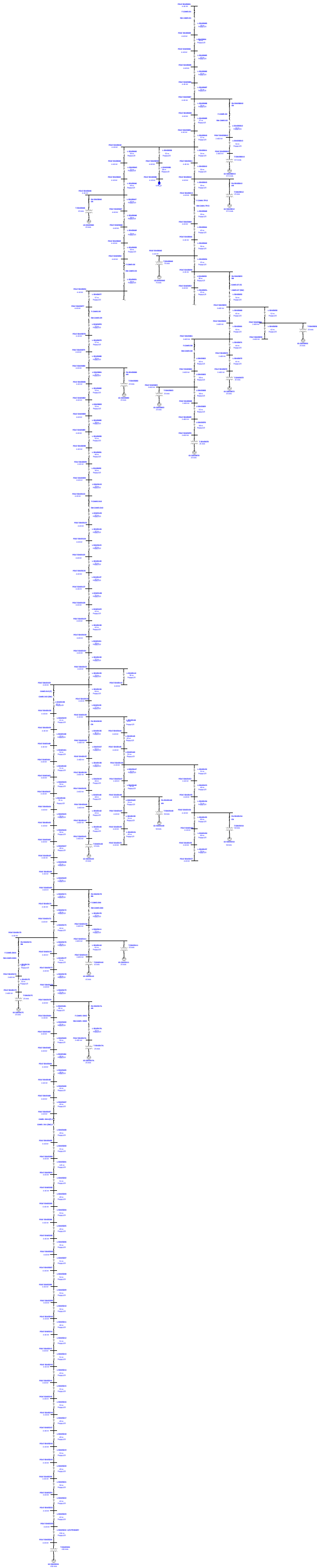
## **Appendix 1.A**

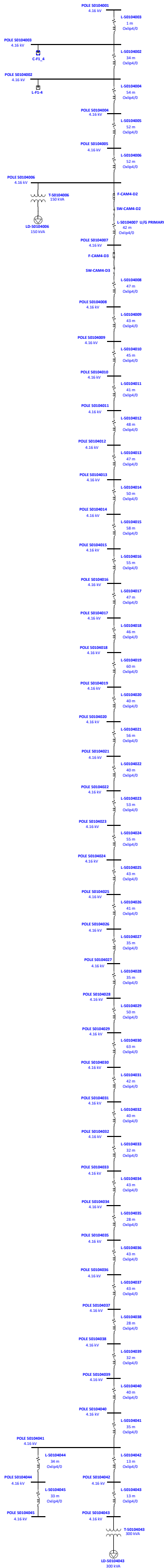
### **Cambridge Bay Network ETAP Model and Results – Option 1**











### Option #1

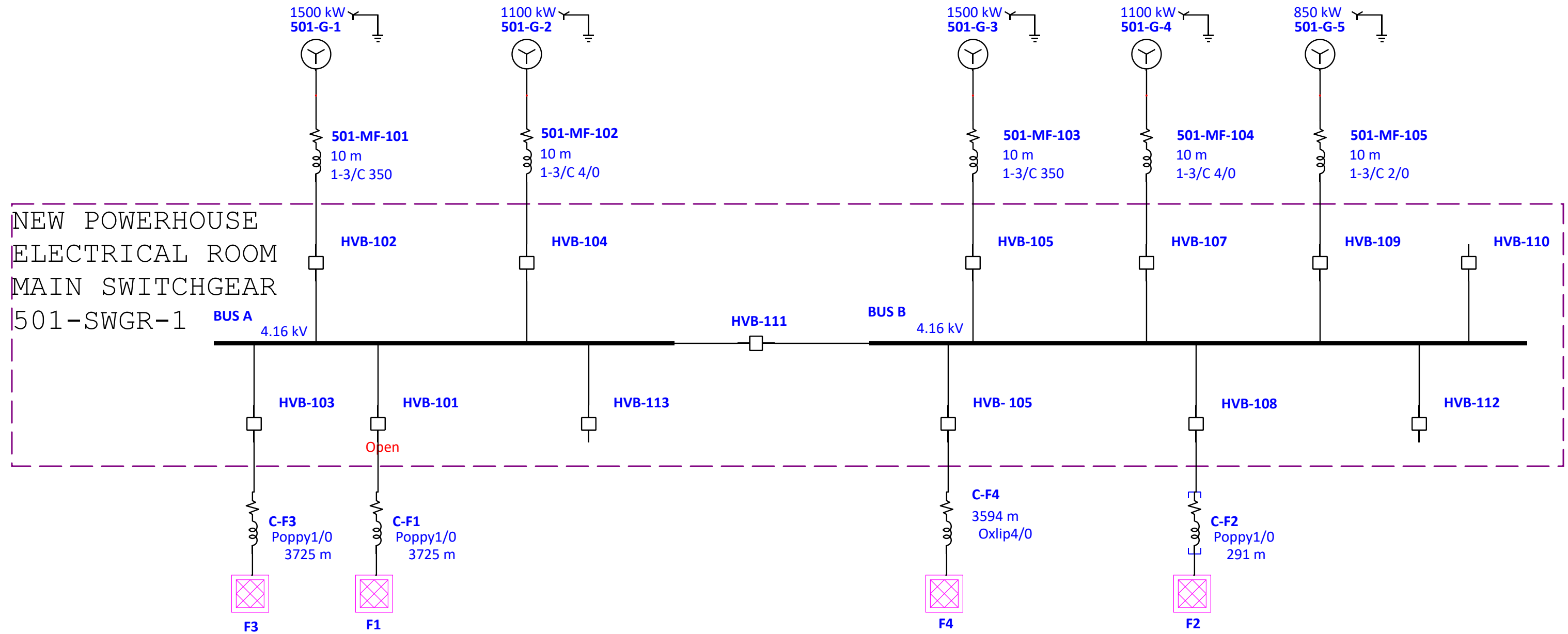
Year	F1		F2		F3		F4	
	Status	Min. Main Line Size L-F1-4	Status	Min. Main Line Size C-F2_3	Status	Min. Main Line Size L-F2_3	Status	Min. Main Line Size C-F1_4
2026		Failed	Passed	1/0 AWG		Failed		Failed
2027		Failed	Passed	1/0 AWG		Failed		Failed
2028		Failed	Passed	1/0 AWG		Failed		Failed
2029		Failed	Passed	1/0 AWG		Failed		Failed
2030		Failed	Passed	1/0 AWG		Failed		Failed
2031		Failed	Passed	1/0 AWG		Failed		Failed
2032		Failed	Passed	1/0 AWG		Failed		Failed
2033		Failed	Passed	1/0 AWG		Failed		Failed
2034		Failed	Passed	1/0 AWG		Failed		Failed
2035		Failed	Passed	1/0 AWG		Failed		Failed
2036		Failed	Passed	1/0 AWG		Failed		Failed
2041		Failed	Passed	2/0 AWG		Failed		Failed
2046		Failed	Passed	2/0 AWG		Failed		Failed
2051		Failed	Passed	3/0 AWG		Failed		Failed
2056		Failed	Passed	3/0 AWG		Failed		Failed
2061		Failed	Passed	4/0 AWG		Failed		Failed
2066		Failed	Passed	4/0 AWG		Failed		Failed

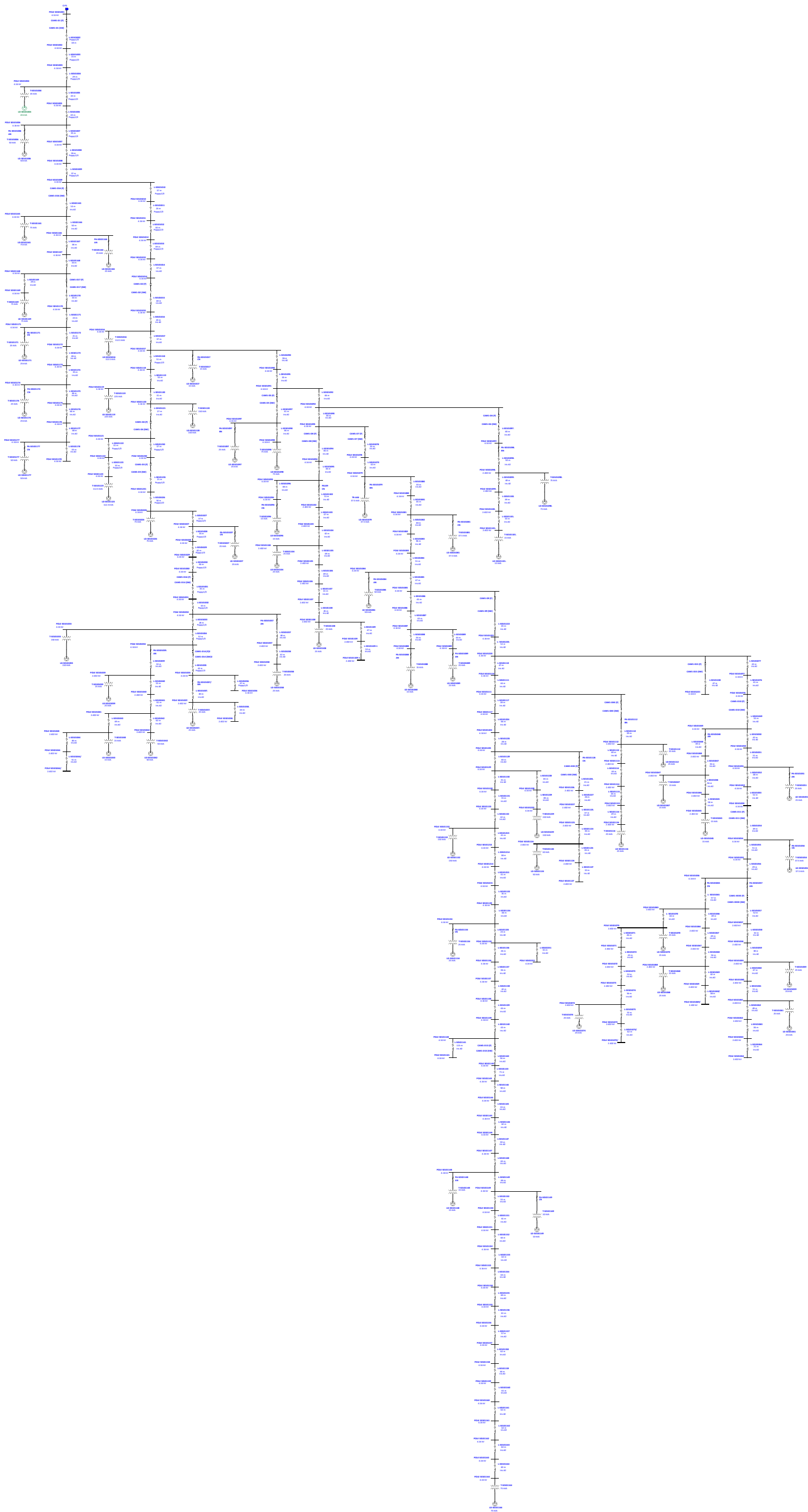


## **Appendix 1.B**

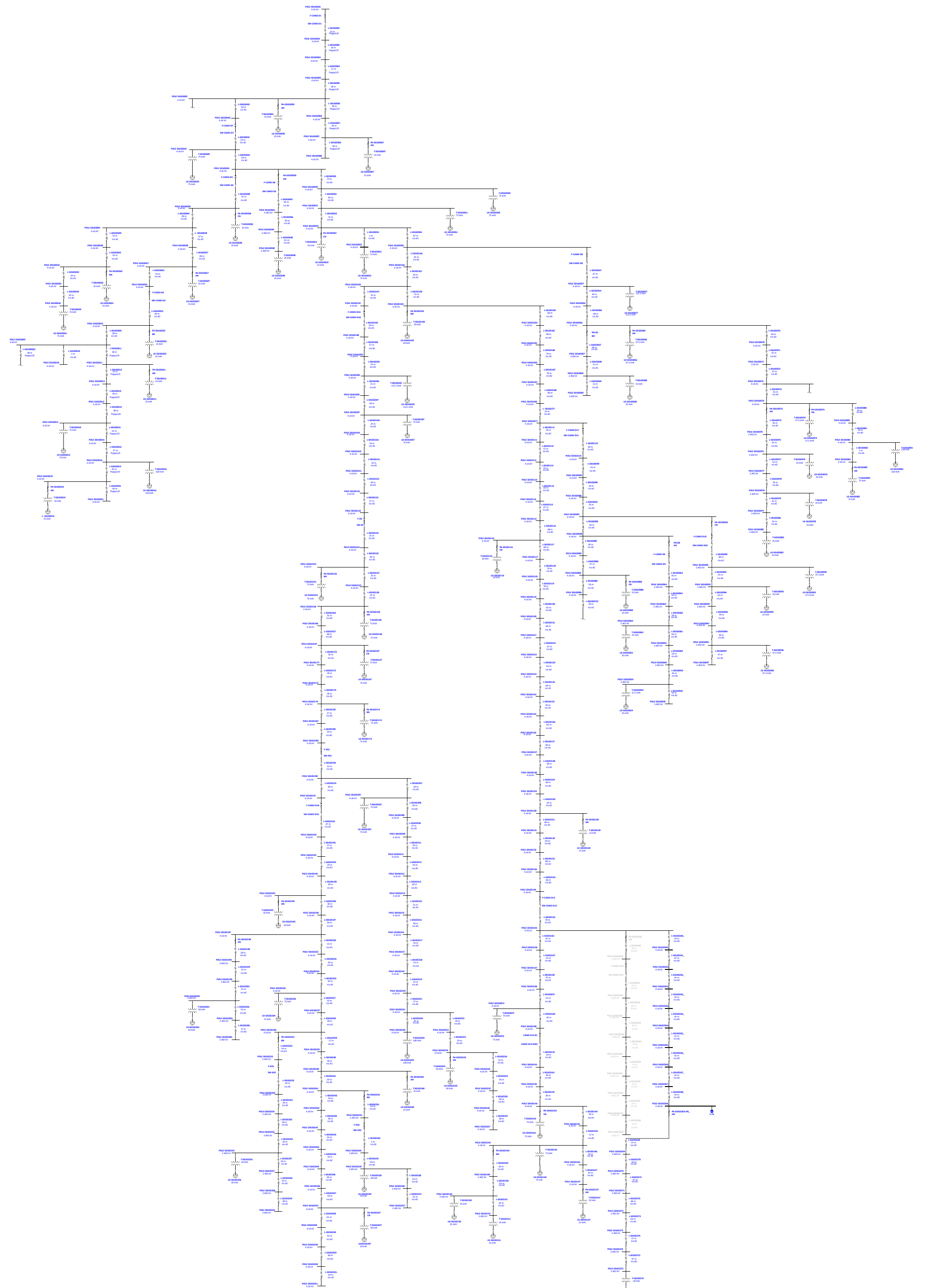
### **Cambridge Bay Network ETAP Model and Results – Option 2**

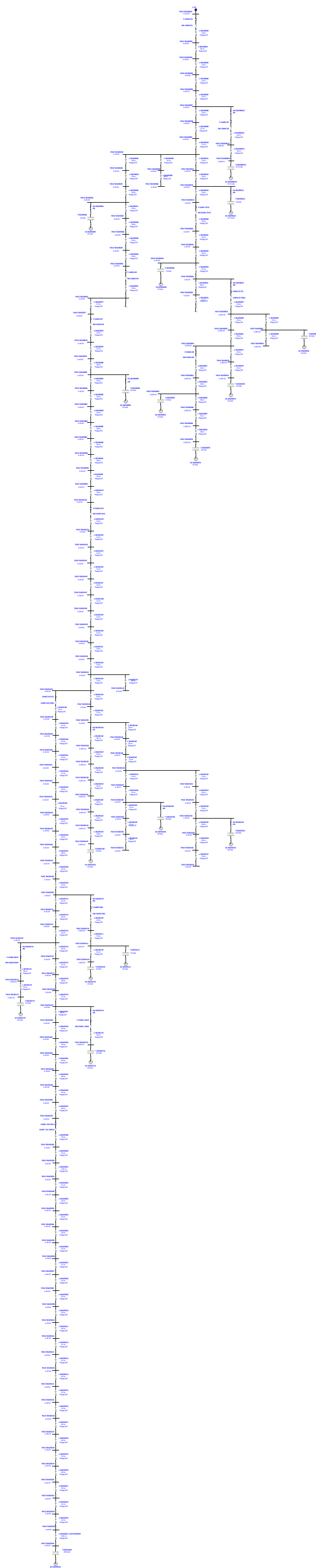
One-Line Diagram - OLV1 (Load Flow Analysis)

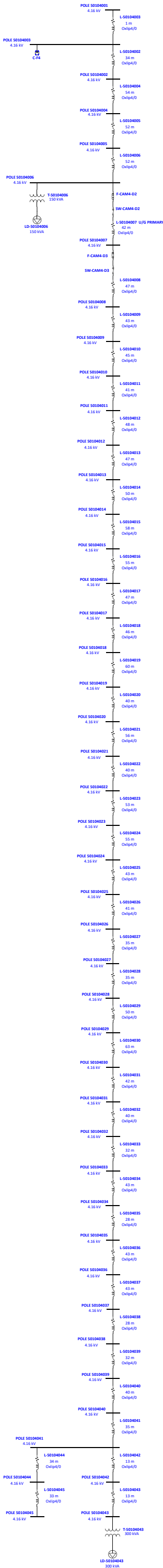




One-Line Diagram - OLV1=>F2 (Load Flow Analysis) - Ahmed.Abdelfattah(Project Editor)







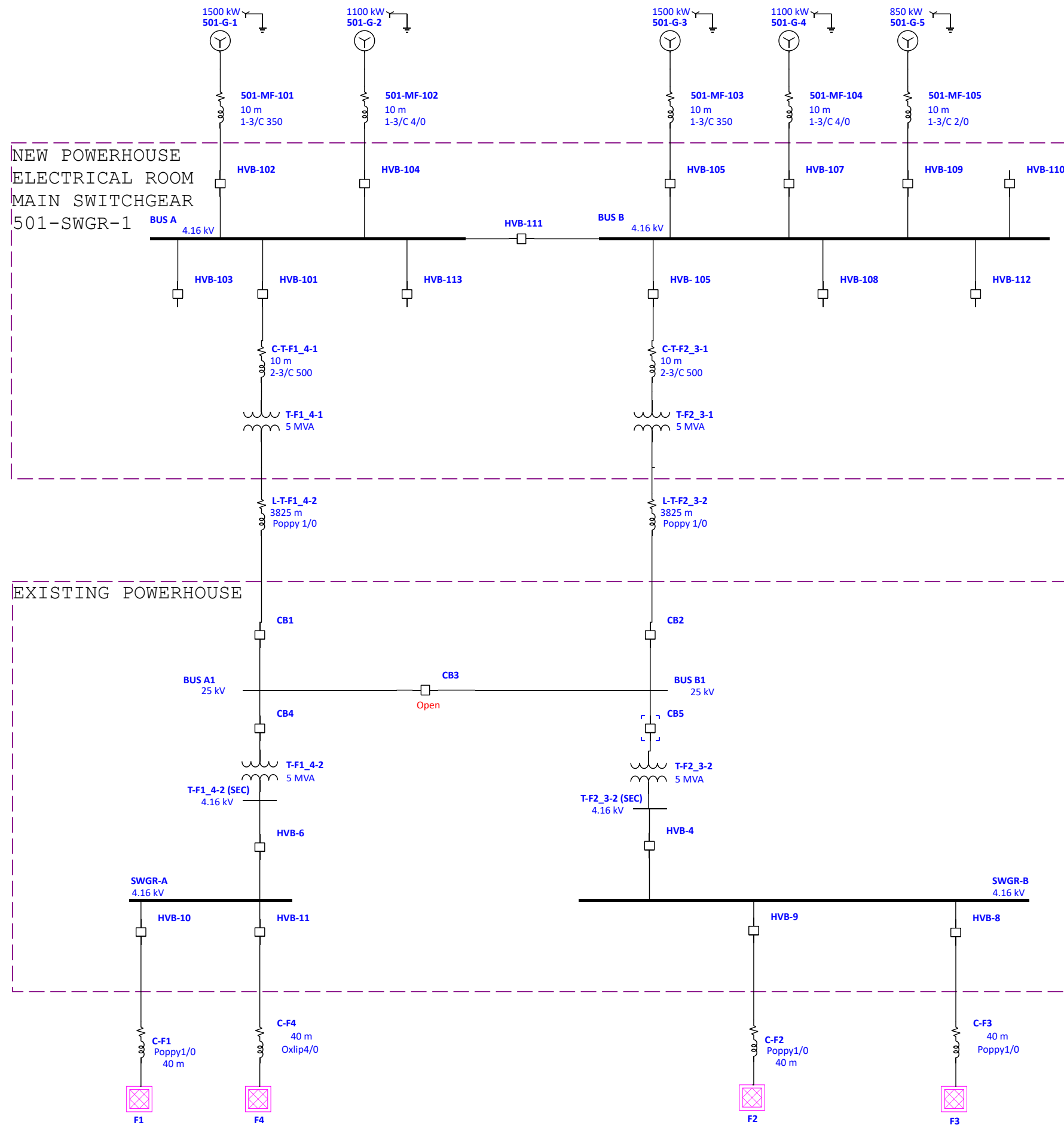
## Option #2

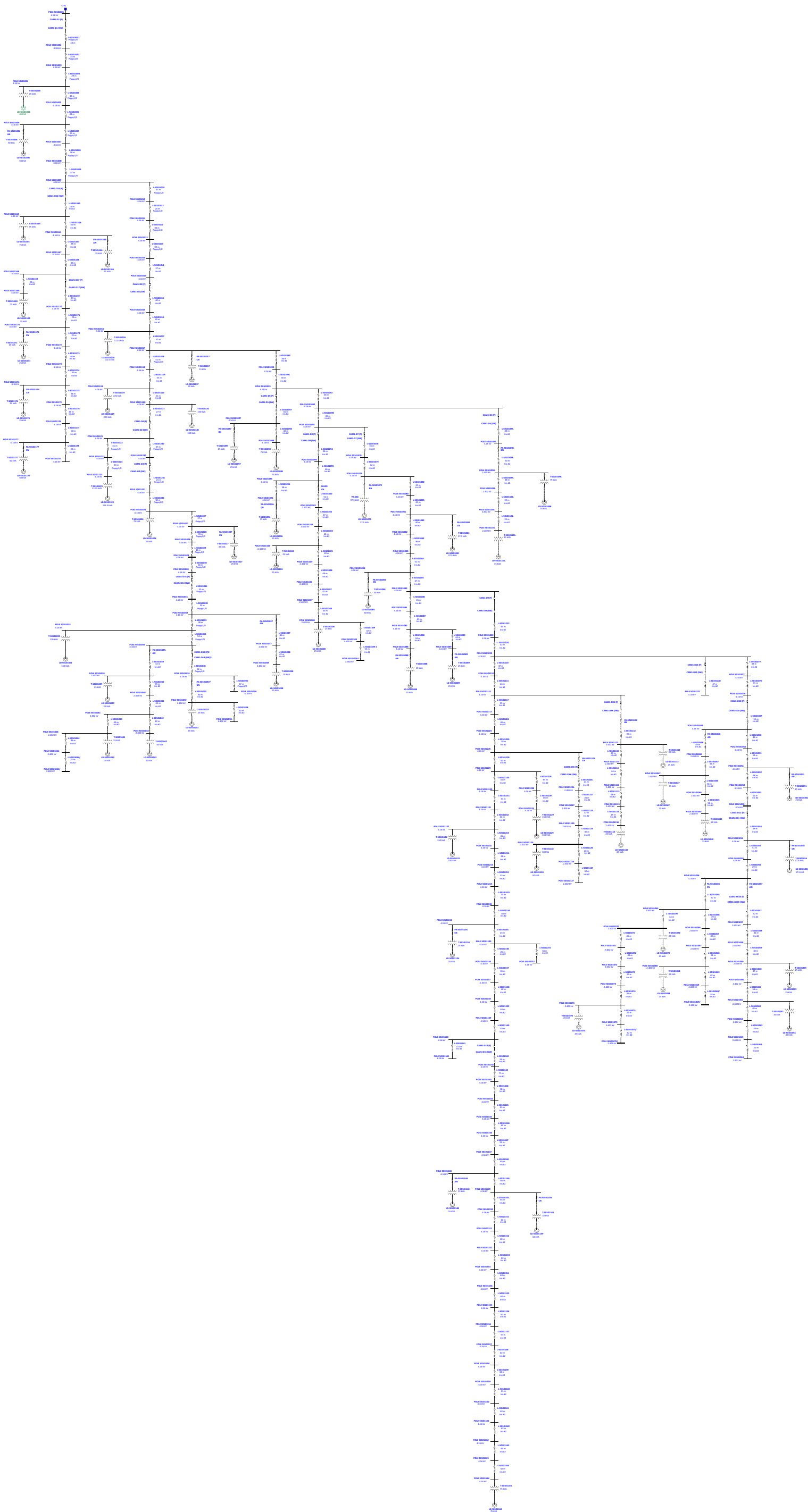
Year	F1		F2		F3		F4	
	Status	Min. Main Line Size C-F1	Status	Min. Main Line Size C-F2	Status	Min. Main Line Size C-F3	Status	Min. Main Line Size C-F4
2026		Failed	Passed	1/0 AWG		Failed		Failed
2027		Failed	Passed	1/0 AWG		Failed		Failed
2028		Failed	Passed	1/0 AWG		Failed		Failed
2029		Failed	Passed	1/0 AWG		Failed		Failed
2030		Failed	Passed	1/0 AWG		Failed		Failed
2031		Failed	Passed	1/0 AWG		Failed		Failed
2032		Failed	Passed	1/0 AWG		Failed		Failed
2033		Failed	Passed	1/0 AWG		Failed		Failed
2034		Failed	Passed	1/0 AWG		Failed		Failed
2035		Failed	Passed	1/0 AWG		Failed		Failed
2036		Failed	Passed	1/0 AWG		Failed		Failed
2041		Failed	Passed	1/0 AWG		Failed		Failed
2046		Failed	Passed	1/0 AWG		Failed		Failed
2051		Failed	Passed	1/0 AWG		Failed		Failed
2056		Failed	Passed	1/0 AWG		Failed		Failed
2061		Failed	Passed	1/0 AWG		Failed		Failed
2066		Failed	Passed	1/0 AWG		Failed		Failed

## **Appendix 1.C**

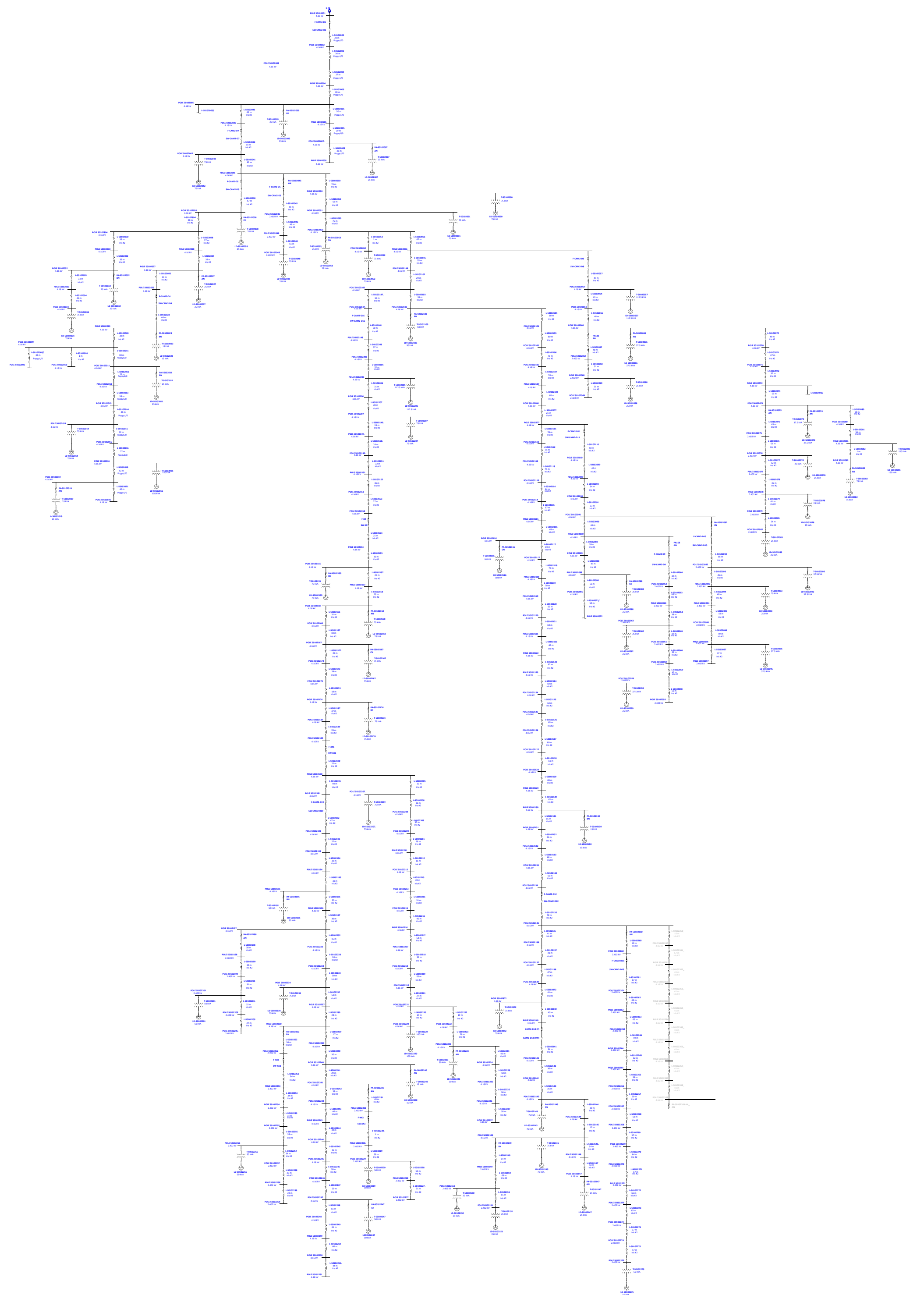
### **Cambridge Bay Network ETAP Model and Results – Option 3**

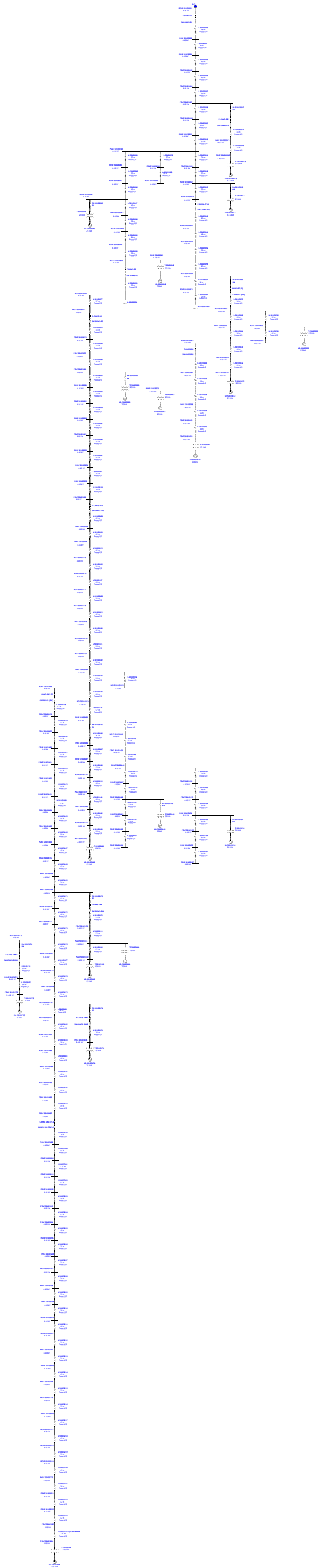


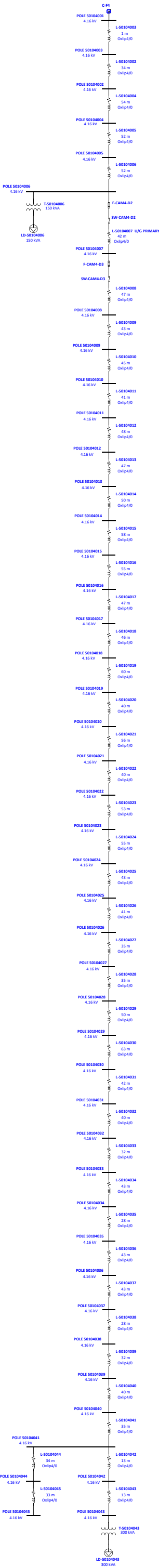




page 1      12:35:55      Oct 15, 2024      Project File: CambridgeBay\_Option\_3





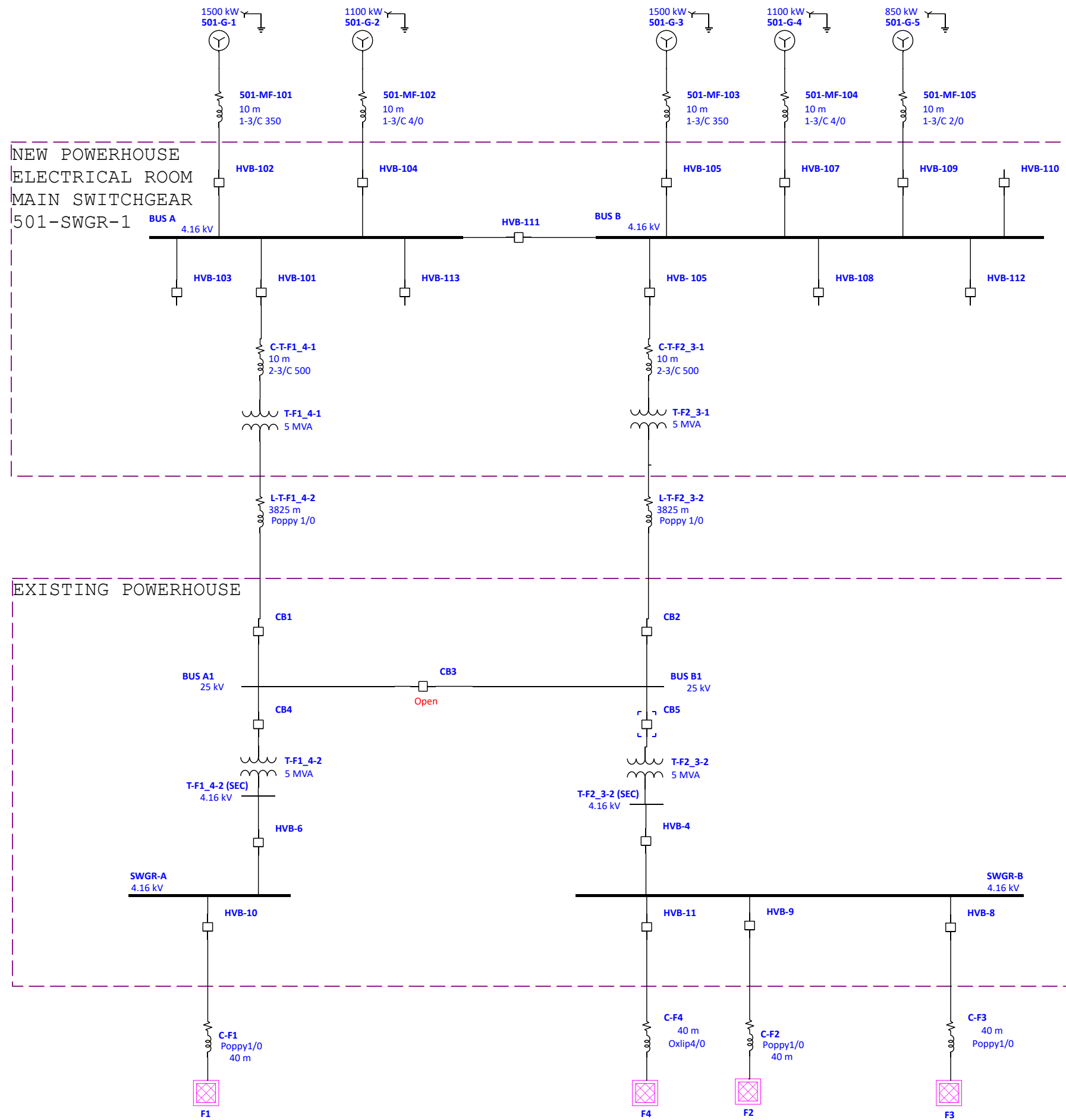




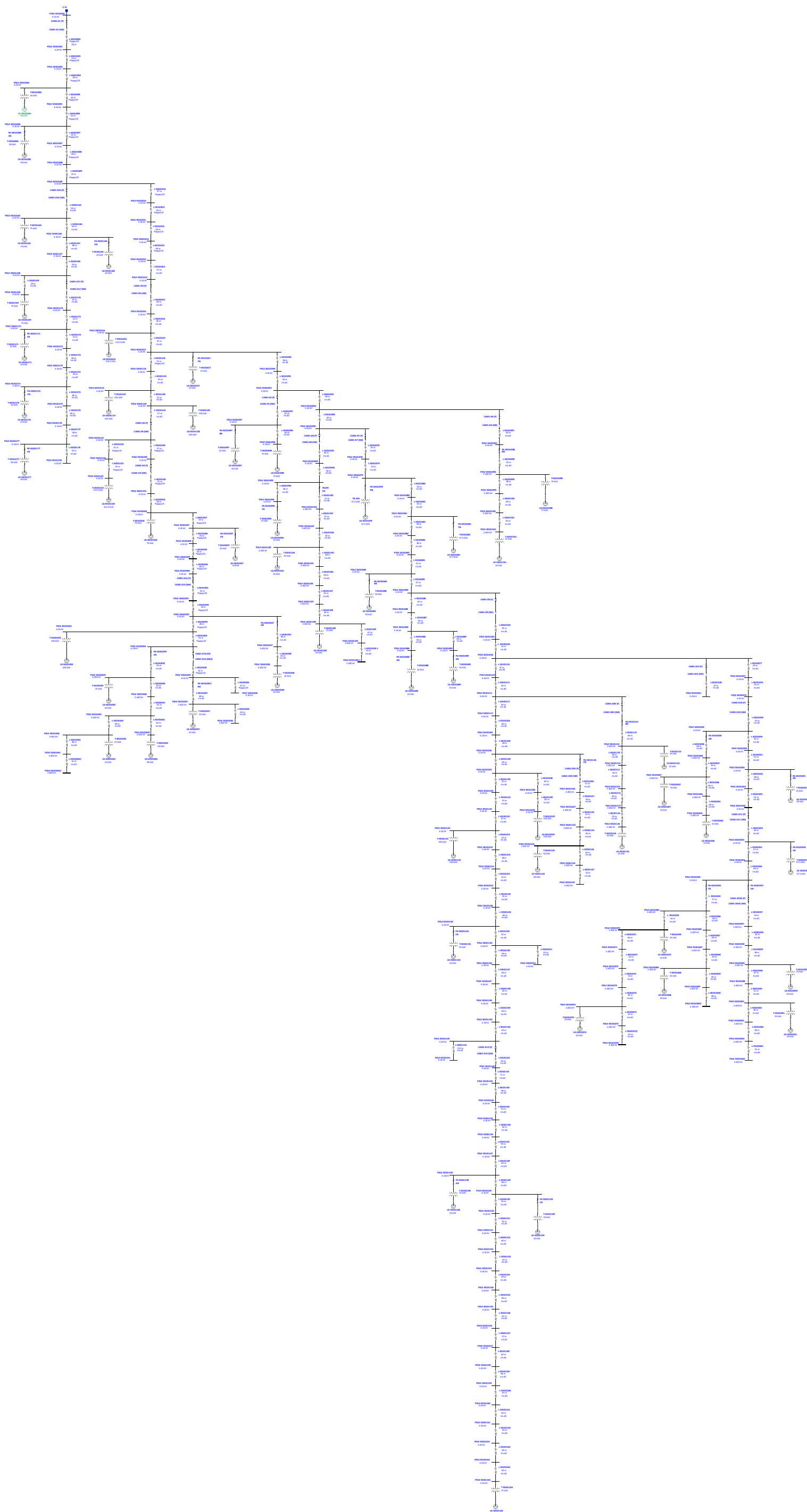
## **Appendix 1.D**

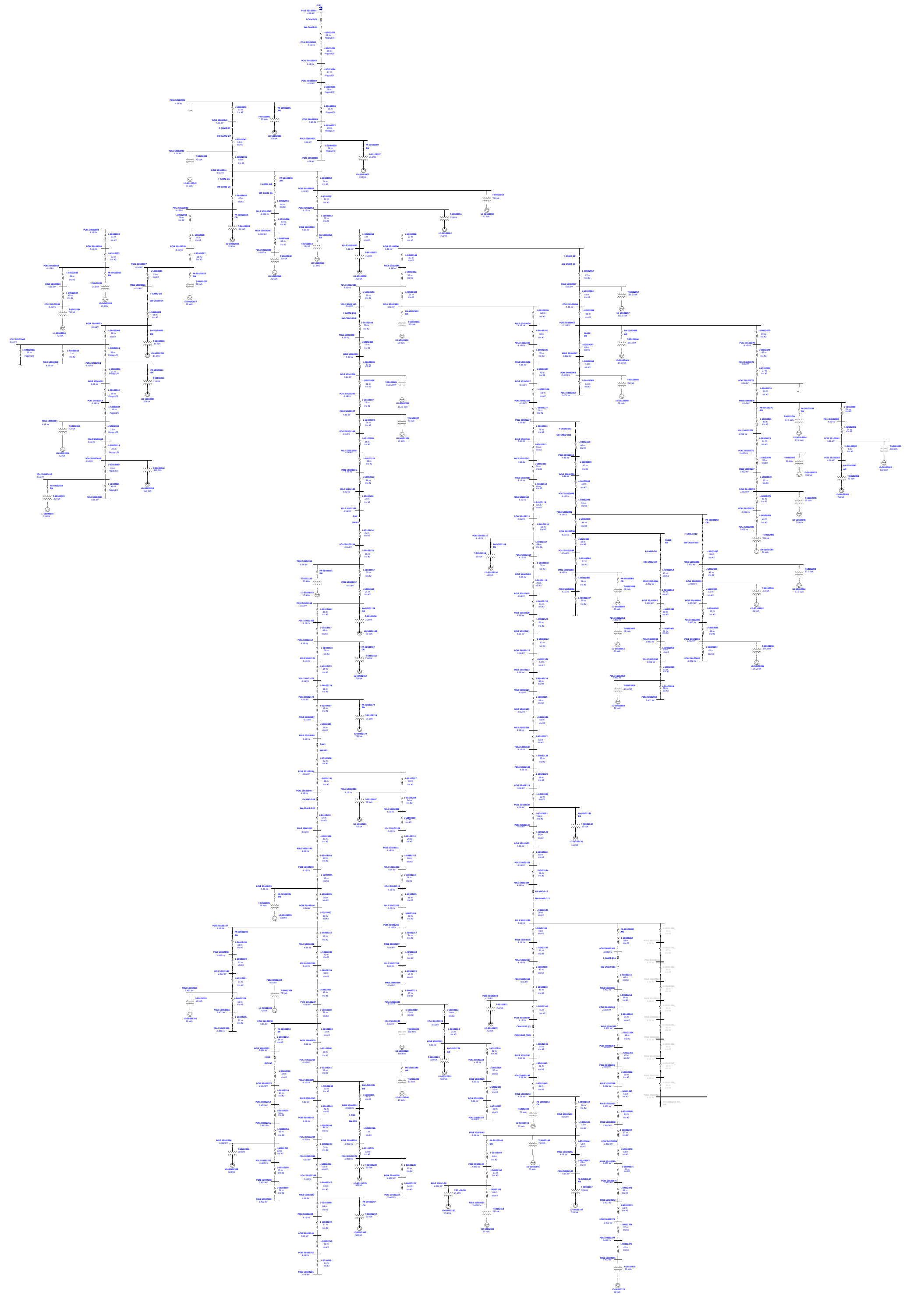
### **Cambridge Bay Network ETAP Model – Option 3A**

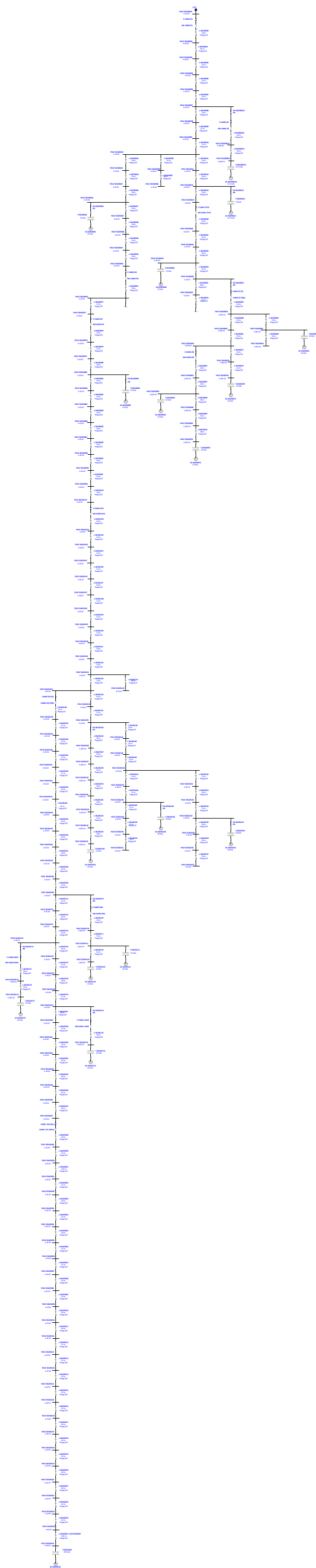
# One-Line Diagram - OLV1 (Load Flow Analysis)

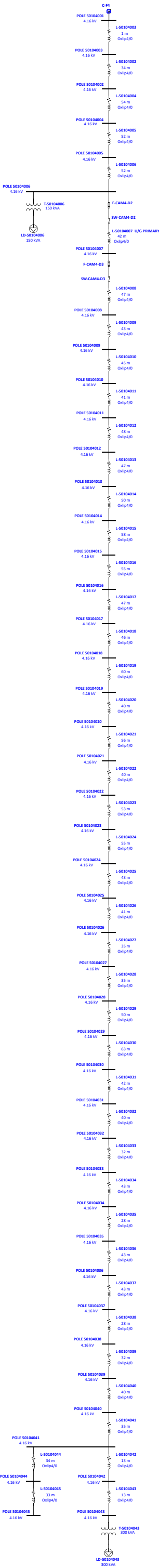












### Option 3A: Scenario A: All Feeders are Fed from One Step-up Transformer

[illegible]

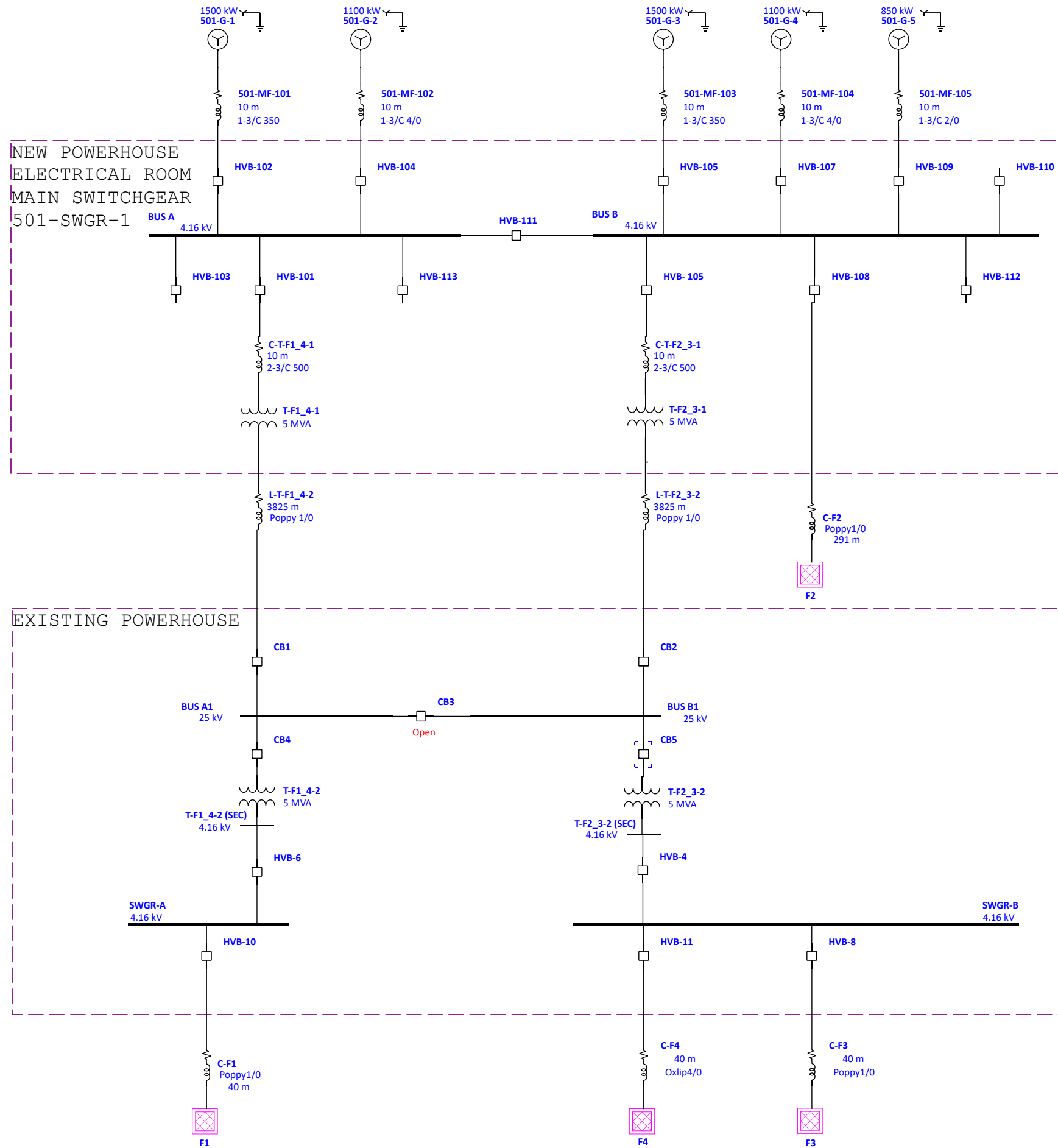
**Option 3A: Scenario B: Feeder 1 is Fed from T-F1 4-2 Step-up Transformer and Feeders 2, 3, and 4 are Fed from T-F2 3-2 Step-Up Transformer**

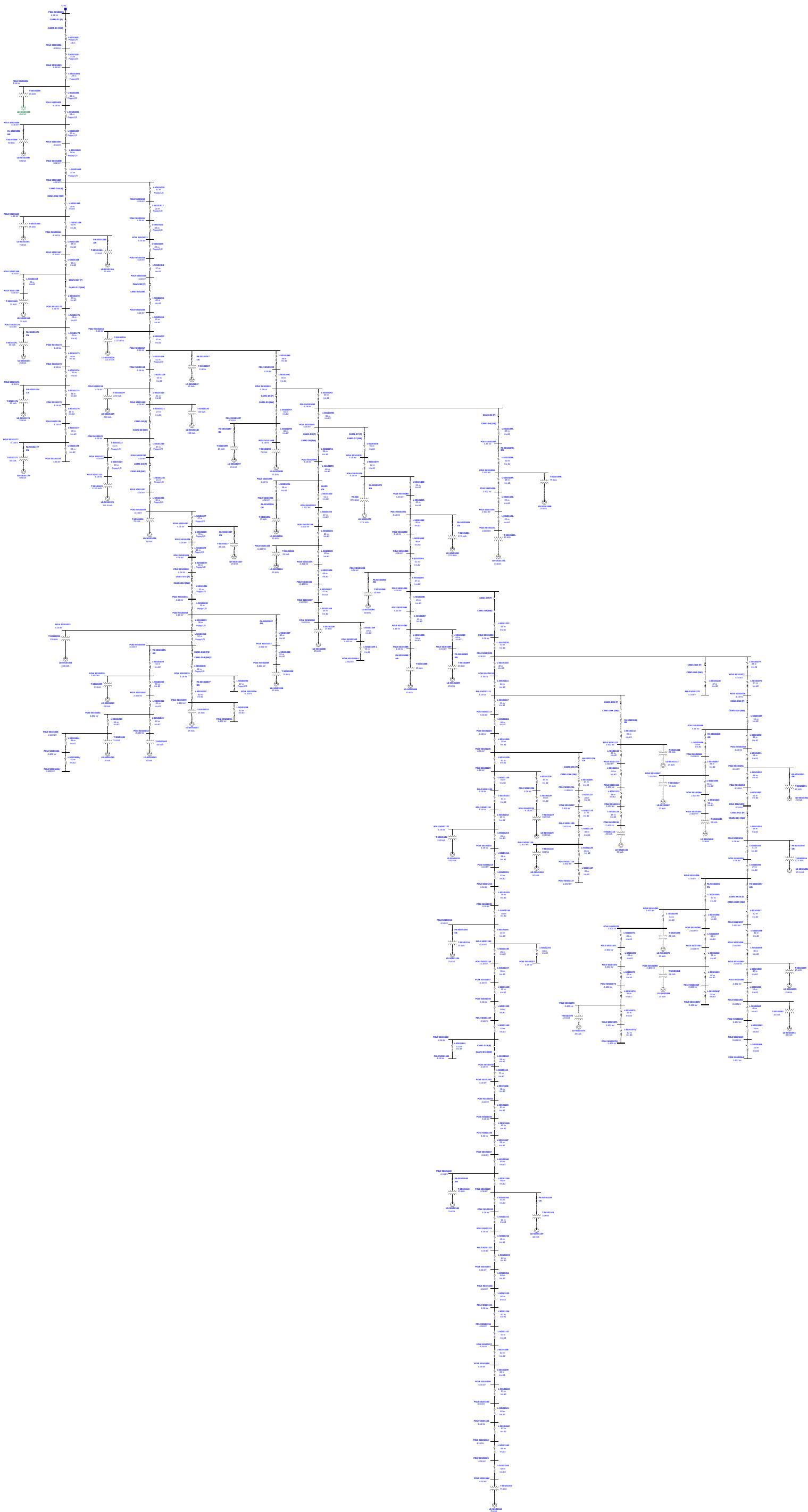
[illegible]

## **Appendix 1.E**

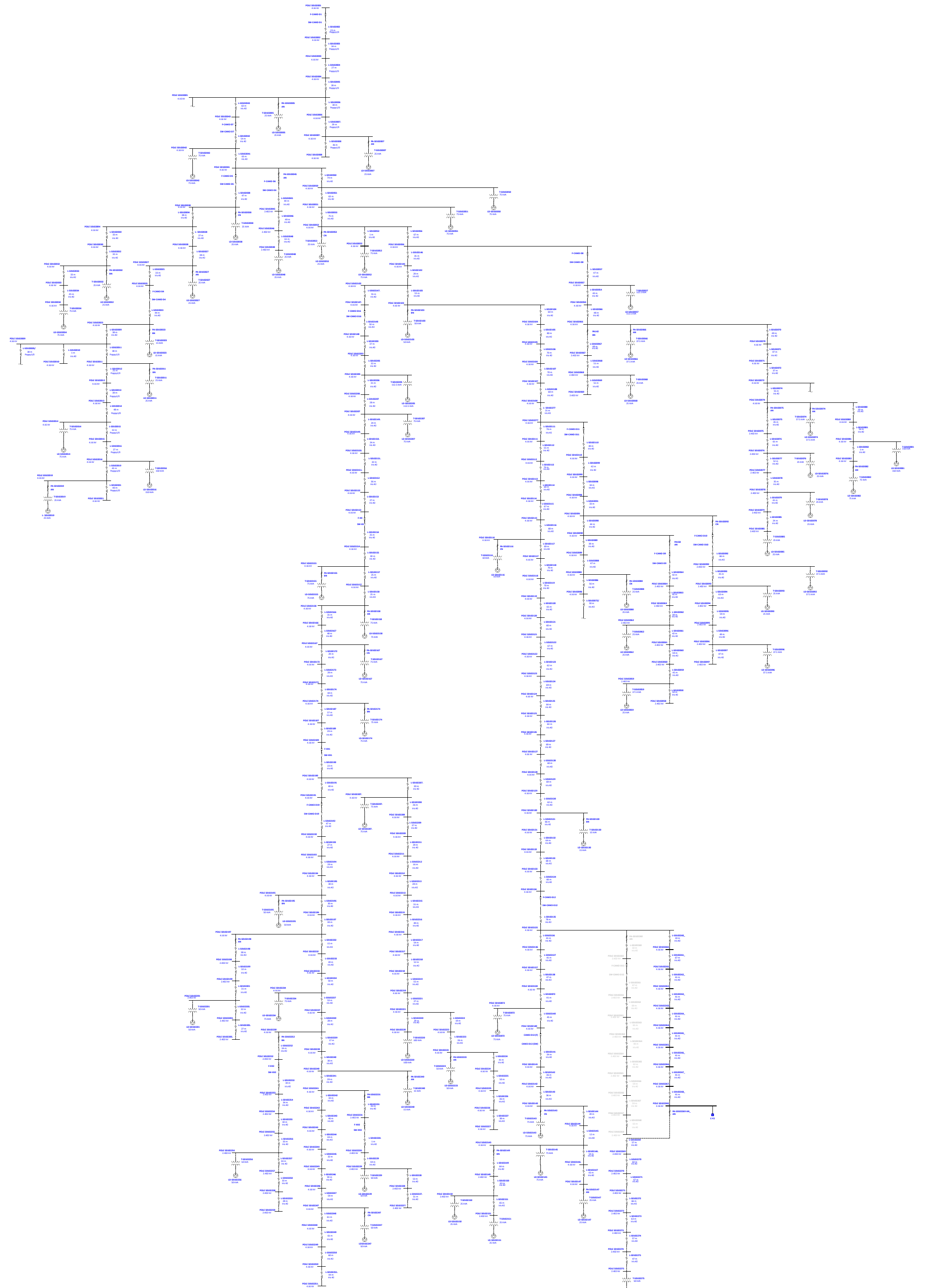
### **Cambridge Bay Network ETAP Model and Results – Option 3B**

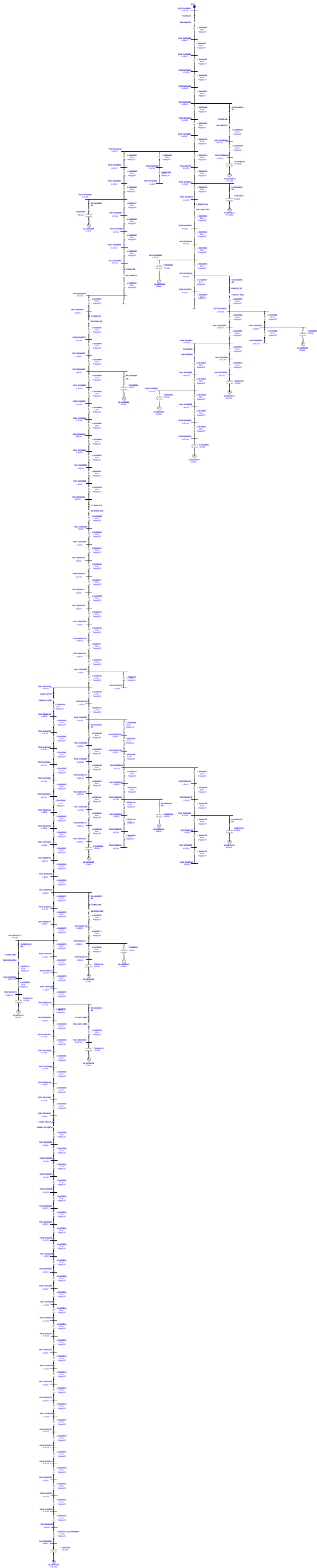
# One-Line Diagram - OLV1 (Load Flow Analysis)

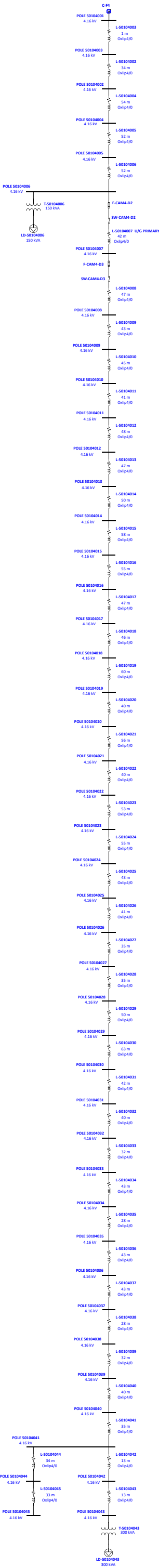












**Option 3B: Scenario A: All Feeders are Fed from One Step-up Transformer**

[illegible]

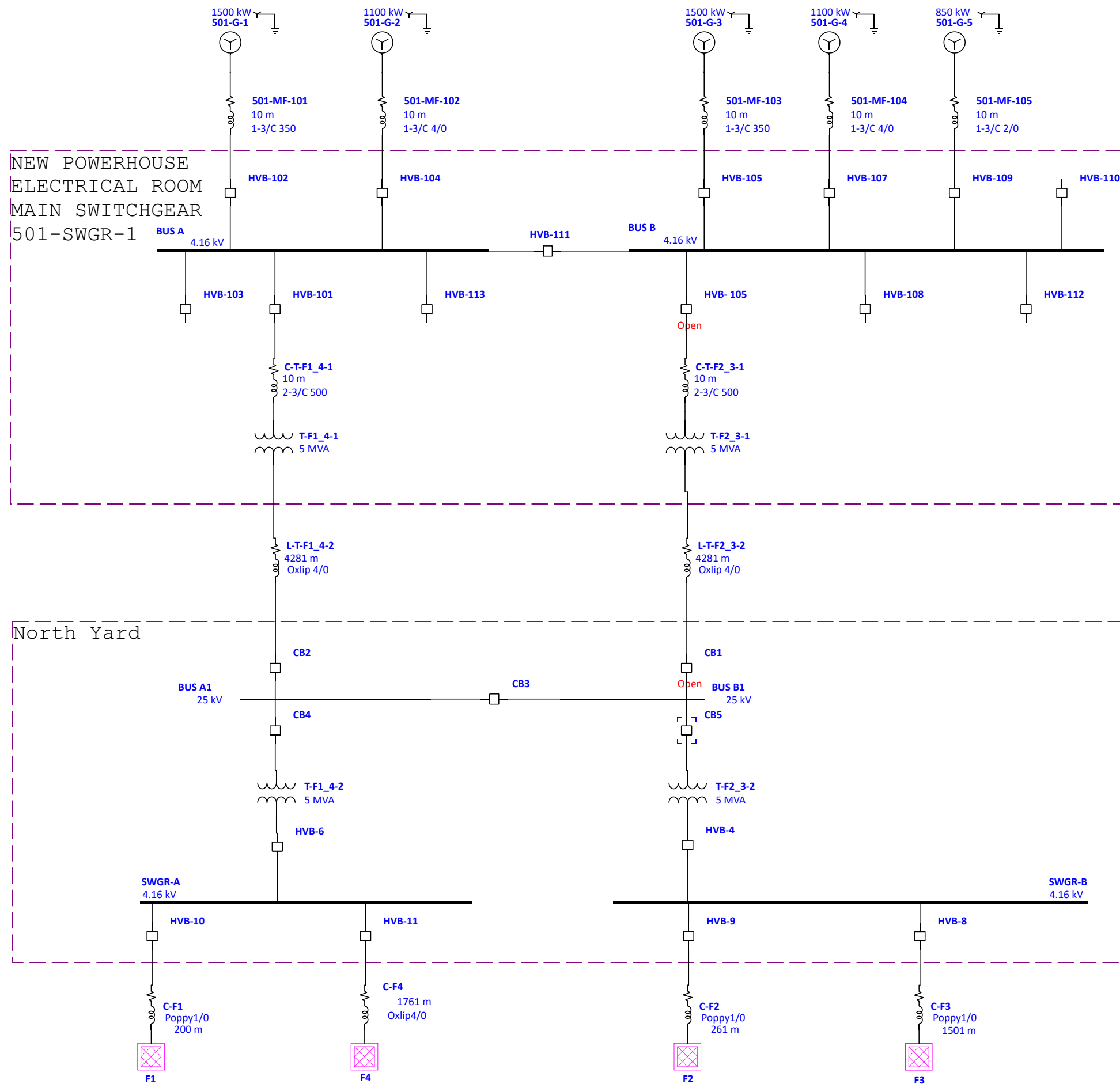
**Option 3B: Scenario B: Feeder 1 is Fed from T-F1 4-2 Step-up Transformer and Feeders 3 and 4 are Fed from T-F2 3-2 Step-Up Transformer**

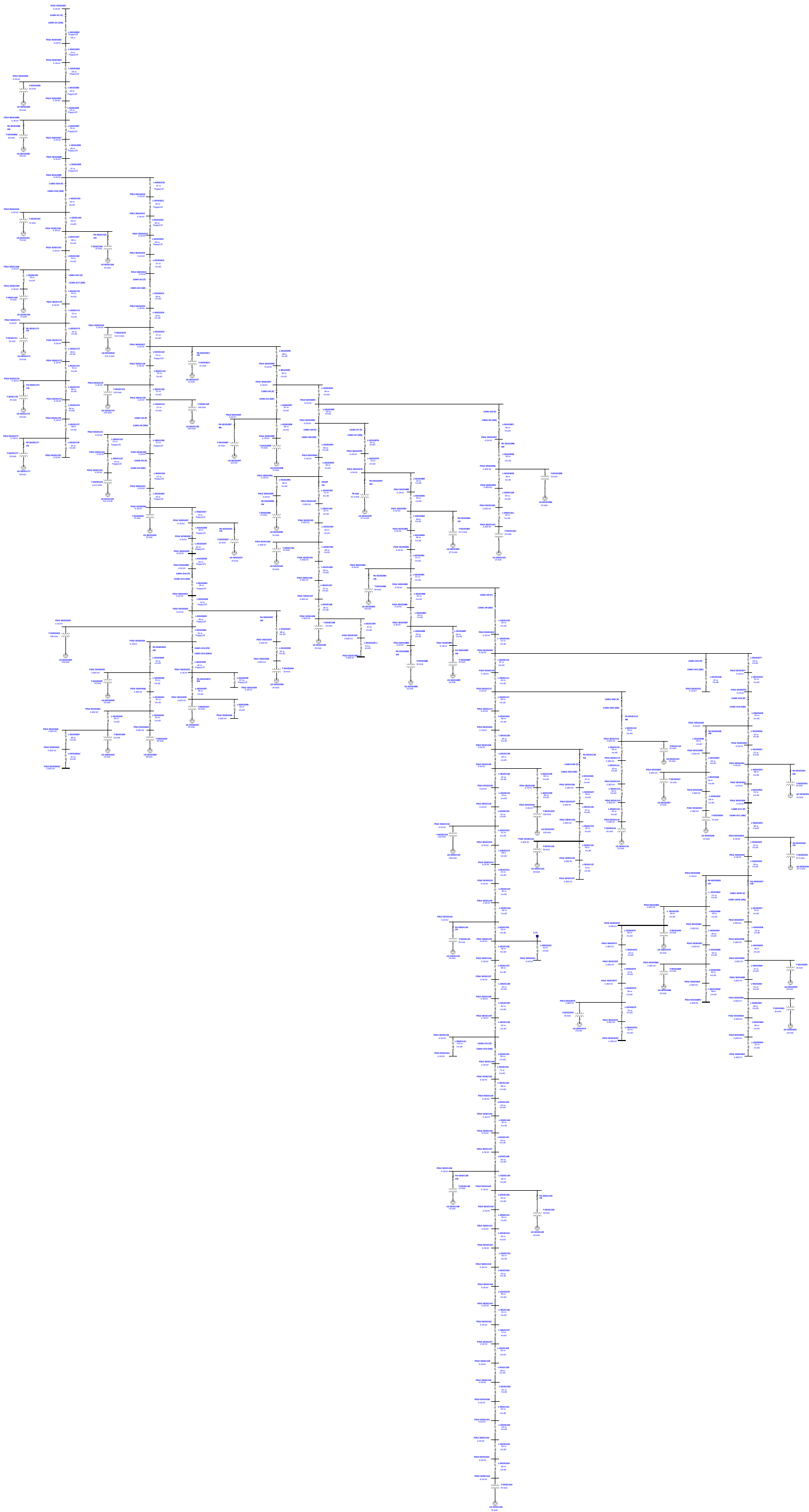
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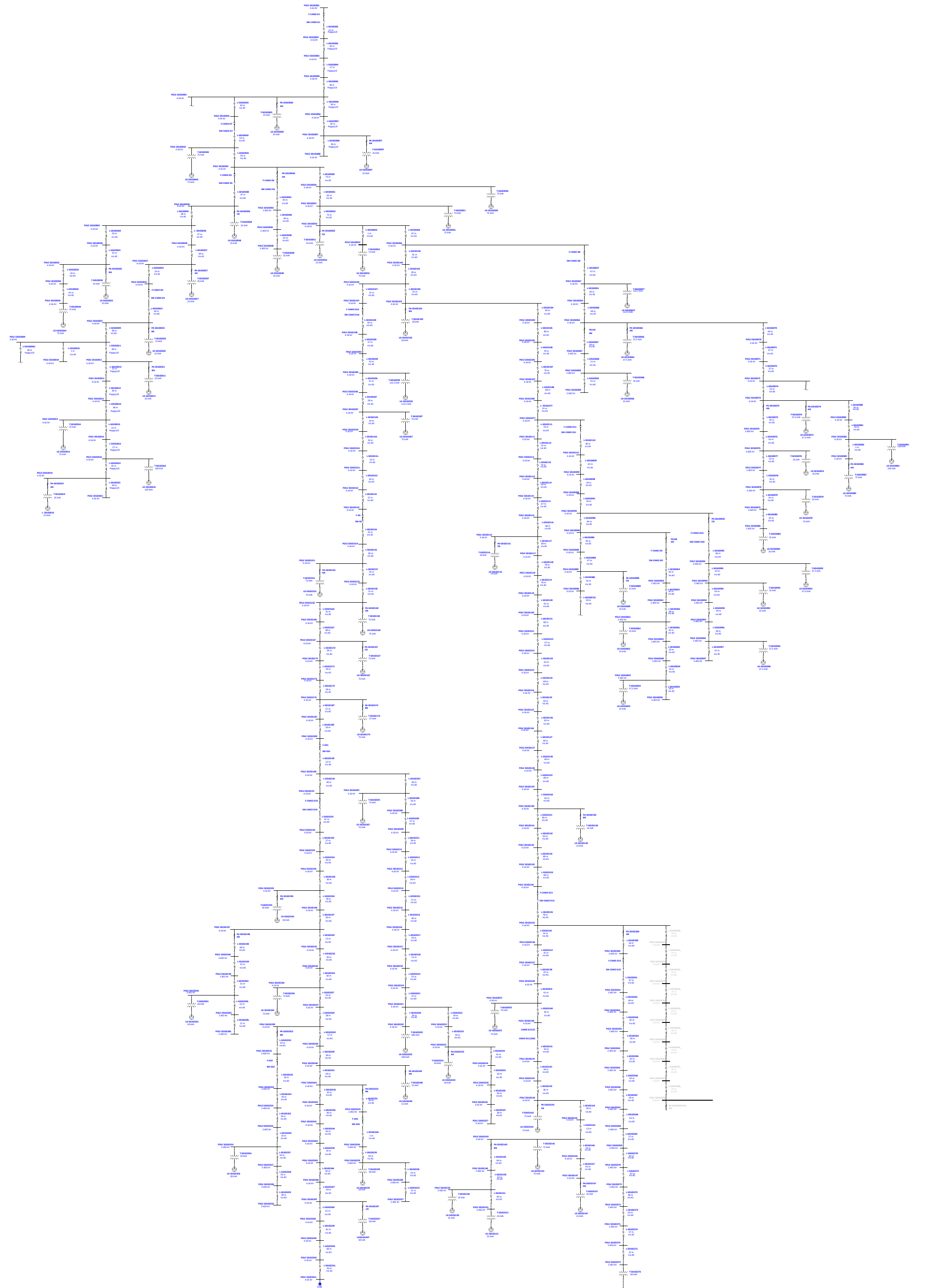
## **Appendix 1.F**

### **Cambridge Bay Network ETAP Model and Results – Option 4**

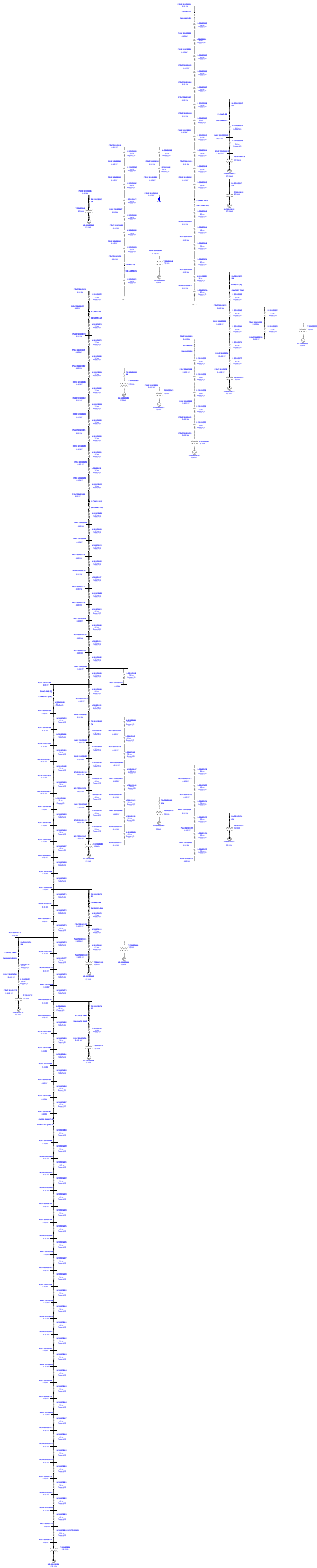
# One-Line Diagram - OLV1 (Load Flow Analysis)

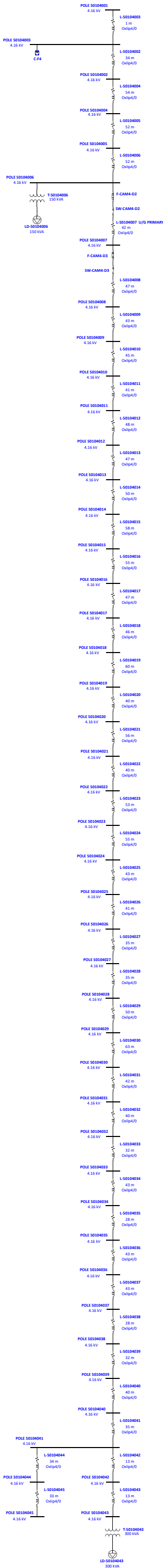










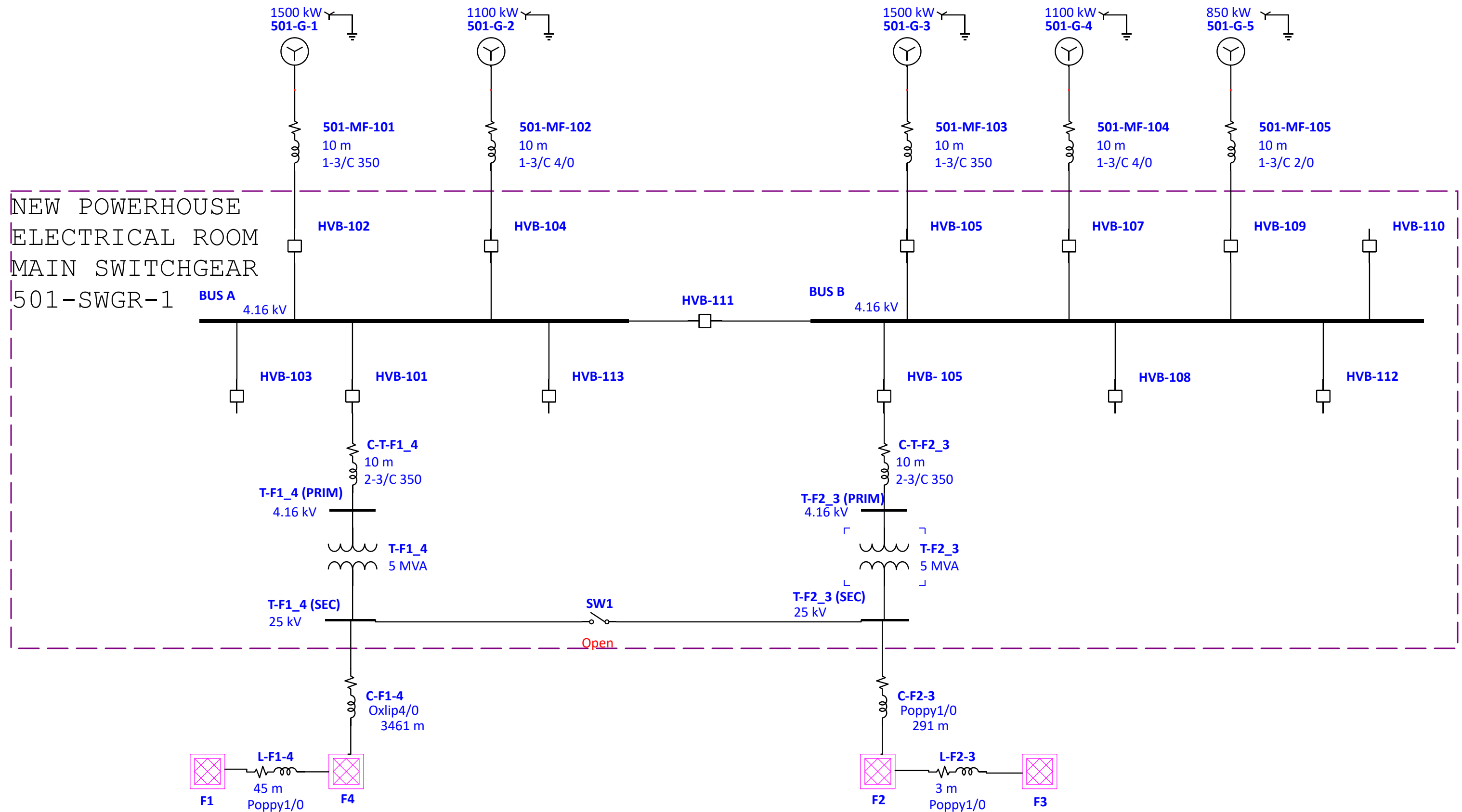


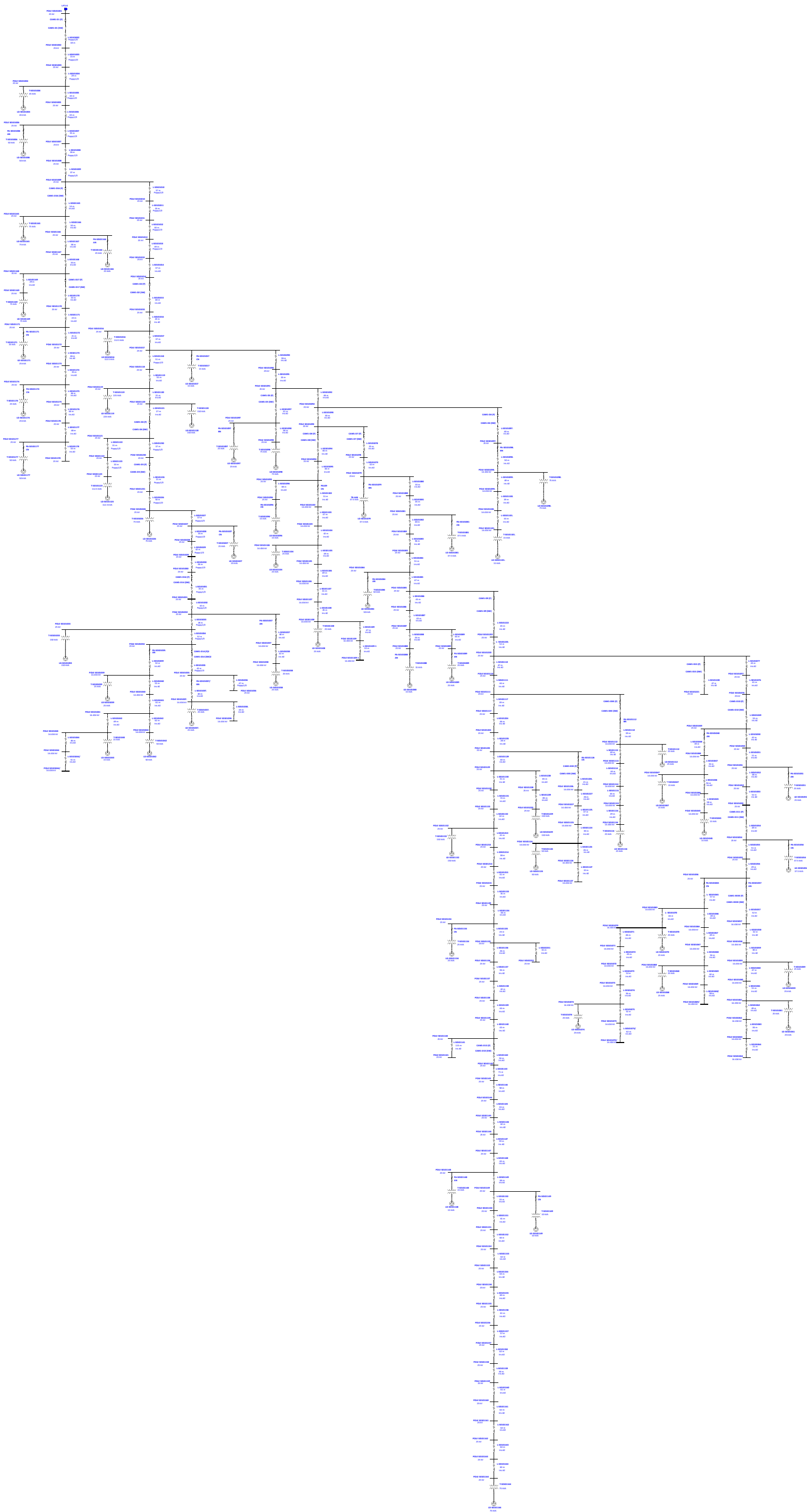


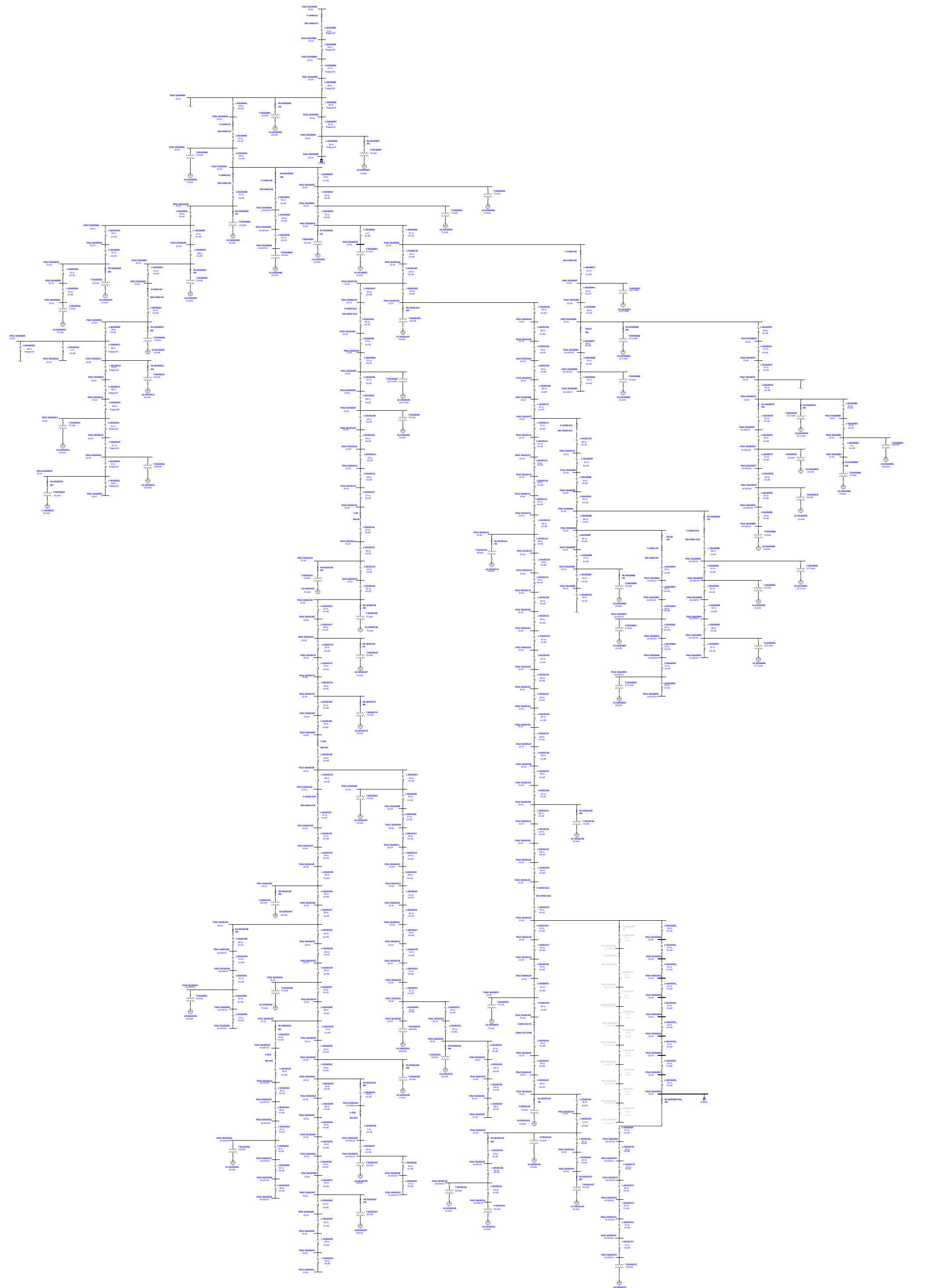
## **Appendix 1.G**

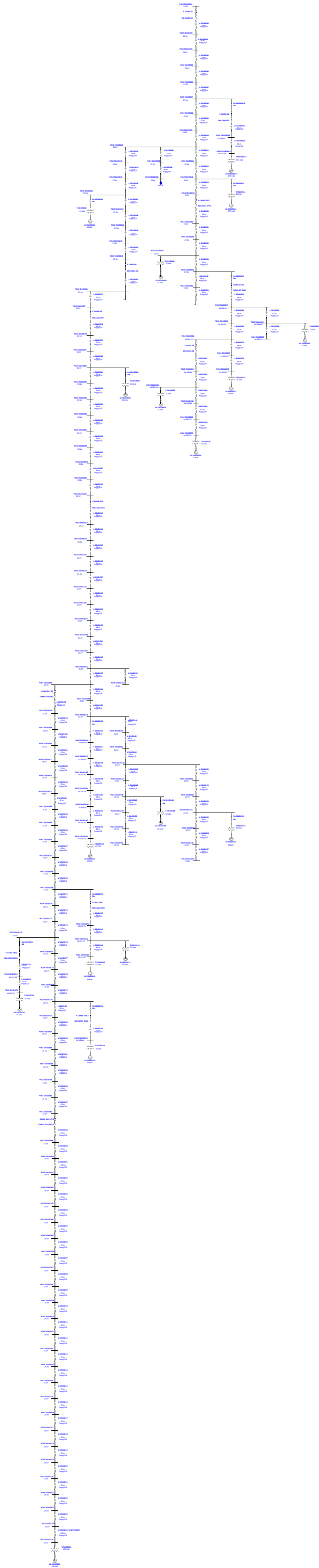
### **Cambridge Bay Network ETAP Model and Result – Option 5**

One-Line Diagram - OLV1 (Load Flow Analysis)

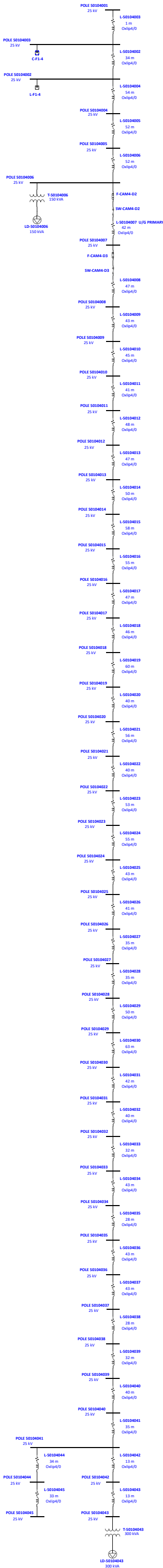














## **Appendix 2**

### **Cambridge Bay – Estimated Electricity Production**



## Appendix C: Calculated power plant electricity generation after 2026

**Estimated yearly electricity production for the new Cambridge Bay power plant**

Year	Population	Population change	Estimated electricity produced (kWh/year)
2026	2,451	+55	15,407,427
2027	2,507	+57	15,763,605
2028	2,565	+58	16,128,017
2029	2,625	+59	16,500,853
2030	2,685	+61	16,882,308
2031	2,747	+62	17,272,581
2032	2,811	+64	17,671,877
2033	2,876	+65	18,080,403
2034	2,942	+66	18,498,373
2035	3,010	+68	18,926,005
2036	3,080	+70	19,363,523
2037	3,151	+71	19,811,155
2038	3,224	+73	20,269,136
2039	3,298	+75	20,737,703
2040	3,375	+76	21,217,103
2041	3,453	+78	21,707,585
2042	3,532	+80	22,209,405
2043	3,614	+82	22,722,827
2044	3,698	+84	23,248,117
2045	3,783	+85	23,785,550
2046	3,871	+87	24,335,408
2047	3,960	+89	24,897,977
2048	4,052	+92	25,473,551
2049	4,145	+94	26,062,430
2050	4,241	+96	26,664,923
2051	4,339	+98	27,281,344
2052	4,439	+100	27,912,015
2053	4,542	+103	28,557,265
2054	4,647	+105	29,217,432
2055	4,755	+107	29,892,860
2056	4,864	+110	30,583,902
2057	4,977	+112	31,290,919
2058	5,092	+115	32,014,280
2059	5,210	+118	32,754,364
2060	5,330	+120	33,511,556
2061	5,453	+123	34,286,252
2062	5,579	+126	35,078,858
2063	5,708	+129	35,889,786
2064	5,840	+132	36,719,461
2065	5,975	+135	37,568,315
2066	6,113	+138	38,436,793



# Engineering Study Final Report

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<b>Document No.</b>	<b>2401E002ST Cambridge Bay</b>
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## **Revision History**

			Asher Engineering Ltd.			Qulliq Energy Corporation
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The results presented in the report are at a conceptual level; no detailed engineering has yet been performed, nor has equipment been selected or an operational plan been defined.

Use of this Document acknowledges acceptance of the foregoing conditions.

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## **Executive Summary**

QEC is building a new power plant on the south-west side of Cambridge Bay to provide sufficient energy to this community. Due to the remote location of the new power plant, different approaches for connecting the existing community feeders to the new power plant were studied.

After studying the different options for the possibility of feeding the existing community feeders from the new power plant, as explained in Cambridge Bay Power Plant Feeder Distribution Line Study 2401E001ST Rev. C, QEC advised to investigate the feasibility to implement the following option (Referenced as Option 4 in the report):

- A new power plant will be constructed in the south-west part of Cambridge Bay community. The new power plant will comprise Five (5) 4.16kV generators, 4.16kV switchgear and Two (2) 4.16/25kV, 5MVA, step-up transformers.
- A new substation will be constructed at the North Yard on the north side of Cambridge Bay community. The new substation will comprise One (1) 25kV switchgear, Two (2) 25/4.16kV, 5MVA, step-down transformers, and Two (2) 4.16kV switchgears.
- The new substation will be connected to the new power plant via Two (2) 25kV transmission lines.

The above option is discussed in detail in Section 1.3. The single-line diagrams showing the network topology are included in Appendix 1.

The previous study showed that this option does not accommodate the load forecast up to the year 2066, and that the off-line tap changers of both step up and step down transformers need to be adjusted to mitigate the voltage drop due to future load increase. Therefore, an alternative approach for voltage drop mitigation was studied as part of the scope of this report. The alternative approach involves the use of Automatic Voltage Regulators (AVRs) that are strategically placed in order to maintain the voltage drop within the  $\pm 3\%$  voltage limits while keeping the network losses at a minimum.

The study considers the estimated electricity production for the years from 2026 to 2066 as shown in Appendix 2.

The study recommends the use of AVRs in the following locations:

- Two (2), 4.16kV, 5MVA, AVRs, one on the primary side of each step-up transformer in the new power plant.
- Feeder 1: Two (2), 4.16kV, 2.5MVA, AVRs on the supply side of Poles 50101135 and 50101225.
- Feeder 2: One (1), 4.16kV, 3.5MVA, AVR on the supply side of Pole 50102135.
- Feeder 3: One (1), 4.16kV, 1MVA, AVR on the supply side of Pole 50103013.
- Feeder 4: One (1), 4.16kV, 0.8MVA, AVR on the supply side of Pole 50104003.

The current study considers that Feeder 2 is connected to the new power plant at Pole 50102260 which is the closest pole with three-phase lines. An alternative option is to connect Feeder 2 to the new power plant at Pole 50102268 which is closer to the power plant and replace the single-phase transmission lines between Poles 50102268 and 50102260 with three-phase. Although this option involves additional transmission lines to be installed, it will eliminate the need for an AVR for Feeder 2.

Table 3 summarizes the study results.

**Table 3: Study Results Summary**

			Operating Scenario		Remarks
			A	B	
Main Power Plant	Min. Main Feeder Line Size		4/0 AWG	1/0 AWG	
	AVR Tap Setting	AVR-T-F1_4-1	-5%	-2.5%	
		AVR-T-F2_3-1	-5%	-2.5%	
Feeder 1	Min. Main Feeder Line Size		2/0 AWG	1/0 AWG	
	AVR Tap Setting	AVR-50101135	-6.25%	-5.625%	
		AVR-50101225	-3.75%	-3.75%	
Feeder 2	Min. Main Feeder Line Size		1/0 AWG	1/0 AWG	
	AVR Tap Setting AVR-50102135		-3.75%	-3.75%	
Feeder 3	Min. Main Feeder Line Size		3/0 AWG	1/0 AWG	
	AVR Tap Setting AVR-50103013		-7.5%	-7.5%	
Feeder 4	Min. Main Feeder Line Size		4/0 AWG	4/0 AWG	
	AVR Tap Setting AVR-50104003		-4.375%	-3.75%	

Scenario A: Feeders 1, 3, and 4 are fed from one North Yard Switchgear incomer.

Scenario B: Feeders 1, 3, and 4 are fed from both North Yard Switchgear incomers.

## 1. Introduction

### 1.1 Background

QEC is building a new power plant on the south-west side of Cambridge Bay to provide sufficient energy to this community. Due to the remote location of the new power plant, different approaches for connecting the existing community feeders to the new power plant were studied. The previous study, Cambridge Bay Power Plant Feeder Distribution Line Study 2401E001ST, considered five (5) options and reviewed the associated load behaviour over the network including the voltage drop and active power losses.

QEC preferred Option 4 of the original study.

#### **Option 4**

Run two (2) x 25kV feeder circuit lines from the new power plant (with two (2) x 5MVA step-up transformers) to the North Yard location (with two (2) x 5MVA step-down transformers and 5kV switchgear).

- Install two (2) new 4.16/25kV, 5MVA, step-up transformers in the new power plant and connect the primary side of these transformers to the new main 5kV switchgear via cables.
- Install two (2) new 25/4.16kV, 5MVA, step-down transformers and Main-Tie-Main, 5kV, switchgear at the North Yard and connect the primary side of these transformers to the outgoing breaker of the new switchgear.
- Connect the incoming breakers of the new switchgear to the secondary side of the new step-up transformers via new transmission lines.
- Connect the existing community feeders to the 5kV switchgear at the North Yard via transmission lines. The tie-in location of each feeder is as below:
  - For Feeder 1: Pole 50101135
  - For Feeder 2: Pole 50102251
  - For Feeder 3: Pole 50103013
  - For Feeder 4: Pole 50104003

For this option, two operating scenarios are considered:

- All community feeders are fed from one step-up transformer. This is considered the worst-case operating scenario.
- Each two of the community feeders are fed from one step-up transformer. The distribution of the community feeders on each transformer was decided based on the peak demand load of the four feeders such that both transformers are equally loaded.

However further review of this option was required in order to satisfy the original criteria of the study which were:

- Minimize the voltage drop across the lines. The voltage drop should not exceed 3% from the generators to each individual consumer.

- Minimize the network active power losses.

## 1.2 Scope of Work

The previous study showed that Option 4 as originally assessed does not accommodate the load forecast up to the year 2066, and that the off-line tap changers of both step up and step down transformers need to be adjusted to mitigate the voltage drop due to future load increase. Therefore, an alternative approach for voltage drop mitigation was included as part of the scope. The alternative approach involves the use of Automatic Voltage Regulators (AVRs) that are strategically placed at different parts of the network in order to maintain the voltage drop within the  $\pm 3\%$  voltage limits while keeping the network losses at a minimum. In addition, alternatives for tie-in of Feeder 2 were considered.

The estimated electricity production for the years from 2026 to 2066 used in the study is included in Appendix 2.

## 1.3 Tie-In Option

The Option 4 approach for tie-in of the community feeders is detailed below with modifications from the original approach in bold.

- Construct a new power plant at the south-west part of Cambridge Bay community. The new power plant will comprise Five (5) 4.16kV generators, **4.16kV switchgear** and Two (2) 4.16/25kV, 5MVA, step-up transformers.
- Construct a new substation at the North Yard on the north side of Cambridge Bay community. The new substation will comprise **One (1) 25kV switchgear**, Two (2) 25/4.16kV, 5MVA, step-down transformers, and **Two (2) 4.16kV switchgears**.
- Run two (2) x 25kV feeder circuit lines from the new power plant each line will connect the 25kV secondary side of the step-up transformer in the new power plant to the 25kV switchgear in the new substation.
- Connect the primary side of the step-up transformers to the 4.16kV switchgear in the new power plant via cables.
- Connect the 25kV switchgear in the new substation to the primary side of the step-down transformers via cables.
- Connect the secondary side of the step-down transformers in the new substation to the **4.16kV switchgear** via cables.
- Connect the existing community feeders to the new power plant and the new substation as below:
  - Feeder 1: Will be connected to the 4.16kV switchgear in the new substation at Pole 50101135.
  - **Feeder 2: Will be connected to the 4.16kV switchgear in the new power plant at Pole 50102135.**
  - Feeder 3: Will be connected to the 4.16kV switchgear in the new substation at Pole 50103013.
  - Feeder 4: Will be connected to the 4.16kV switchgear in the new substation at Pole 50104003.

Two operating scenarios are considered:

- **Community Feeders 1, 3, and 4 are fed from one step-up transformer. This is considered the worst-case operating scenario.**
- Community Feeders 1 and 4 are fed from one step-up transformer while community Feeder 3 is fed from the other step-up transformer. The distribution of the community feeders on each transformer was decided based on the peak demand load of the three feeders such that both transformers are equally loaded.

The single-line diagram showing the network topology is included under Appendix 1.

## 2. **Discussion**

As with the previous study, the solution discussed in this study uses the following criteria in order to provide recommended optimum locations of AVRs and select a tie-in location for Feeder 2:

- Minimize the voltage drop across the lines. The voltage drop should not exceed 3% from the generators to each individual consumer.
- Minimize the network active power losses.

### 2.1 **Sources of Data**

Network model and simulation parameters are set based on the following inputs:

- **ETAP Model:**  
The ETAP model used is based on the model developed for QEC Penetration Study. The model of the power plant is updated to reflect the topology of the new plant.
- **One-line Diagrams:**  
The Network model is built using the provided one-line diagrams. These diagrams are also used to obtain the connected load and phase connection of each customer.
- **Generation Forecast:**  
QEC provided a table showing the estimated electricity produced over the years from 2026 to 2066 (See Appendix 2). These estimates are used for feeder sizing, voltage drop, and network losses calculations.

### 2.2 **Assumptions**

- The maximum demand factors of each feeder load in 2019 are calculated based on the load data reading provided by QEC. The estimated electricity production for subsequent years (Appendix 2) is used to calculate the maximum demand factor for these years.
- Normally open switches, interconnecting different feeders and used during the failure or maintenance of any of the feeder breakers, are not included in the model and the penetration study except for the options where each two feeders are combined.

- Since the specified AASC cables are not available in the standard ETAP library, AAC cables are used instead. The electrical and geometric characteristics of the selected cable are modified to match the AASC cable specifications provided by QEC.
- The boundary conditions for the voltage limits at all networks nodes (buses) are assumed to be  $\pm 3\%$ .
- The maximum transmission line size to be used is 4/0 AWG with a single conductor per phase.
- QEC advised that most of the loads are non-inductive and that the overall power factor for each feeder is in the order of 0.99. For the purpose of this study, all loads are assumed to have a 0.95 power factor for more conservative values of load currents.
- Based on overhead line conductor parameters provided by QEC, resistance, reactance, and susceptance values for overhead lines are calculated using ETAP considering the following conductor configuration on the pole structure:
  - Conductor height: 34 ft (unless otherwise indicated on the single-line diagrams).
  - Spacing between phases: 2 ft.
- Generator plant service loads are not considered in the analysis.
- Proposed AVR's have voltage adjustment limits of  $\pm 10\%$  with steps of 0.625%. AVR impedances are included in the study based on their assumed values as provided by ETAP software.

## **2.3 Network Configuration**

The new power plant for Cambridge Bay consists of two (2) 1500kW, two (2) 1100kW and one (1) 850kW generators with an output voltage of 4.16kV. Generator outputs are connected to a main 4.16kV switchgear with two (2) bus sections connected together via tie breaker such that one (1) 1500kW and one (1) 1100kW generators are connected to one bus section, and one (1) 1500kW, one (1) 1100kW, and one (1) 850kW generators are connected to the other bus section.

With the exception of Feeder #2, in order to improve customer power supply reliability, feeders are interconnected via a set of normally open switches. Any of these switches may be closed in the case when one of the feeder breakers is out of duty due to failure or for maintenance purposes. Since the case where both feeders are connected to one feeder breaker does not represent normal network operation and is used only for maintenance purposes, these configurations are not included in the model except where two feeders are combined into one feeder. For this case, only the tie switch is considered closed.

The network ETAP model is provided in Appendix 1.

## **2.4 Calculation Procedures**

### **2.4.1 Load Parameters Calculations**

The peak demand load for the year 2019 is obtained from the metering readings provided by QEC for this year and is used to calculate the maximum demand factor for the loads of each feeder as shown in Table 1.

**Table 1: Maximum Demand (2019)**

	Connected Load (kVA)	Max. Demand Load (kVA)	Max. Demand Factor (%)
Feeder 1	2537.5	989.625	39.00%
Feeder 2	3017.5	754.375	25.00%
Feeder 3	642.5	334.1	52.00%
Feeder 4	450	234	52.00%
<b>Total</b>	6647.5	2312.1	

The estimated electricity production (Appendix 2) is used to calculate the percentage growth of electricity demand which is, in turn, used to calculate the maximum demand for the successive years as shown in Table 2.

**Table 2: Estimated Growth in Demand Load**

Year	Population Demand Load Change (%)	Maximum Demand Factors			
		Feeder 1	Feeder 2	Feeder 3	Feeder 4
2019	-	39.00%	25.00%	52.00%	52.00%
2026	55.00%	60.45%	38.75%	80.60%	80.60%
2027	57.00%	61.23%	39.25%	81.64%	81.64%
2028	58.00%	61.62%	39.50%	82.16%	82.16%
2029	59.00%	62.01%	39.75%	82.68%	82.68%
2030	61.00%	62.79%	40.25%	83.72%	83.72%
2031	62.00%	63.18%	40.50%	84.24%	84.24%
2032	64.00%	63.96%	41.00%	85.28%	85.28%
2033	65.00%	64.35%	41.25%	85.80%	85.80%
2034	66.00%	64.74%	41.50%	86.32%	86.32%
2035	68.00%	65.52%	42.00%	87.36%	87.36%
2036	70.00%	66.30%	42.50%	88.40%	88.40%
2041	78.00%	69.42%	44.50%	92.56%	92.56%
2046	87.00%	72.93%	46.75%	97.24%	97.24%
2051	98.00%	77.22%	49.50%	102.96%	102.96%
2056	110.00%	81.90%	52.50%	109.20%	109.20%
2061	123.00%	86.97%	55.75%	115.96%	115.96%
2066	138.00%	92.82%	59.50%	123.76%	123.76%

As agreed with QEC, the study considers the load demand of the first 10 years (2026 to 2036) in one-year steps, and the following 30 years (2037 to 2066) in 5-year steps.

The above demand factors are used in the ETAP model.

The maximum demand load analysis of the four feeders based on the table above shows that:

- The maximum generation capacity for each bus section of the switchgear is 2500 kW. The peak demand load forecast for all the years exceeds 2500kW. Therefore, the switchgear bus-tie breaker needs to be closed such that the total load can be distributed among all the generators.
- Customer transformers connected to Feeders 3 and 4 need to be upgraded to 125% of their current ratings to accommodate the forecasted demand.

#### **2.4.2 Design Constraints**

The following design constraint are established by QEC:

- The total voltage drop from the generators to each customer load shall not exceed 3%.
- The maximum size of a transmission line is 4/0AWG with no more than one conductor per phase.
- Initial calculations are made with all transformer taps set at the zero-position. Voltage drop compensation is achieved using AVRs.

### **2.5 Results**

Electricity production estimate for the years from 2026 to 2066 is used to calculate the demand load and demand factor for each feeder. These demand factors were applied to calculate the minimum feeder size that is required to achieve maximum voltage drop of 3% at the customer transformer using the tie-in option detailed under Section 1.3.

An iterative method is used to find the optimum connection locations for the AVR. The objective constraints used in this method is to:

- 1) Maintain the voltages at different poles within the  $\pm 3\%$  voltage drop limits.
- 2) Minimize the active power losses in the network.
- 3) Minimize the number of AVRs to be used.

The results of this iterative method show that the AVR are best located near the heaviest loaded lines.

The study concludes that the tie-in configuration discussed in this study will provide the required energy to the community feeders up to the forecasted load for the year 2066 when using AVRs strategically located at different points of the network to compensate for potential voltage drops and to minimize network losses.



**Table 3: Study Results Summary**

			Operating Scenario		Remarks
			A	B	
Main Power Plant	Min. Main Feeder Line Size		4/0 AWG	1/0 AWG	
	AVR Tap Setting	AVR-T-F1_4-1	-5%	-2.5%	
		AVR-T-F2_3-1	-5%	-2.5%	
Feeder 1	Min. Main Feeder Line Size		2/0 AWG	1/0 AWG	
	AVR Tap Setting	AVR-50101135	-6.25%	-5.625%	
		AVR-50101225	-3.75%	-3.75%	
Feeder 2	Min. Main Feeder Line Size		1/0 AWG	1/0 AWG	
	AVR Tap Setting AVR-50102135		-3.75%	-3.75%	
Feeder 3	Min. Main Feeder Line Size		3/0 AWG	1/0 AWG	
	AVR Tap Setting AVR-50103013		-7.5%	-7.5%	
Feeder 4	Min. Main Feeder Line Size		4/0 AWG	4/0 AWG	
	AVR Tap Setting AVR-50104003		-4.375%	-3.75%	

Scenario A: Feeders 1, 3, and 4 are fed from one North Yard Switchgear incomer.

Scenario B: Feeders 1, 3, and 4 are fed from both North Yard Switchgear incomers.

Table 4: Study Results Details

Year	Operating Scenario	Main Power Plant			Feeder 1			Feeder 2		Feeder 3		Feeder 4	
		Min. Main Feeder Line Size	AVR Tap Setting		Min. Main Feeder Line Size	AVR Tap Setting		Min. Main Feeder Line Size	AVR Tap Setting	Min. Main Feeder Line Size	AVR Tap Setting	Min. Main Feeder Line Size	AVR Tap Setting
			AVR-T-F1_4-1	AVR-T-F2_3-1		AVR-50101135	AVR-50101225		AVR-50102135		AVR-50103013		AVR-50104003
2026	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.25%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.25%
2027	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.25%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.25%
2028	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.25%
2029	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.25%
2030	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.25%
2031	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-5%	4/0 AWG	-1.875%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.875%
2032	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-5%	4/0 AWG	-1.875%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.75%	4/0 AWG	-1.875%
2033	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-5%	4/0 AWG	-2.5%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.75%	4/0 AWG	-1.875%
2034	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-5%	4/0 AWG	-2.5%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.75%	4/0 AWG	-1.875%
2035	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-5%	4/0 AWG	-2.5%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.75%	4/0 AWG	-1.875%
2036	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-5.625%	4/0 AWG	-2.5%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.75%	4/0 AWG	-1.875%
2041	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-4.375%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-6.25%	4/0 AWG	-3.125%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%

Year	Operating Scenario	Main Power Plant			Feeder 1			Feeder 2		Feeder 3		Feeder 4	
		Min. Main Feeder Line Size	AVR Tap Setting		Min. Main Feeder Line Size	AVR Tap Setting		Min. Main Feeder Line Size	AVR Tap Setting	Min. Main Feeder Line Size	AVR Tap Setting	Min. Main Feeder Line Size	AVR Tap Setting
			AVR-T-F1_4-1	AVR-T-F2_3-1		AVR-50101135	AVR-50101225				AVR-50103013		AVR-50104003
2046	A	1/0 AWG	-4.375%	-4.375%	1/0 AWG	-4.375%	-2.5%	1/0 AWG	-2.5%	1/0 AWG	-6.25%	4/0 AWG	-3.125%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-3.125%	1/0 AWG	-2.5%	1/0 AWG	-5%	4/0 AWG	-1.875%
2051	A	1/0 AWG	-4.375%	-4.375%	1/0 AWG	-5%	-3.125%	1/0 AWG	-2.5%	1/0 AWG	-6.875%	4/0 AWG	-3.125%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.75%	-3.125%	1/0 AWG	-2.5%	1/0 AWG	-5%	4/0 AWG	-2.5%
2056	A	3/0 AWG	-4.375%	-4.375%	1/0 AWG	-5%	-3.75%	1/0 AWG	-3.125%	1/0 AWG	-7.5%	4/0 AWG	-3.75%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-5%	-3.125%	1/0 AWG	-3.125%	1/0 AWG	-6.25%	4/0 AWG	-3.125%
2061	A	3/0 AWG	-5%	-5%	1/0 AWG	-5%	-3.75%	1/0 AWG	-3.125%	1/0 AWG	-7.5%	4/0 AWG	-3.75%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-5%	-3.125%	1/0 AWG	-3.125%	1/0 AWG	-6.875%	4/0 AWG	-3.125%
2066	A	4/0 AWG	-5%	-5%	2/0 AWG	-6.25%	-3.75%	1/0 AWG	-3.75%	3/0 AWG	-7.5%	4/0 AWG	-4.375%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-5.625%	-3.75%	1/0 AWG	-3.75%	1/0 AWG	-7.5%	4/0 AWG	-3.75%

Scenario A: Feeders 1, 3, and 4 are fed from one North Yard Switchgear incomer.  
Scenario B: Feeders 1, 3, and 4 are fed from both North Yard Switchgear incomers.

### **3. Conclusion and Recommendations**

The tie-in configuration discussed in this study will provide the required energy to the community feeders up to the forecasted load for the year 2066 when using AVRs strategically located at different points of the network to compensate for potential voltage drops and to minimize network losses.

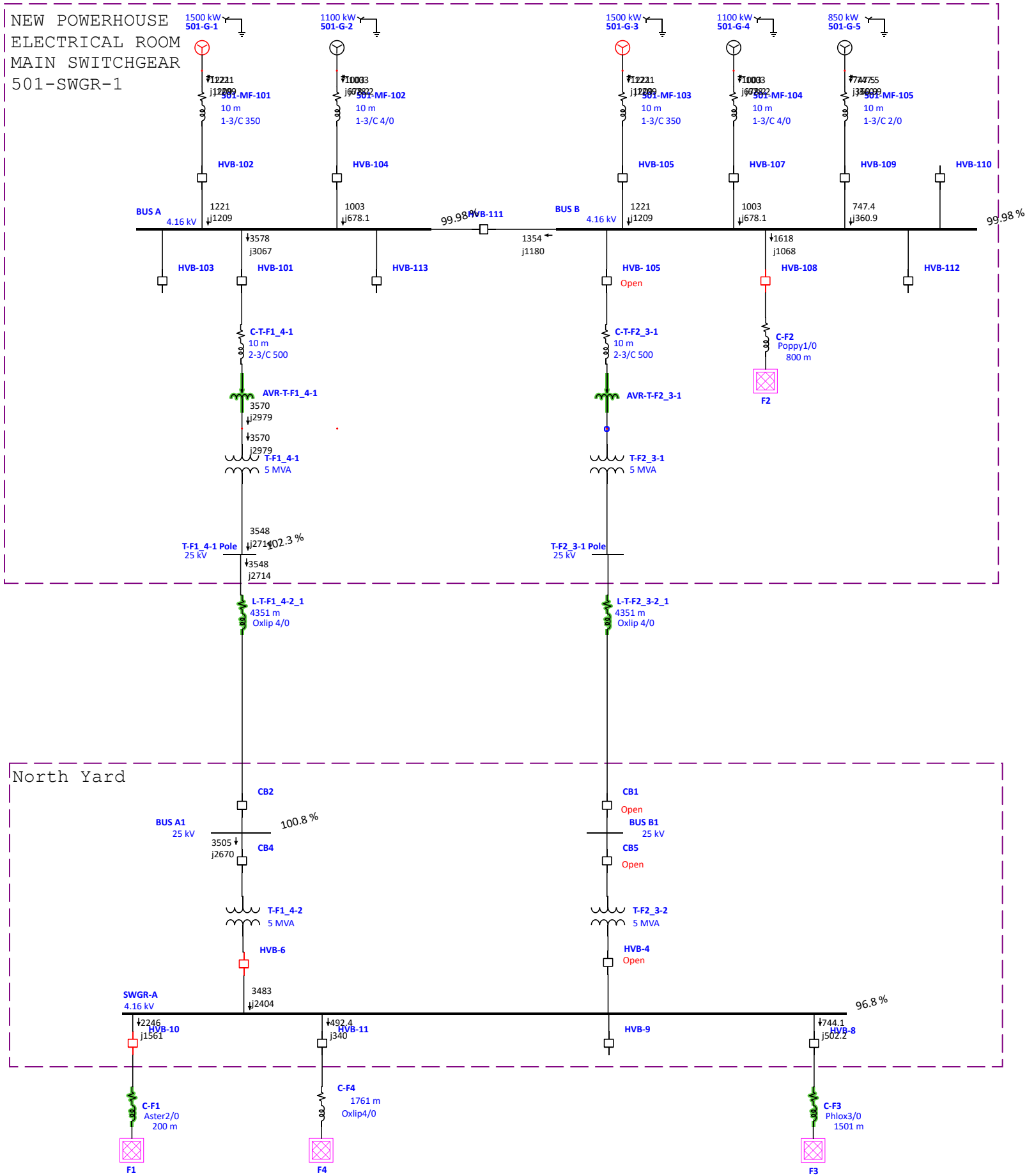
The current study considers that Feeder 2 is connected to the new power plant at Pole 50102135 which is the closest pole with three-phase lines. An alternative recommendation would be to connect Feeder 2 to the new power plant at Pole 50102268 which is closer to the power plant and replace the single-phase transmission lines between Poles 50102268 and 50102135 with three-phase. Although this option involves additional transmission lines, it would eliminate the need for an AVR for Feeder 2.

The study can be revisited upon the final selection of the AVRs to verify their connection locations based on their tap setting range and impedances.

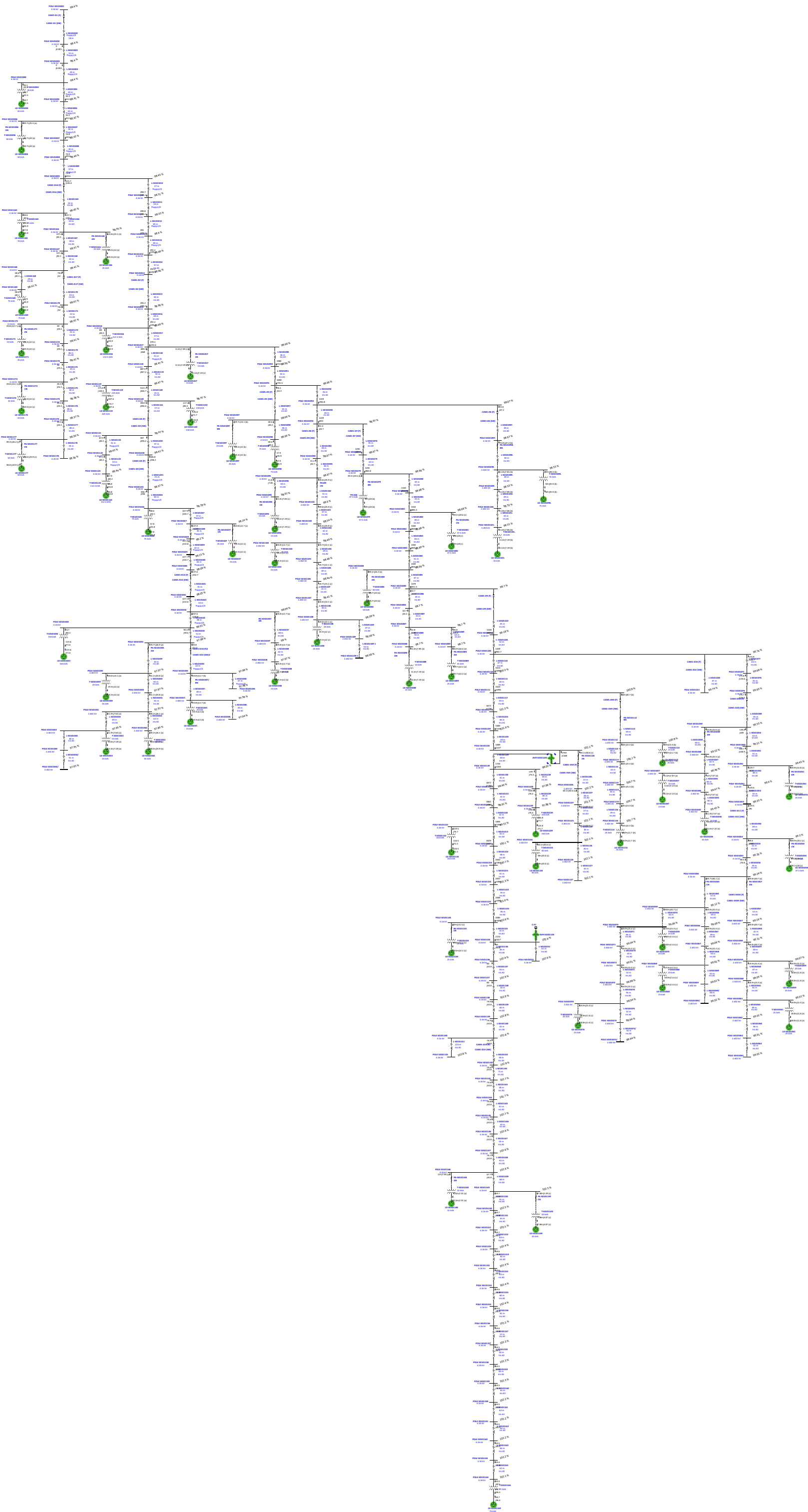
Engineering Study – Final Report  
Feeder Distribution Line Study  
Cambridge Bay North Yard Substation  
Rev A

## **Appendix 1**

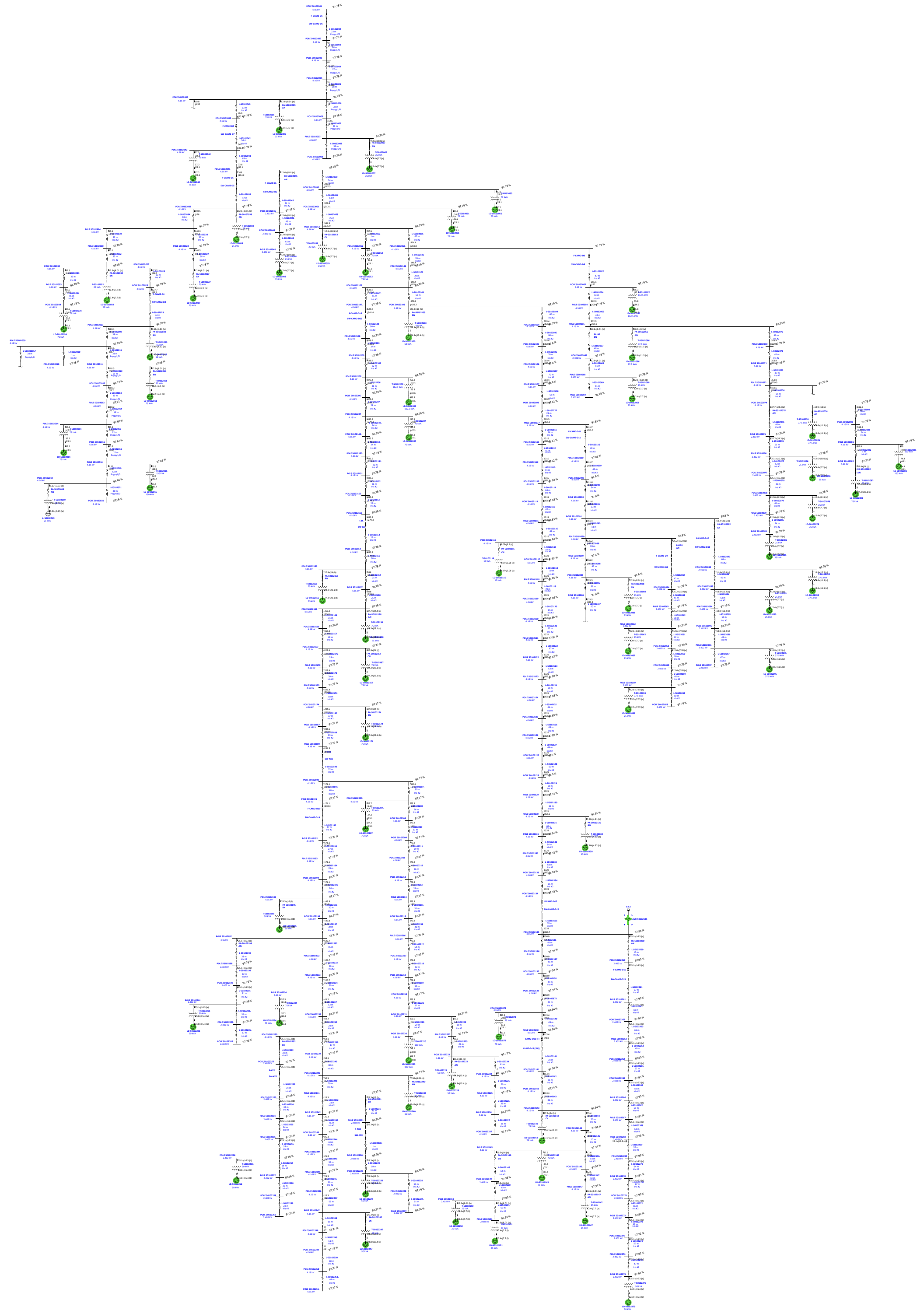
### **Cambridge Bay Network ETAP Model and Results**



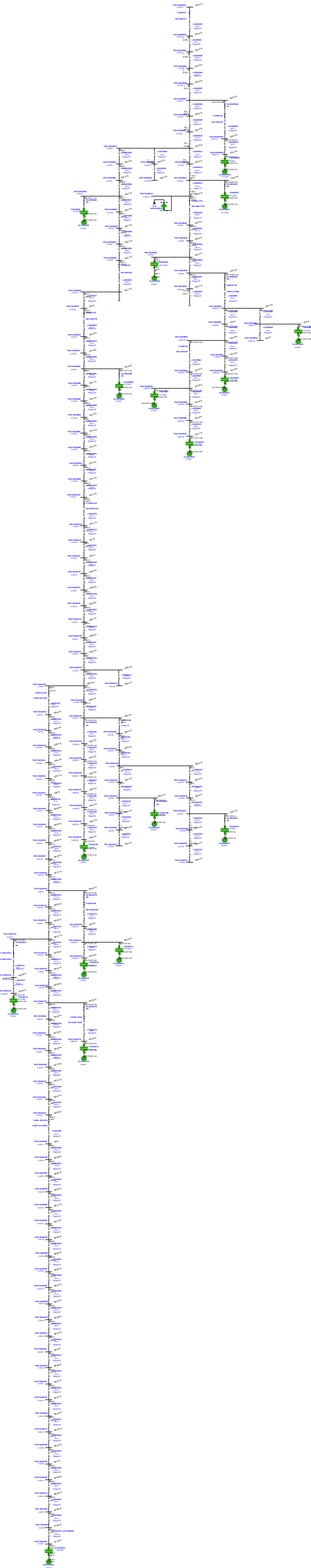
# One-Line Diagram - OLV1->F1 | Load Flow Analysis | LF

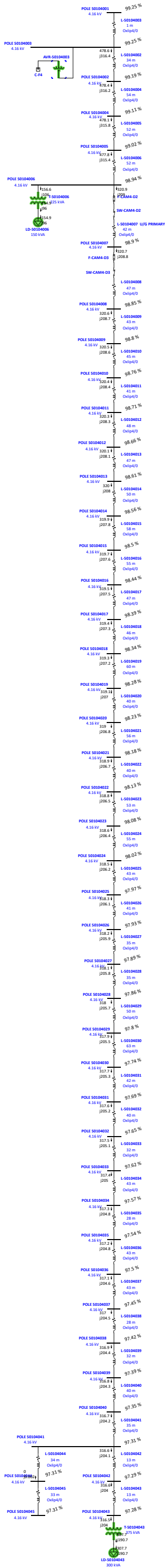


# One-Line Diagram - OLV1->F2 | Load Flow Analysis | LF









## **Appendix 2**

### **Cambridge Bay – Estimated Electricity Production**



## Appendix C: Calculated power plant electricity generation after 2026

**Estimated yearly electricity production for the new Cambridge Bay power plant**

Year	Population	Population change	Estimated electricity produced (kWh/year)
2026	2,451	+55	15,407,427
2027	2,507	+57	15,763,605
2028	2,565	+58	16,128,017
2029	2,625	+59	16,500,853
2030	2,685	+61	16,882,308
2031	2,747	+62	17,272,581
2032	2,811	+64	17,671,877
2033	2,876	+65	18,080,403
2034	2,942	+66	18,498,373
2035	3,010	+68	18,926,005
2036	3,080	+70	19,363,523
2037	3,151	+71	19,811,155
2038	3,224	+73	20,269,136
2039	3,298	+75	20,737,703
2040	3,375	+76	21,217,103
2041	3,453	+78	21,707,585
2042	3,532	+80	22,209,405
2043	3,614	+82	22,722,827
2044	3,698	+84	23,248,117
2045	3,783	+85	23,785,550
2046	3,871	+87	24,335,408
2047	3,960	+89	24,897,977
2048	4,052	+92	25,473,551
2049	4,145	+94	26,062,430
2050	4,241	+96	26,664,923
2051	4,339	+98	27,281,344
2052	4,439	+100	27,912,015
2053	4,542	+103	28,557,265
2054	4,647	+105	29,217,432
2055	4,755	+107	29,892,860
2056	4,864	+110	30,583,902
2057	4,977	+112	31,290,919
2058	5,092	+115	32,014,280
2059	5,210	+118	32,754,364
2060	5,330	+120	33,511,556
2061	5,453	+123	34,286,252
2062	5,579	+126	35,078,858
2063	5,708	+129	35,889,786
2064	5,840	+132	36,719,461
2065	5,975	+135	37,568,315
2066	6,113	+138	38,436,793