

Qulliq Energy Corporation



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Qulliq Energy Corporation
Société d'énergie Qulliq
Qulliq Alruyaktutnik Ikumatjutiit

Application for Major Project Permits

MAJOR PROJECT FOR
CAMBRIDGE BAY DISTRIBUTION SYSTEM UPGRADE

February 2026



1 Executive Summary

2 Qulliq Energy Corporation (QEC) hereby applies to the Minister Responsible for Qulliq
3 Energy Corporation pursuant to section 18.1 of the *Qulliq Energy Corporation Act*,
4 R.S.N.W.T. 1988, c.N-2 for a major project permit to upgrade the feeder distribution system
5 interconnecting the new power plant to the community of Cambridge Bay.

6 QEC is in the process of building a new power plant in Cambridge Bay with the approval of
7 a major project permit (MPP) by the Minister responsible for QEC in August 2021 replacing
8 the existing power plant which was constructed in 1958. The plant is expected to come in-
9 service in 2029.

10 The current Cambridge Bay distribution system is fed from the existing generation plant
11 that consists of three 1100kW and one 550kW generators with an output voltage of 4.16kV.
12 All generators are connected to a common switchgear bus and are used to provide power
13 to four community feeders. The switchgear is also used to provide power to other service
14 loads. In order to improve customer power supply reliability, feeders are interconnected via
15 a set of normally open switches. Any of these switches may be closed in the case when
16 one of the feeder breakers is out of duty due to failure or maintenance purposes.

17 In the 2021 MPP application, QEC discussed that a single supply line without any
18 alternative means of transmission would create a high risk of power interruption to the
19 community, especially in areas with high winds and extreme cold temperatures.
20 Accordingly, the new power plant construction scope included installation of a second line
21 that increases reliability of the power supply and provides an alternative for electricity
22 transmission from the plant to the community.

23 The proposed distribution upgrade will interconnect the new power plant to the existing
24 community feeders via the new distribution line. The project scope has been developed
25 with consideration of future load growth and meeting other system requirements in the
26 community and includes the following:

- Install 4.16 kV switchgear and two 4.16/25 kV, 5 MVA, step-up transformers in the new power plant
- Construct a new substation at the North yard on the north side of Cambridge Bay comprising of one 25 kV switchgear, two 25/4.16 kV 5 MVA step-down transformers, and one 4.16KV switchgears. Existing two 25/4.16 kV 5 MVA step-down transformers from the existing power plant location shall to relocated and re-used at this new substation.
- Run two 4/0 3-phase overhead feeder lines at 25KV from the new power plant on different pole lines, interconnecting closer to town to the new substation at the North Yard on the northside of Cambridge Bay.



- 1 • Connect the existing town distribution feeders to the new power plant and substations
2 per below:
 - 3 ○ Feeder 1: Will be connected to the 4.16kV switchgear in the new substation
4 using approximately 130m of underground cables
 - 5 ○ Feeder 2: Will be connected to the 4.16kV switchgear in the new power plant
6 using approximately 60m of underground cables
 - 7 ○ Feeder 3: Will be connected to the 4.16kV switchgear in the new substation
8 using approximately 650m of overhead lines
 - 9 ○ Feeder 4: Will be connected to the 4.16kV switchgear in the new substation
10 using approximately 1300m of overhead lines
- 11 • Perform load switching to balance loads around the feeders.

12 QEC's estimated cost to complete this project is \$11.6 million. This would result in an
13 estimated 0.46 cents/kWh increase in revenue requirement by the time the project is fully
14 in service. The project will have no impact on rates until the time of QEC's first General
15 Rate Application following the project in-service date.

16 The project is anticipated to be completed by the 2029/30 fiscal year.



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1 1.0 Application

2 Qulliq Energy Corporation (QEC) hereby applies to the Minister Responsible for Qulliq
3 Energy Corporation pursuant to Section 18.1 of the *Qulliq Energy Corporation Act*,
4 R.S.N.W.T. 1988, cN-2 for a major project permit to upgrade the feeder distribution system
5 interconnecting the new power plant to the community of Cambridge Bay. QEC is
6 requesting permission to proceed with this project. Details in support of the requested
7 project permit are set out below.

8 2.0 Background

9 2.1 Project Background

10 Cambridge Bay is a hamlet located on Victoria Island in the Kitikmeot Region of Nunavut.
11 The community had a population of 1,760 in the 2021 census. Access is mainly by air
12 through the Cambridge Bay Airport and by sealift during the summer shipping season.

13 The location of the community is shown in Figure 2.1.

Figure 2.1 – Cambridge Bay Location



15
16 QEC is in the process of building a new power plant in Cambridge Bay, which was granted
17 a major project permit by the Minister responsible for QEC in August 2021, replacing the
18 existing power plant which was constructed in 1958. The plant is expected to come in-
19 service in 2029.



1 The current Cambridge Bay distribution system is fed from the existing generation plant
2 that consists of three 1100 kW and one 550 kW generators with an output voltage of
3 4.16kV. All generators are connected to a common switchgear bus and are used to provide
4 power to four community feeders. The switchgear is also used to provide power to other
5 service loads. In order to improve customer power supply reliability, feeders are
6 interconnected via a set of normally open switches. Any of these switches may be closed
7 in the case when one of the feeder breakers is out of duty due to failure or maintenance
8 purposes.

9 In the 2021 MPP application, QEC discussed that a single supply line without any
10 alternative means of transmission would create a high risk of power interruption to the
11 community, especially in areas with high winds and extreme cold temperatures.
12 Accordingly, the new power plant construction scope included installation of a second line
13 that increases reliability of the power supply and provides an alternative for electricity
14 transmission from the plant to the community.

15 In 2024, QEC engaged an independent engineering consulting company (Asher
16 Engineering) to undertake a review of options to interconnect the new power plant to the
17 existing community feeders via the new distribution line.

18 3.0 Assessment of Project Options

19 In accordance with QEC's request, the consultant performed technical analysis of various
20 tie-in options of the new power plant to the existing community feeders, including:

- **Option 1:** Run two 5 kV feeder circuit lines from the new power plant to the existing distribution system. Tie in to the nearest feeder point and reduce the four feeders to two feeders within the existing distribution system.
- **Option 2:** The four existing community feeders are connected to the new power plant via new 5 kV transmission lines, which includes changing all the single-phase power lines between Feeder 2 poles to be three-phase.
- **Option 3:** Run two 25 kV feeder circuit lines from the new power plant (with two 5 MVA step-up transformers) to the existing distribution system (with two 5 MVA step-down transformers).
- **Option 4:** Run two 25 kV feeder circuit lines from the new power plant (with two 5 MVA step-up transformers) to the North Yard location (with two 5 MVA step-down transformers and 5 kV switchgear).
- **Option 5:** Upgrade all customers' transformers to have 25 kV primary voltage.

34 Since the new power plant is located in a considerably remote location that is far from the
35 existing power plant location, the analysis of options focused on optimizing the following
36 criteria:



- Minimizing the voltage drop across the lines. The voltage drop should not exceed 3% from the generators to each individual consumer.
- Minimizing the network active power losses.

Network model and simulation parameters were set based on the following inputs:

- **Electrical Transient Analyzer Program (ETAP) Model:** The ETAP model used was based on the model developed by Asher Engineering for the QEC Penetration Study. The model of the power plant was updated to reflect the topology of the new plant.
- **One-line Diagrams:** The network model was built using the one-line diagrams provided by QEC, which were also used to obtain the connected load and phase connection of each customer.
- **Generation Forecast:** Generation estimates for 2026-2066 period were used for feeder sizing, voltage drop, and network losses calculations.

The study used generation forecast for the years from 2026 to 2066 to calculate the demand load and demand factor for each feeder. These demand factors were applied to calculate the minimum feeder size that is required to achieve a maximum voltage drop of 3% at the customer transformer under each option.

The initial study by Asher Engineering, included in Appendix A, concluded that the option 4 preferred by QEC as presented did not accommodate the load forecast up to the year 2066, and that the off-line tap changers of both step up and step down transformers needed to be adjusted to mitigate the voltage drop due to future load increase.

Upon reviewing the initial study by Asher Engineering, QEC requested the consultant to investigate the feasibility to implement an alternative approach for voltage drop mitigation. The alternative approach involves the use of Automatic Voltage Regulators (AVRs) that are strategically placed at different parts of the network in order to maintain the voltage drop within the $\pm 3\%$ voltage limits while keeping the network losses at a minimum. In addition, alternatives for tie-in of Feeder 2 were considered. The alternative approach study is included in Appendix B.

The proposed distribution upgrade project will interconnect the new power plant to the existing community feeders via the new distribution line. The project scope has been developed with consideration of future load growth and meeting other system requirements in the community and includes the following:

- Install 4.16 kV switchgear and two 4.16/25 kV, 5 MVA, step-up transformers in the new power plant
- Construct a new substation at the North yard on the north side of Cambridge Bay comprising of one 25 kV switchgear, two 25/4.16 kV 5 MVA step-down transformers, and one 4.16KV switchgears. Existing two 25/4.16 kV 5 MVA step-down



transformers from the existing power plant location shall be relocated and re-used at this new substation.

- Run two 4/0 3-phase overhead feeder lines at 25KV from the new power plant on different pole lines, interconnecting closer to town to the new substation at the North Yard on the northside of Cambridge Bay.
- Connect the existing town distribution feeders to the new power plant and substations per below:
 - Feeder 1: Will be connected to the 4.16kV switchgear in the new substation using approximately 130m of underground cables
 - Feeder 2: Will be connected to the 4.16kV switchgear in the new power plant using approximately 60m of underground cables
 - Feeder 3: Will be connected to the 4.16kV switchgear in the new substation using approximately 650m of overhead lines
 - Feeder 4: Will be connected to the 4.16kV switchgear in the new substation using approximately 1300m of overhead lines
- Perform load switching to balance loads around the feeders.

The estimated cost to complete this project is \$11.567 million. The project is anticipated to be completed by the 2029/30 fiscal year.

4.0 Impact of the Project on Ratepayers

QEC conducted an analysis of the impact of the project on ratepayers. It should be noted that the project will have no impact on rates until the time of QEC's General Rate Application following the project coming in-service. QEC conducted the rate impact analysis based on a territorial rate design assuming the project is completed by the 2029/30 fiscal year.

The rate impact analysis is based on QEC's estimated cost for this project of \$11.567 million.

Table 4.1 summarizes the estimated incremental revenue requirement increase due to the project of \$11.567 million. The estimated rate increase under territory-wide rates is 0.46 cents/kWh.



1 **Table 4.1 Distribution Line Upgrade Project Estimated Rate Impact**

Project Characteristics	
Capital Cost (\$000)	11,567
Amortization Period (year)	45
2025/26 GRA Approved Return on Ratebase	5.95%
<u>Revenue Requirement Impacts</u>	
Amortization Expense (\$000)	257
Return on Ratebase (\$000)	689
sub-total: Revenue Requirement Increase (\$000)	946
Total Revenue Requirement Impact (\$000)	946
2029/30 Forecast Sales (MWh)	204,578
Average Territorial Rate Increase (c/kWh)	0.46

2
3 It is important to note that this analysis has been provided for illustrative purposes only.
4 Actual rate impacts will depend on the overall revenue requirements and rate designs
5 approved in subsequent General Rate Applications.

6 **5.0 Grounds in Support of the Application**

7 The implementation of the proposed project is very important to QEC's customers. The
8 project will provide a stable, cost effective, safe, and reliable service to the community of
9 Cambridge Bay and support the new power plant operation.
10 Power is an essential service in Nunavut, and QEC must plan to be able to deliver reliable
11 electricity.

12 **6.0 Project Timelines**

13 Based on QEC's experience with procurement, delivery of materials and construction
14 windows, this project is anticipated to be completed by the 2029/30 fiscal year.

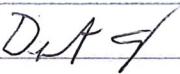
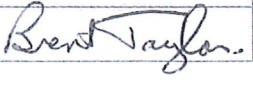


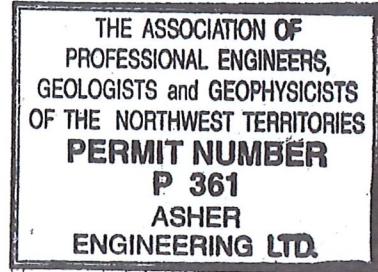
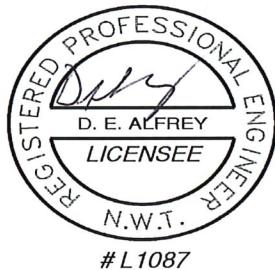
Engineering Study

Final Report

Title	Cambridge Bay Power Plant Feeder Distribution Line Studies
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Executor	Ahmed Abdelfattah, P.Eng.
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November 8, 2024

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The results presented in the report are at a conceptual level; no detailed engineering has yet been performed, nor has equipment been selected or an operational plan been defined.

Use of this Document acknowledges acceptance of the foregoing conditions.

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Appendix 2	Cambridge Bay – Estimated Electricity Production

Executive Summary

Qulliq Energy Corporation (QEC) currently delivers electricity to approximately 15,000 customers in 25 communities across Nunavut using 25 standalone diesel power plants with total installed capacity of 76MW. Each community has its own independent generation and distribution system that does not have any backup from the utility grid.

QEC is planning to de-commission the existing Cambridge Bay Community power plant and build a new power plant on the south-west side of the community to provide sufficient energy to this community. Due to the remote location of the new power plant, different approaches for connecting the existing community feeders to the new power plant need to be studied.

QEC proposes five (5) options to tie-in the new power plant to the existing community feeders. Additionally, Asher has proposed rearrangements for some of these options to improve the voltage drop. These options are summarized as below:

Option 1 involves the following:

- Feeders 1 and 4 and Feeders 2 and 3 are combined into two (2) feeders.
- Two (2) new 5kV power lines are installed from the new power plant to these two feeders to tie in at the nearest locations for Feeders 1 and 2.

Option 2 involves the following:

- The four existing community feeders are connected to the new power plant using new 5kV power lines to tie in at the nearest location for each feeder.

Option 3 involves the following:

- Two (2) 4.16/25kV, 5MVA, step-up transformers are installed at the new power plant and connected via cables to the new generator distribution switchgear.
- Two (2) 25/4.16kV, 5MVA, step-down transformers with Main-Tie-Main, 5kV, switchgear are installed at the existing power plant and connected to the step-up transformers via two (2) 25kV power lines.
- The 5kV switchgear at the existing power plant is connected via four (4) new 5kV power lines to tie in at the nearest locations to the existing community feeders such that two feeders are connected to each switchgear section.

Option 3A, proposed by Asher, is similar to QEC Option 3 except that feeders are redistributed with one feeder connected to one switchgear section, while the other three feeders are connected to the other switchgear section.

Option 3B, proposed by Asher, is an alternative approach for using Option 3 where Feeder 2 is connected directly to the new switchgear in the new power plant.

Option 4 involves the following:

- Two (2) 4.16/25kV, 5MVA, step-up transformers are installed at the new power plant and connected via cables to the new generator distribution switchgear.

- Two (2) 25/4.16kV, 5MVA, step-down transformers with Main-Tie-Main, 5kV, switchgear are installed at the North Yard and connected to the step-up transformers via two (2) 25kV power lines.
- The 5kV switchgear at the North Yard is connected via four (4) new 5kV power lines to tie in at the nearest locations the existing community feeders.

Option 5 involves the following:

- Two (2) 4.16/25kV, 5MVA, step-up transformers are installed at the new power plant and connected via cables to the new generator distribution switchgear.
- Upgrade all existing community transformers to have 25kV primary voltage.
- Feeders 1 and 3 and Feeders 2 and 4 are combined into two (2) feeders and connected to the step-up transformers, via an intermediate Main-Tie-Main switchgear, at the nearest location.

The above options are discussed in detail in Section 1.3. The single-line diagrams showing the network topology for each option are included in Appendices 1.A to 1.G.

The scope of the study is to calculate the maximum voltage drop and network active power losses for each community feeder, considering each of the tie-in options and provide the option that will offer the minimum voltage drop and network losses. Additionally, the study will recommend the minimum feeders sizes required to tie-in the new power plant to the existing feeders under each option in order to achieve a maximum voltage drop of 3%.

The study considers the estimated electricity production for the years from 2026 to 2066 as shown in Appendix 2.

Recommendations provided by this study consider technical aspects only. Construction cost estimates associated with each option are presented in a separate report.

Table 3 summarizes the study results.

Table 3: Study Results Summary

Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks		
		Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers			
1		Failed									
2		Failed									
3	A	Failed									
	B	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%			
3A	A	Failed									
	B	1/0 AWG	3/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%			
3B	A	2/0 AWG	1/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%			
	B	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%			
4	A	Failed									
	B	Failed									
5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-5%	N/A			
	B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A			

Scenario A: All feeders are fed from one step-up transformer

Scenario B: Feeders are distributed across both step-up transformers

1. Introduction

1.1 Background

Qulliq Energy Corporation (QEC) currently delivers electricity to approximately 15,000 customers in 25 communities across Nunavut using 25 standalone diesel power plants with total installed capacity of 76MW. Each community has its own independent generation and distribution system that does not have any backup from the utility grid.

QEC is planning to de-commission the existing Cambridge Bay Community power plant and build a new power plant on the south-west side of the community to provide sufficient energy to this community. Due to the remote location of the new power plant, different approaches for connecting the existing community feeders to the new power plant need to be studied.

1.2 Scope of Work

The estimated electricity production for the years from 2026 to 2066, shown in Appendix 2, is used to calculate the maximum voltage drop and network active power losses for each community feeder, when each of the tie-in options is utilized and provide the option that will offer the minimum voltage drop and network losses. Additionally, the study will recommend the minimum feeders sizes required to tie-in the new power plant to the existing feeders under each option in order to achieve a maximum voltage drop of 3%.

1.3 Tie-In Options

In order to connect the new power plant to the existing community feeders, QEC proposed five (5) options to be considered. Additionally, upon further study of the load behavior when connected to the network, Asher proposed two alternative implementations of Option 3. The different options are detailed below.

1.3.1 Option 1

Run two (2) x 5kV feeder circuit lines from the new power plant to the existing distribution system. Tie in to the nearest feeder point and reduce the four (4) feeders to two (2) feeders within the existing distribution system.

- Feeders 1 and 4 are combined into one feeder by connecting the lines at Poles 50101001 in Feeder 1 and 50104002 in Feeder 4.
- Feeders 2 and 3 are combined into one feeder by connecting the lines at Pole 50102008.
- Connect the new combined feeders to the main 4.16kV switchgear at the new power plant using a new 5kV transmission line.

The nearest tie-in location is at Pole 50104003 in Feeder 4 and Pole 50102268 in Feeder 2. This will require changing all the single-phase power lines between Poles 50102268 and 50102135 to be three-phase.

1.3.2 Option 2

The four (4) existing community feeders are connected to the new power plant via new 5kV transmission lines. The tie-in location for each feeder is as below:

- For Feeder 1: Pole 50101001.
- For Feeder 2: Pole 50102268. This will require changing all the single-phase power lines between Poles 50102268 and 50102135 to be three-phase.
- For Feeder 3: Pole 50103001.
- For Feeder 4: Pole 50104003.

1.3.3 Option 3

Run two (2) x 25kV feeder circuit lines from the new power plant (with two (2) x 5MVA step-up transformers) to the existing distribution system (with two (2) x 5MVA step-down transformers).

- Install two (2) new 4.16/25kV, 5MVA, step-up transformers in the new power plant and connect the primary side of these transformers to the new main 5kV switchgear via cables.
- Install two (2) new 25/4.16kV, 5MVA, step-down transformers and Main-Tie-Main, 5kV, switchgear at the existing power plant and connect the primary side of these transformers to the outgoing breaker of the new switchgear.
- Connect the incoming breakers of the new switchgear to the secondary side of the new step-up transformers via new transmission lines.
- Connect the existing community feeders to the existing 5kV switchgear at the existing power plant using new 5kV transmission lines. The nearest tie-in location for each feeder is as below:
 - For Feeder 1: Pole 50101001
 - For Feeder 2: Pole 50102001
 - For Feeder 3: Pole 50103001
 - For Feeder 4: Pole 50104001

For this option, two operating scenarios are considered:

- All community feeders are fed from one step-up transformer. This is considered the worst-case operating scenario.
- Each two of the community feeders are fed from one step-up transformer. The distribution of the community feeders on each transformer was decided based on the peak demand load of the four feeders such that both transformers are equally loaded.

1.3.4 Option 3A

The study of the voltage drop using Option 3 showed that Feeder 1 experiences the highest voltage drop among the other feeders. Therefore, this option suggests rearranging the feeders so that Feeder 1 is connected alone to one step-down transformer, while the other three feeders are connected to the other step-down transformer.

1.3.5 Option 3B

The study of the voltage drop using various options showed that Feeder 2 has the least voltage drop among other feeders and it can be connected directly to the 5kV switchgear without violating

the voltage drop limits.

In this option, Feeder 2 is connected directly to the new switchgear in the new power plant in order to reduce the load on the transformers.

1.3.6 Option 4

Run two (2) x 25kV feeder circuit lines from the new power plant (with two (2) x 5MVA step-up transformers) to the North Yard location (with two (2) x 5MVA step-down transformers and 5kV switchgear).

- Install two (2) new 4.16/25kV, 5MVA, step-up transformers in the new power plant and connect the primary side of these transformers to the new main 5kV switchgear via cables.
- Install two (2) new 25/4.16kV, 5MVA, step-down transformers and Main-Tie-Main, 5kV, switchgear at the North Yard and connect the primary side of these transformers to the outgoing breaker of the new switchgear.
- Connect the incoming breakers of the new switchgear to the secondary side of the new step-up transformers via new transmission lines.
- Connect the existing community feeders to the 5kV switchgear at the North Yard via transmission lines. The tie-in location of each feeder is as below:
 - For Feeder 1: Pole 50101135
 - For Feeder 2: Pole 50102251
 - For Feeder 3: Pole 50103013
 - For Feeder 4: Pole 50104003

For this option, two operating scenarios are considered:

- All community feeders are fed from one step-up transformer. This is considered the worst-case operating scenario.
- Each two of the community feeders are fed from one step-up transformer. The distribution of the community feeders on each transformer was decided based on the peak demand load of the four feeders such that both transformers are equally loaded.

1.3.7 Option 5

Upgrade all customers' transformers to have 25kV primary voltage.

- Install two (2) new 4.16/25kV, 5MVA, step-up transformers in the new power plant and connect the primary side of these transformers to the new main 5kV switchgear via cables.
- Feeders 1 and 3 are combined into one feeder by connecting the lines at Poles 50101001 in Feeder 1 and 50103001 in Feeder 3.
- The combined feeders are connected to one step-up transformer at Pole 50101001 in Feeder 1.

- Feeders 2 and 4 are combined into one feeder by connecting the lines at Pole 50102003 in Feeder 2 and 50104003 in Feeder 4.
- The combined feeders are connected to the other step-up transformer at Pole 50102268 in Feeder 2.

The single-line diagrams showing the network topology for each option are included under Appendices 1.A to 1.G.

2. Discussion

Since the new power plant is located in a considerably remote location that is far from the existing power plant location, it became crucial to find a proper solution for the connection of the existing community feeders to the new power plant. The recommended solution optimizes the following criteria:

- Minimizing the voltage drop across the lines. The voltage drop should not exceed 3% from the generators to each individual consumer.
- Minimizing the network active power losses.

This study evaluates the five (5) options proposed by QEC and the adjustments made by Asher to determine the most technically feasible option and the provides recommendations for further aspects to be considered.

2.1 Sources of Data

Network model and simulation parameters are set based on the following inputs:

- **ETAP Model:**

The ETAP model used is based on the model developed for QEC Penetration Study. The model of the power plant is updated to reflect the topology of the new plant.

- **One-line Diagrams:**

The Network model is built using the provided one-line diagrams. These diagrams are also used to obtain the connected load and phase connection of each customer.

- **Generation Forecast:**

QEC provided a table showing the estimated electricity produced over the years from 2026 to 2066 (See Appendix 2). These estimates are used for feeder sizing, voltage drop, and network losses calculations.

2.2 Assumptions

- The maximum demand factors of each feeder load in 2019 are calculated based on the load data reading provided by QEC. The estimated electricity production for subsequent years (Appendix 2) is used to calculate the maximum demand factor for these years.

- Normally open switches, interconnecting different feeders and used during the failure or maintenance of any of the feeder breakers, are not included in the model and the penetration study except for the options where each two feeders are combined.
- Since the specified AASC cables are not available in the standard ETAP library, AAC cables are used instead. The electrical and geometric characteristics of the selected cable are modified to match the AASC cable specifications provided by QEC.
- The new power plant main switchgear tie breaker is assumed to be open.
- The boundary conditions for the voltage limits at all networks nodes (buses) are assumed to be $\pm 3\%$.
- The maximum transmission line size to be used is 4/0 AWG with a single conductor per phase.
- QEC advised that most of the loads are non-inductive and that the overall power factor for each feeder is in the order of 0.99. For the purpose of this study, all loads are assumed to have a 0.95 power factor for more conservative values of load currents.
- Based on overhead line conductor parameters provided by QEC, resistance, reactance, and susceptance values for overhead lines are calculated using ETAP considering the following conductor configuration on the pole structure:
 - Conductor height: 34 ft (unless otherwise indicated on the single-line diagrams).
 - Spacing between phases: 2 ft.
- Generator plant service loads are not considered in the analysis.

2.3 Network Configuration

The new power plant for Cambridge Bay consists of two (2) 1500kW, two (2) 1100kW and one (1) 850kW generators with an output voltage of 4.16kV. Generator outputs are connected to a main 4.16kV switchgear with two (2) bus sections connected together via tie breaker such that one (1) 1500kW and one (1) 1100kW generators are connected to one bus section, and the one (1) 1500kW, one (1) 1100kW, and one (1) 850kW generators are connected to the other bus section.

Existing community feeders are connected to the two bus sections of the main switchgear. The connection scheme depends on the tie-in option to be studied.

In order to improve customer power supply reliability, feeders are interconnected via a set of normally open switches. Any of these switches may be closed in the case when one of the feeder breakers is out of duty due to failure or for maintenance purposes. Since the case where both feeders are connected to one feeder breaker does not represent normal network operation and is used only for maintenance purposes, these configurations are not included in the model except where two feeders are combined into one feeder. For this case, only the tie switch is considered closed.

The network ETAP model for each study option is provided in Appendices 1.A to 1.G.

2.4 Calculation Procedures

2.4.1 Load Parameters Calculations

The peak demand load for the year 2019 is obtained from the metering readings provided by QEC for this year and is used to calculate the maximum demand factor for the loads of each feeder as shown in Table 1.

Table 1: Maximum Demand (2019)

	Connected Load (kVA)	Max. Demand Load (kVA)	Max. Demand Factor (%)
Feeder 1	2537.5	989.625	39.00%
Feeder 2	3017.5	754.375	25.00%
Feeder 3	642.5	334.1	52.00%
Feeder 4	450	234	52.00%
Total	6647.5	2312.1	

The estimated electricity production (Appendix 2) is used to calculate the percentage growth of electricity demand which is, in turn, used to calculate the maximum demand for the successive years as shown in Table 2.

Table 2: Estimated Growth in Demand Load

Year	Population Demand Load Change (%)	Maximum Demand Factors			
		Feeder 1	Feeder 2	Feeder 3	Feeder 4
2019	-	39.00%	25.00%	52.00%	52.00%
2026	55.00%	60.45%	38.75%	80.60%	80.60%
2027	57.00%	61.23%	39.25%	81.64%	81.64%
2028	58.00%	61.62%	39.50%	82.16%	82.16%
2029	59.00%	62.01%	39.75%	82.68%	82.68%
2030	61.00%	62.79%	40.25%	83.72%	83.72%
2031	62.00%	63.18%	40.50%	84.24%	84.24%
2032	64.00%	63.96%	41.00%	85.28%	85.28%
2033	65.00%	64.35%	41.25%	85.80%	85.80%
2034	66.00%	64.74%	41.50%	86.32%	86.32%
2035	68.00%	65.52%	42.00%	87.36%	87.36%
2036	70.00%	66.30%	42.50%	88.40%	88.40%
2041	78.00%	69.42%	44.50%	92.56%	92.56%

Year	Population Demand Load Change (%)	Maximum Demand Factors			
		Feeder 1	Feeder 2	Feeder 3	Feeder 4
2046	87.00%	72.93%	46.75%	97.24%	97.24%
2051	98.00%	77.22%	49.50%	102.96%	102.96%
2056	110.00%	81.90%	52.50%	109.20%	109.20%
2061	123.00%	86.97%	55.75%	115.96%	115.96%
2066	138.00%	92.82%	59.50%	123.76%	123.76%

As agreed with QEC, the study considers the load demand of the first 10 years (2026 to 2036) in one-year steps, and the following 30 years (2037 to 2066) in 5-year steps.

The above demand factors are used in the ETAP model.

The maximum demand load analysis of the four feeders based on the table above shows that:

- The balanced connection of feeders for the options where two feeders are supposed to be connected, is to connect Feeders 1 and 4 together and Feeders 2 and 3 together.
- The maximum generation capacity for each bus section of the switchgear is 2500 kW. The peak demand load forecast for all the years exceeds 2500kW. Therefore, the switchgear bus-tie breaker needs to be closed such that the total load can be distributed among all the generators.
- Customer transformers connected to Feeders 3 and 4 need to be upgraded to 125% of their current ratings to accommodate the forecasted demand.

2.4.2 Design Constraints

The following design constraint are established by QEC:

- The total voltage drop from the generators to each customer load shall not exceed 3%.
- The maximum size of a transmission line is 4/0AWG with no more than one conductor per phase.
- Initial calculations are made with all transformer taps set at the zero-position. However, transformer tap settings can be changed to compensate for excessive voltage drop when needed.

2.5 Results

Electricity production estimate for the years from 2026 to 2066 is used to calculate the demand load and demand factor for each feeder. These demand factors were applied to calculate the minimum feeder size that is required to achieve a maximum voltage drop of 3% at the customer transformer using the different options detailed under Section 1.3.

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The study concludes that:

- Options 1 and 2 do not satisfy the 3% voltage drop criteria due to the distance between the new power plant and the tie-ins of Feeders 1, 3, and 4. Therefore, these options cannot be utilized.
- Comparing the results of Options 3 and 4, it can be shown that Option 3 provides better results than Option 4 since the North Yard is farther away from the nearest tie-in to the community feeders than the existing power plant.

Both Options 3 and 4 fail to satisfy the 3% voltage drop criteria when all the feeders are fed from one step-up transformer.

- The alternatives proposed for Option 3 provide better results in terms of voltage drop and active power losses. However, unlike Option 3A, Option 3B allows all feeders to be fed from one step-up transformer without violating the voltage drop criteria.

The study, also, concludes that Option 5 is the recommended option since it involves less voltage drop and active power loses along the power lines as shown by Table 4 below.

Table 3: Study Results Summary

Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks	
		Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers		
1		Failed								
2		Failed								
3	A	Failed								
	B	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%		
3A	A	Failed								
	B	1/0 AWG	3/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%		
3B	A	2/0 AWG	1/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%		
	B	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%		
4	A	Failed								
	B	Failed								
5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-5%	N/A		
	B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A		

Scenario A: All feeders are fed from one step-up transformer

Scenario B: Feeders are distributed across both step-up transformers

Table 4: Study Results Details

Year	Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2026	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	2/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
2027	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	
	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	3/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

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Year	Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2028	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	3/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
2029	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	
	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	3/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

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			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2030	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	3/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	4/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	2/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
2031	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	2/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

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			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2032	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	2/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
2033	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	2/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

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			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2034	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	3/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
2035	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	0%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	3/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

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			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2036	1		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	3/0 AWG	3/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
2041	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	
	1		Failed	2/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

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Year	Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2046	1		Failed	2/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	Failed	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	Failed	Failed	
2051	1		Failed	3/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	4/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	4/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3A	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	4	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	Failed	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	Failed	Failed	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	0%	N/A	

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Year	Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2056	1		Failed	3/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3A	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-2.5%	-5%	
	4	A	Failed	1/0 AWG	Failed	Failed	4/0 AWG	Failed	Failed	
		B	Failed	1/0 AWG	2/0 AWG	4/0 AWG	4/0 AWG	Failed	Failed	
2061	1		Failed	4/0 AWG	Failed	Failed	N/A	-2.5%	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3A	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3B	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	4	A	Failed	1/0 AWG	Failed	Failed	4/0 AWG	Failed	Failed	
		B	Failed	1/0 AWG	3/0 AWG	4/0 AWG	4/0 AWG	Failed	Failed	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	

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Year	Option	Operating Scenario	Min Main Feeder Line Size				Main Line Size	Transformer Tap Settings		Remarks
			Feeder 1	Feeder 2	Feeder 3	Feeder 4		Step-up Transformers	Step-Down Transformers	
2066	1		Failed	4/0 AWG	Failed	Failed	N/A	N/A	N/A	
	2		Failed	1/0 AWG	Failed	Failed	N/A	N/A	N/A	
	3	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3A	A	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	3B	A	2/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	4/0 AWG	-5%	-5%	
	4	A	Failed	1/0 AWG	Failed	Failed	4/0 AWG	Failed	Failed	
		B	Failed	1/0 AWG	Failed	4/0 AWG	4/0 AWG	Failed	Failed	
	5	A	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-5%	N/A	
		B	1/0 AWG	1/0 AWG	1/0 AWG	4/0 AWG	N/A	-2.5%	N/A	

Scenario A: All feeders are fed from one step-up transformer

Scenario B: Feeders are distributed across both step-up transformers

3. Conclusion and Recommendations

The utilization of Options 1 and 2 was found to be not feasible due to the distance between the new power plant and the tie-in locations of the community feeders particularly for Feeders 1, 3, and 4.

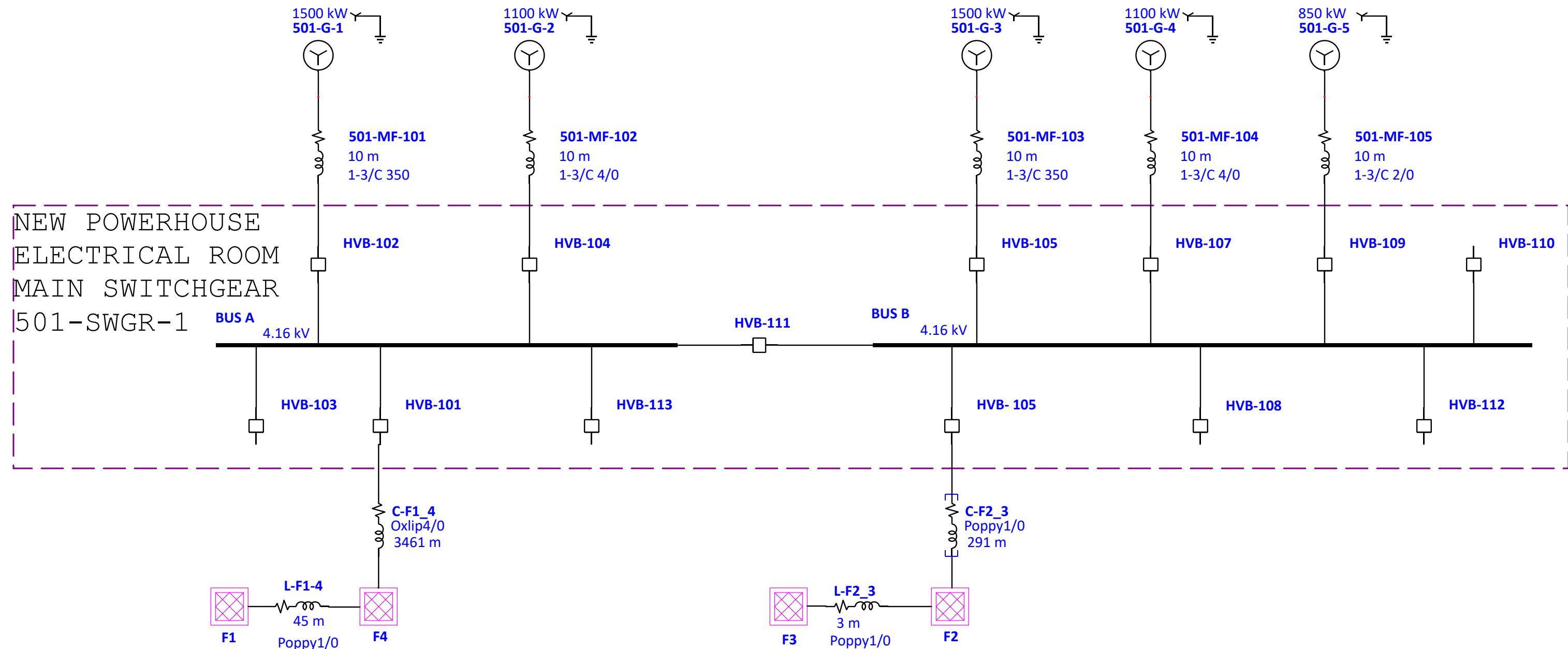
Options 3, 3A, and 4 can be utilized with the exception that all feeders cannot be fed from one step-up transformer. However, Option 3B allows the two scenarios where feeders can either be fed from one transformer or their loads is distributed on both step-up transformers.

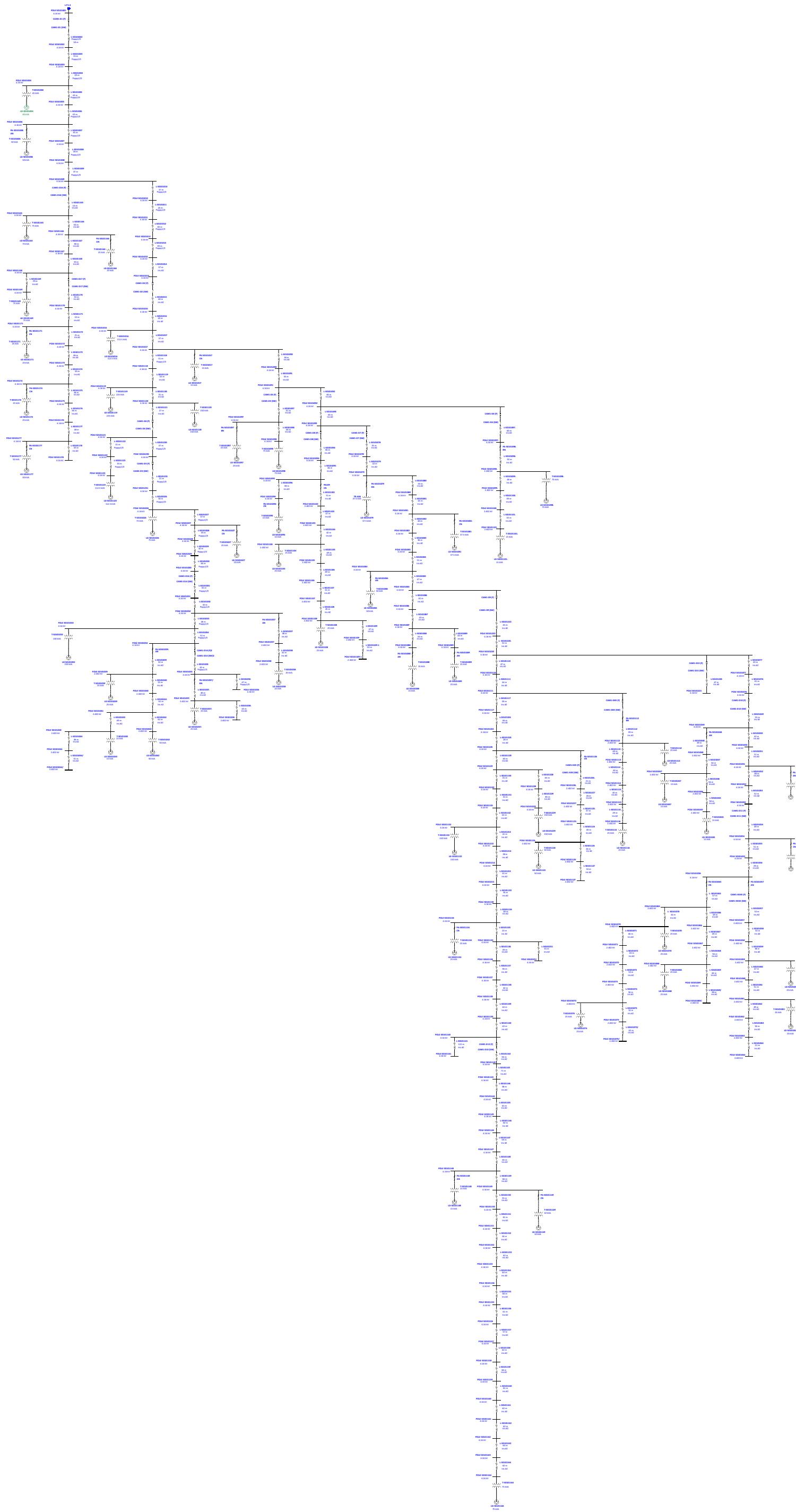
Option 5 was found to be the most technically preferred since it involves less voltage drop and active power losses.

Appendix 1.A

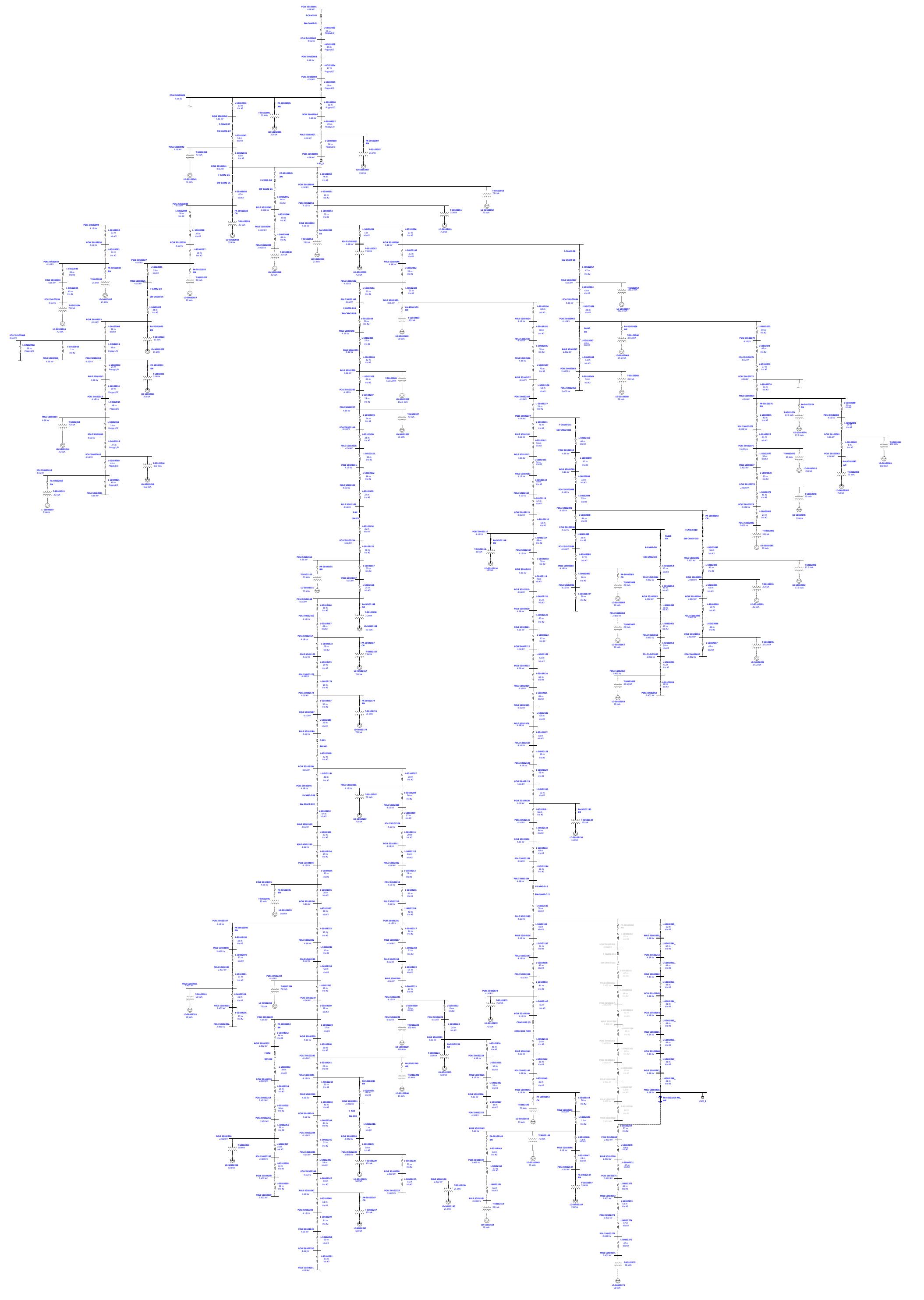
Cambridge Bay Network ETAP Model and Results – Option 1

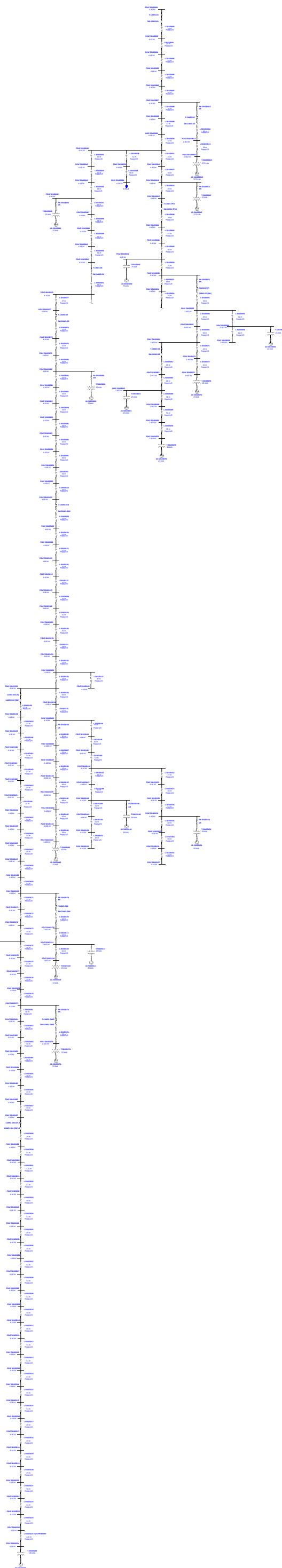
One-Line Diagram - OLV1 (Load Flow Analysis)

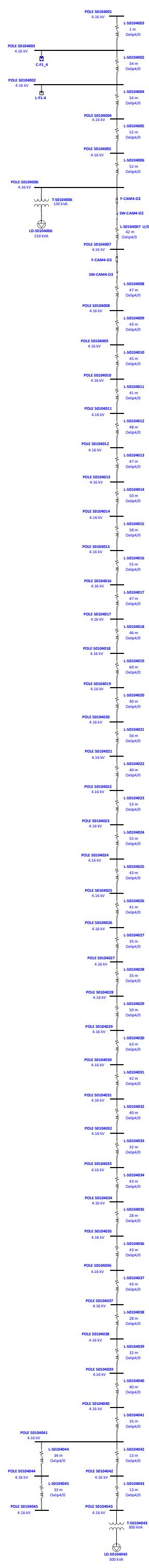




One-Line Diagram - OLV1=>F2 (Load Flow Analysis) - Ahmed.Abdelfattah(Project Editor)







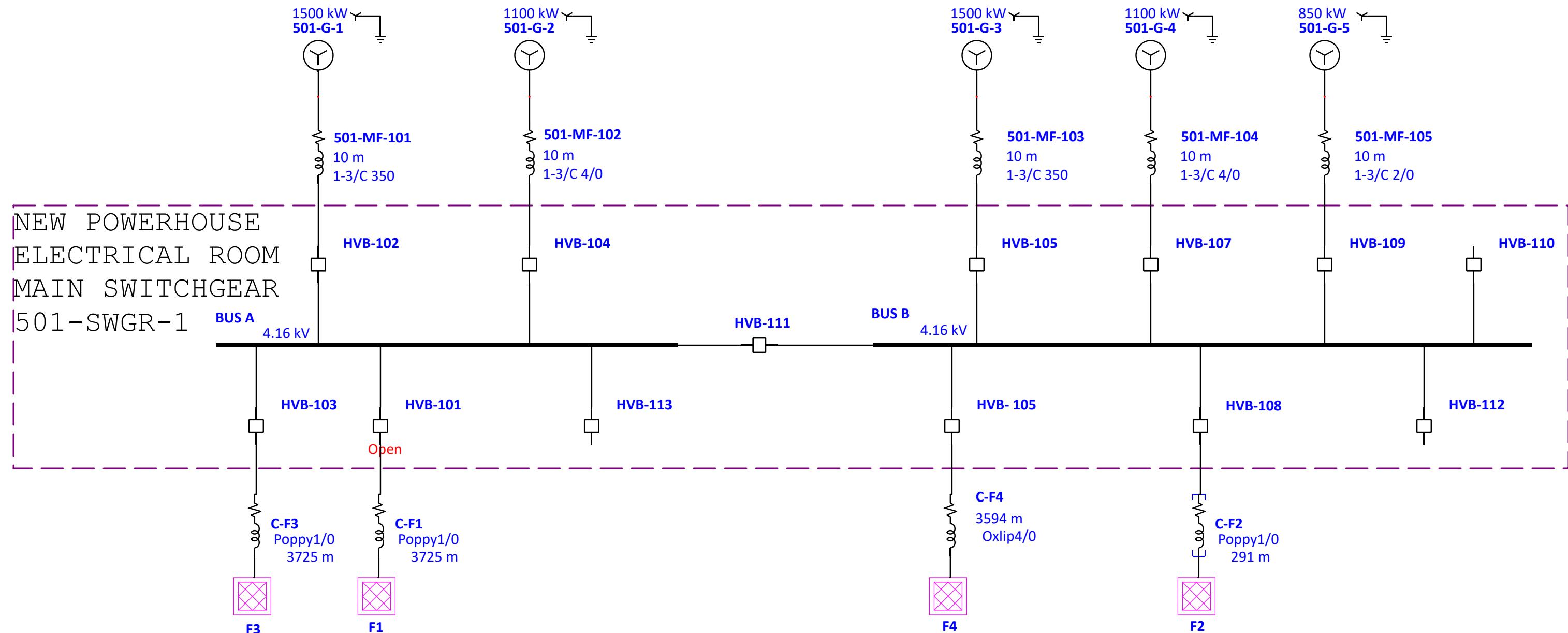
Option #1

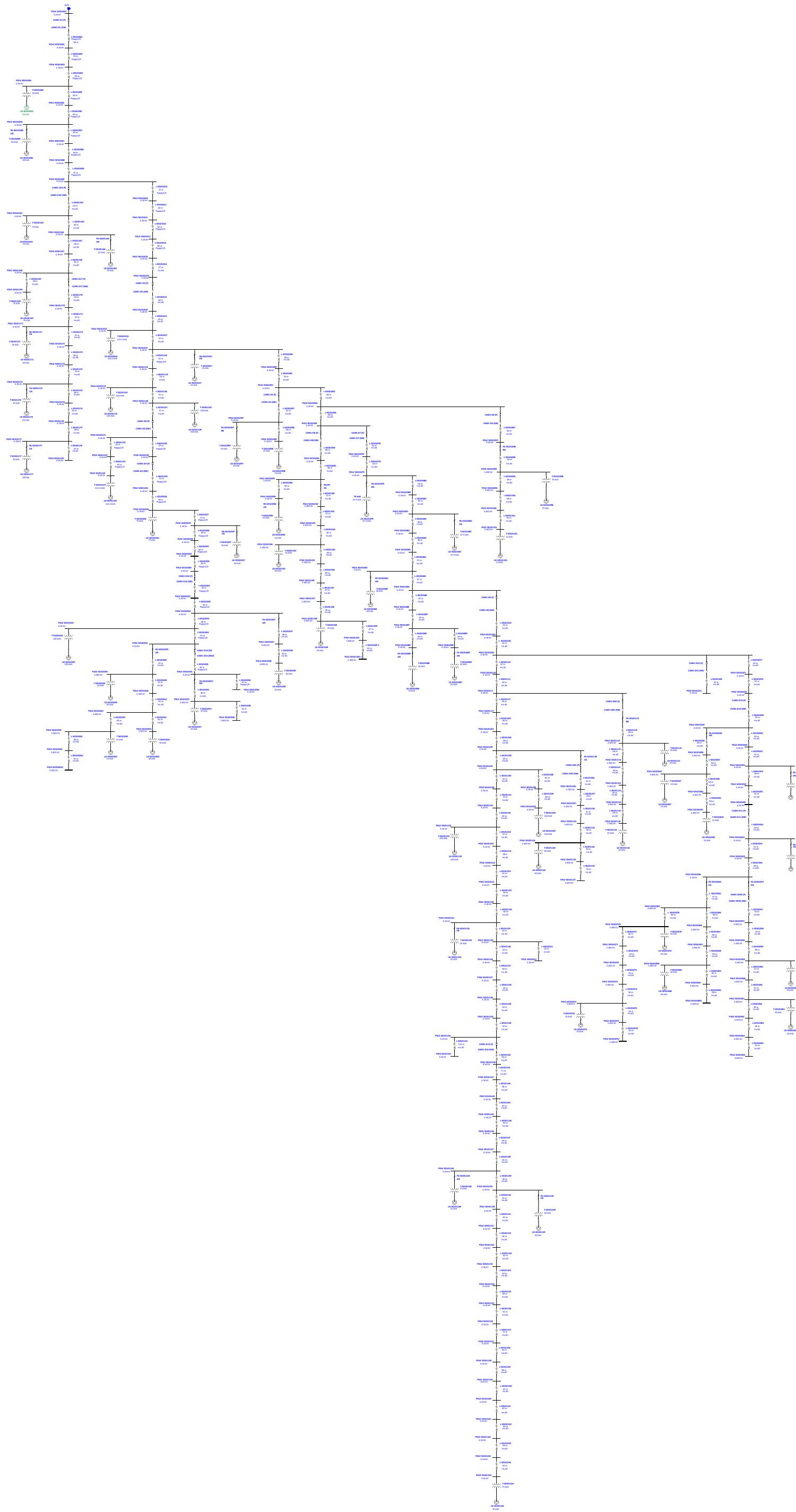
Year	F1		F2		F3		F4	
	Status	Min. Main Line Size L-F1_4	Status	Min. Main Line Size C-F2_3	Status	Min. Main Line Size L-F2_3	Status	Min. Main Line Size C-F1_4
2026	Failed		Passed	1/0 AWG	Failed		Failed	
2027	Failed		Passed	1/0 AWG	Failed		Failed	
2028	Failed		Passed	1/0 AWG	Failed		Failed	
2029	Failed		Passed	1/0 AWG	Failed		Failed	
2030	Failed		Passed	1/0 AWG	Failed		Failed	
2031	Failed		Passed	1/0 AWG	Failed		Failed	
2032	Failed		Passed	1/0 AWG	Failed		Failed	
2033	Failed		Passed	1/0 AWG	Failed		Failed	
2034	Failed		Passed	1/0 AWG	Failed		Failed	
2035	Failed		Passed	1/0 AWG	Failed		Failed	
2036	Failed		Passed	1/0 AWG	Failed		Failed	
2041	Failed		Passed	2/0 AWG	Failed		Failed	
2046	Failed		Passed	2/0 AWG	Failed		Failed	
2051	Failed		Passed	3/0 AWG	Failed		Failed	
2056	Failed		Passed	3/0 AWG	Failed		Failed	
2061	Failed		Passed	4/0 AWG	Failed		Failed	
2066	Failed		Passed	4/0 AWG	Failed		Failed	

Appendix 1.B

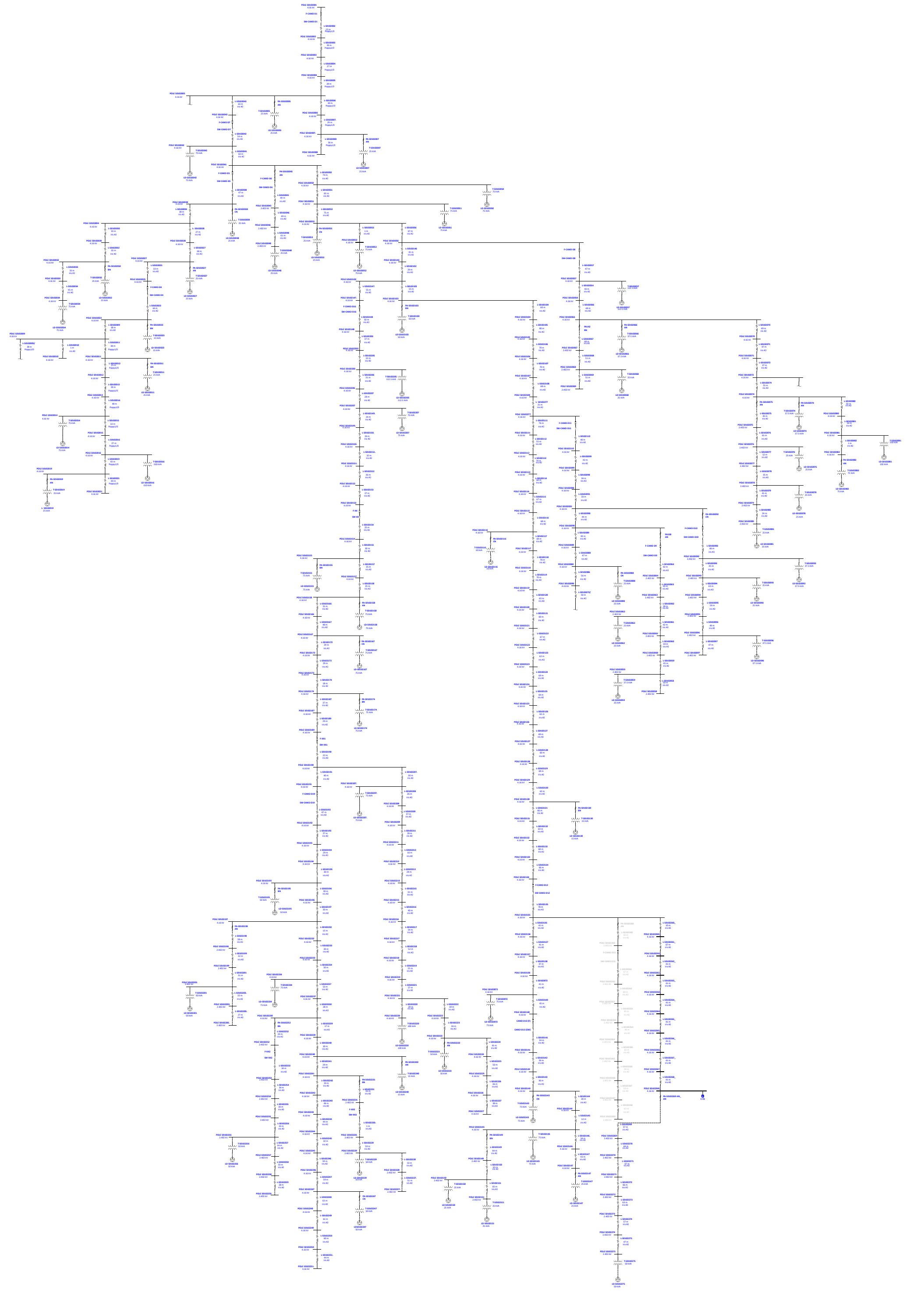
Cambridge Bay Network ETAP Model and Results – Option 2

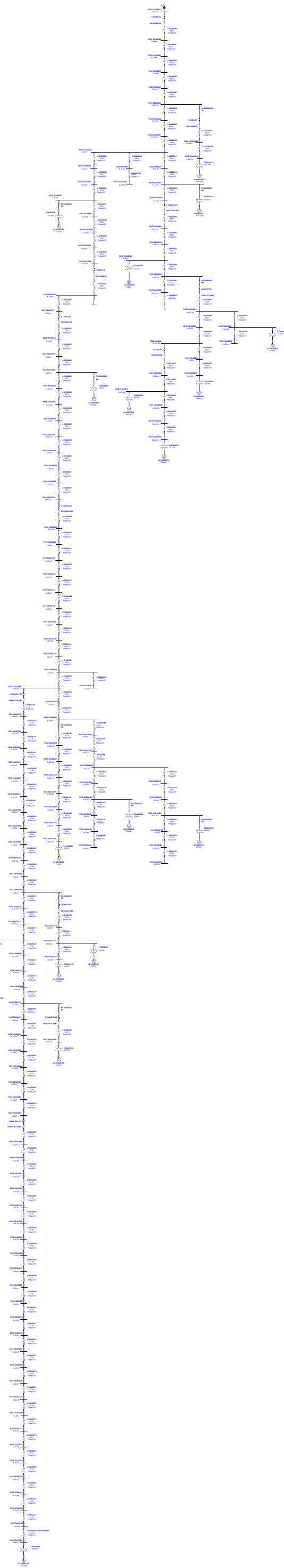
One-Line Diagram - OLV1 (Load Flow Analysis)

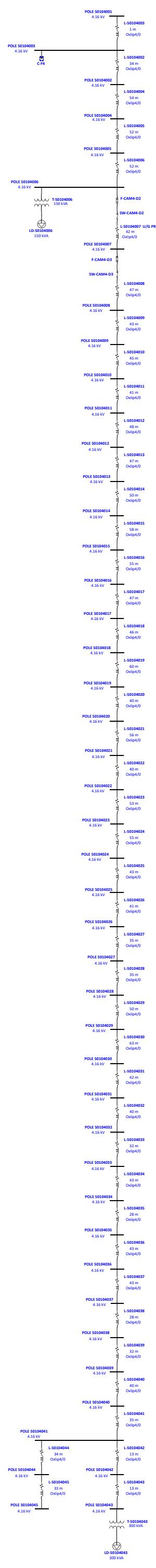




One-Line Diagram - OLV1=>F2 (Load Flow Analysis) - Ahmed.Abdelfattah(Project Editor)







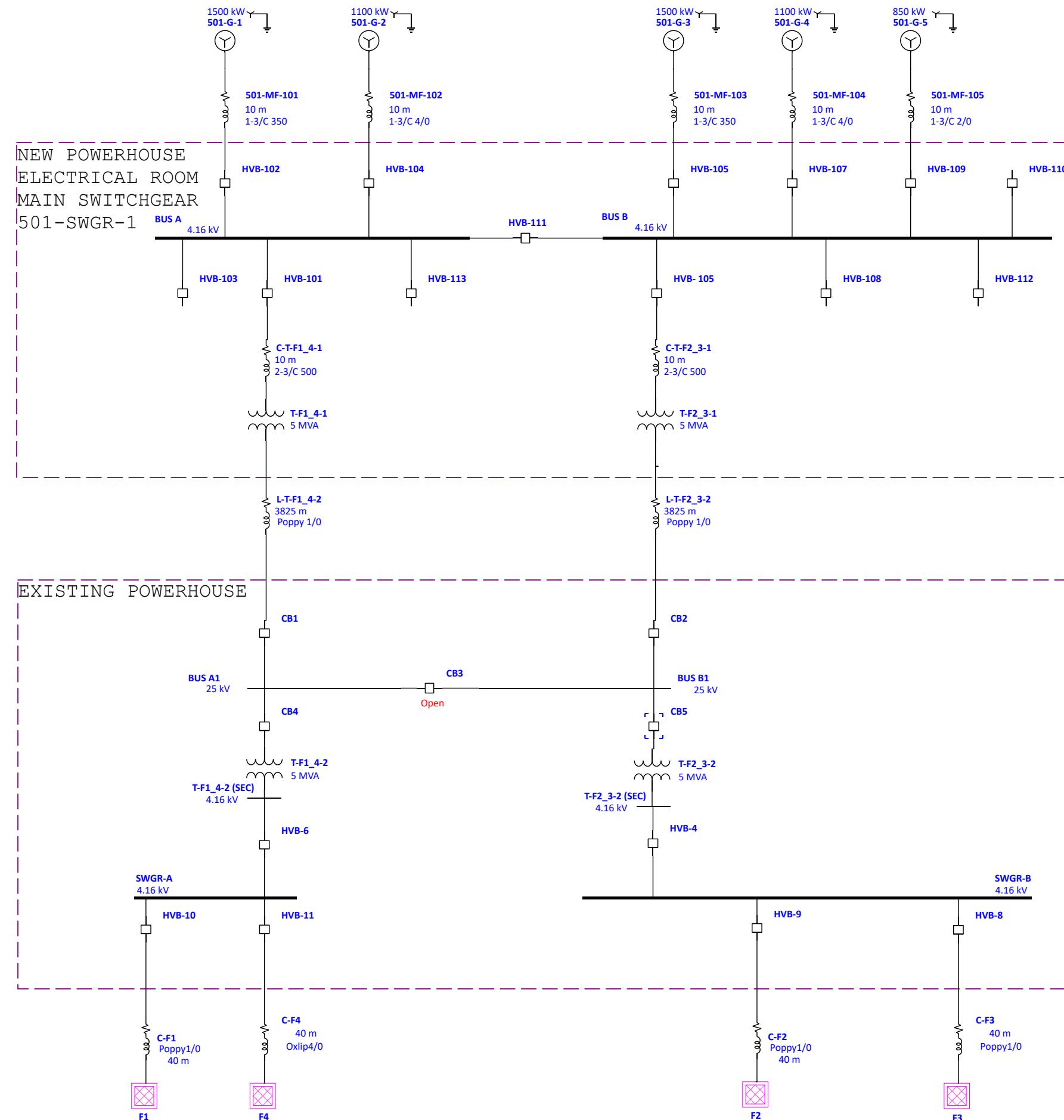
Option #2

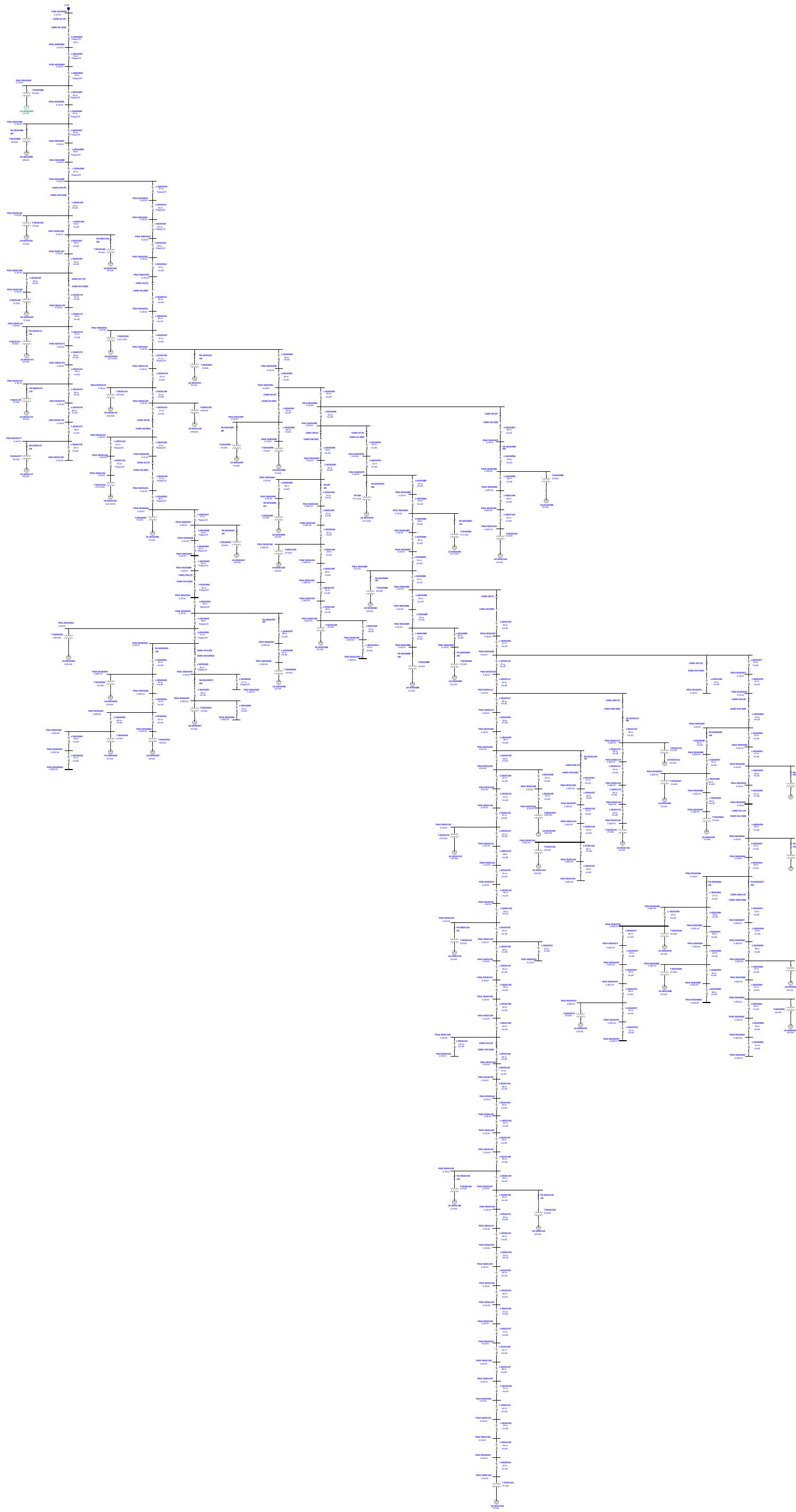
Year	F1		F2		F3		F4	
	Status	Min. Main Line Size C-F1	Status	Min. Main Line Size C-F2	Status	Min. Main Line Size C-F3	Status	Min. Main Line Size C-F4
2026	Failed		Passed	1/0 AWG	Failed		Failed	
2027	Failed		Passed	1/0 AWG	Failed		Failed	
2028	Failed		Passed	1/0 AWG	Failed		Failed	
2029	Failed		Passed	1/0 AWG	Failed		Failed	
2030	Failed		Passed	1/0 AWG	Failed		Failed	
2031	Failed		Passed	1/0 AWG	Failed		Failed	
2032	Failed		Passed	1/0 AWG	Failed		Failed	
2033	Failed		Passed	1/0 AWG	Failed		Failed	
2034	Failed		Passed	1/0 AWG	Failed		Failed	
2035	Failed		Passed	1/0 AWG	Failed		Failed	
2036	Failed		Passed	1/0 AWG	Failed		Failed	
2041	Failed		Passed	1/0 AWG	Failed		Failed	
2046	Failed		Passed	1/0 AWG	Failed		Failed	
2051	Failed		Passed	1/0 AWG	Failed		Failed	
2056	Failed		Passed	1/0 AWG	Failed		Failed	
2061	Failed		Passed	1/0 AWG	Failed		Failed	
2066	Failed		Passed	1/0 AWG	Failed		Failed	

Appendix 1.C

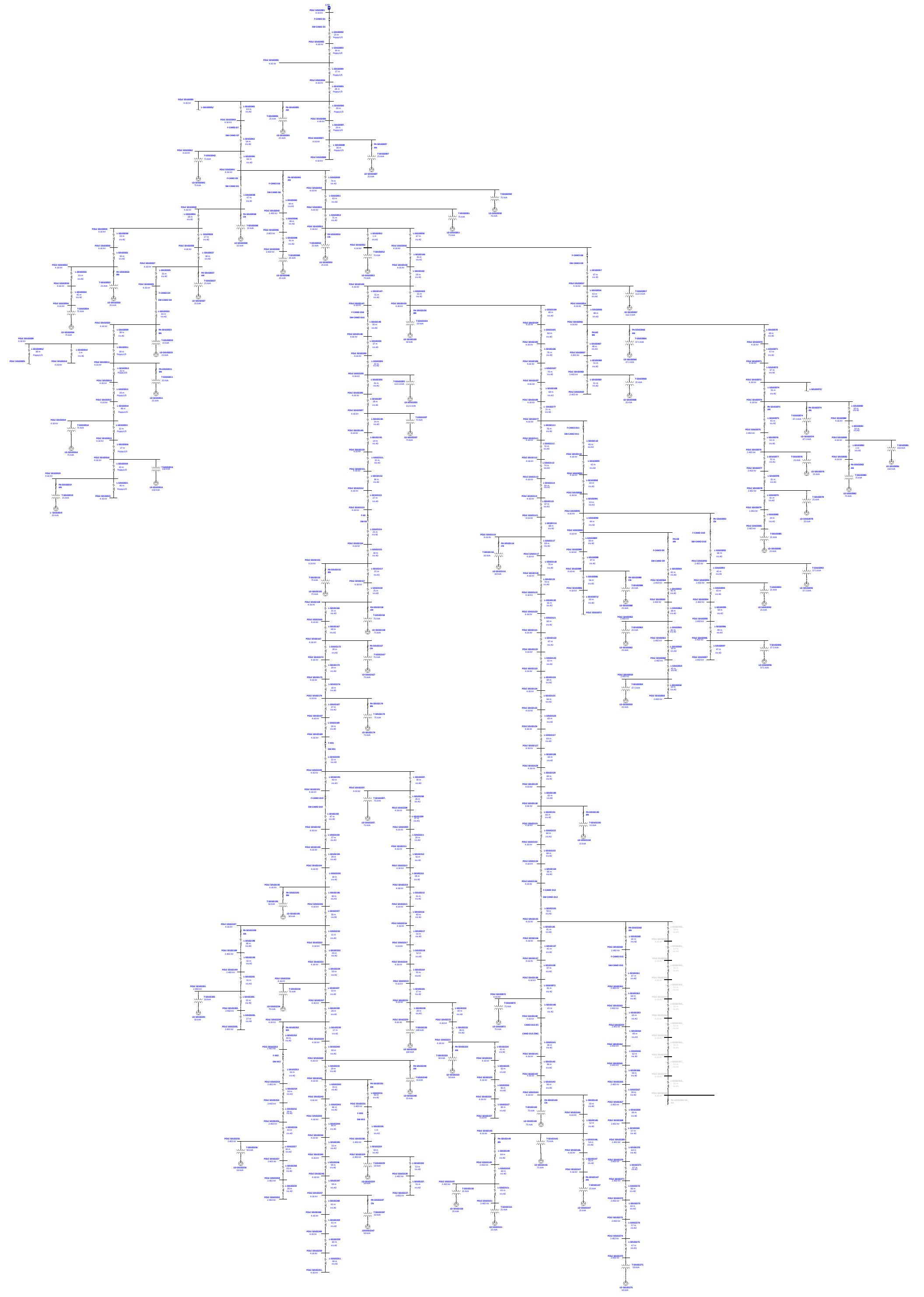
Cambridge Bay Network ETAP Model and Results – Option 3

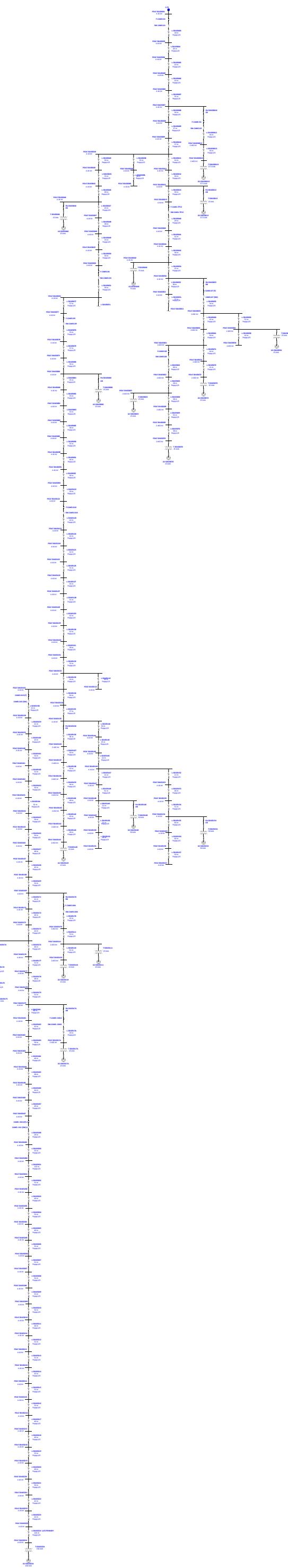
One-Line Diagram - OLV1 (Edit Mode)



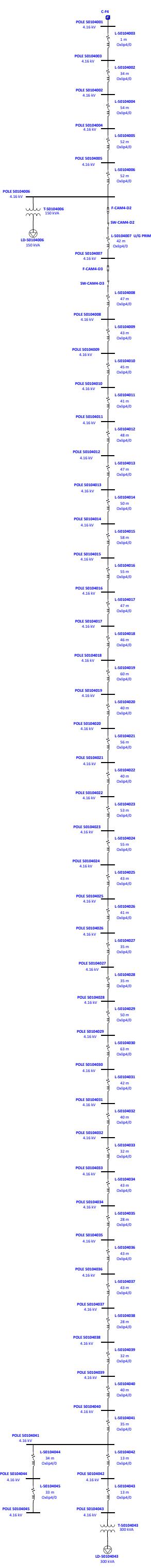


One-Line Diagram - OLV1=>F2 (Edit Mode) - Ahmed.Abdelfattah(Project Editor)





One-Line Diagram - OLV1=>F4 (Edit Mode) - Ahmed.Abdelfattah(Project Editor)

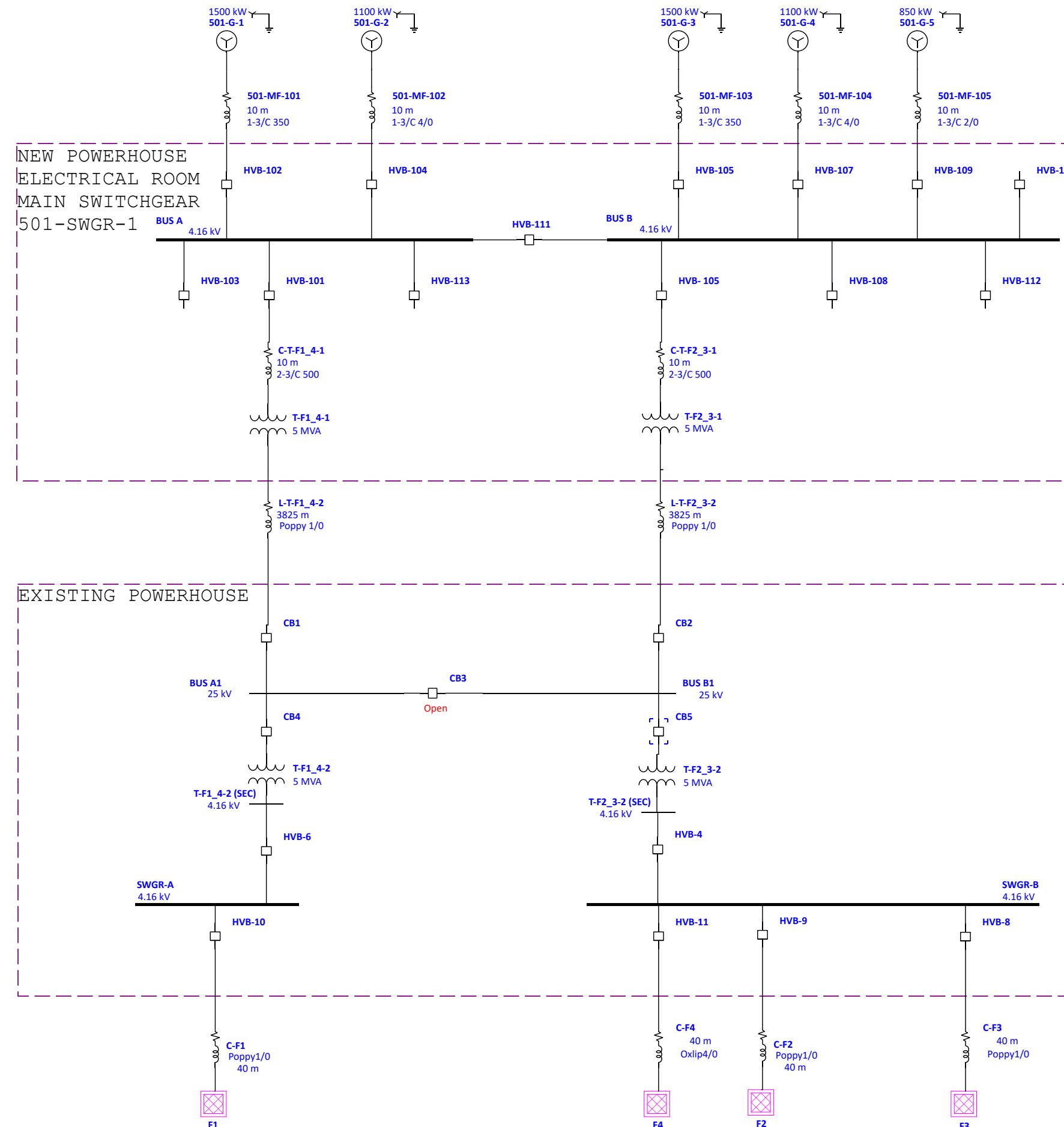


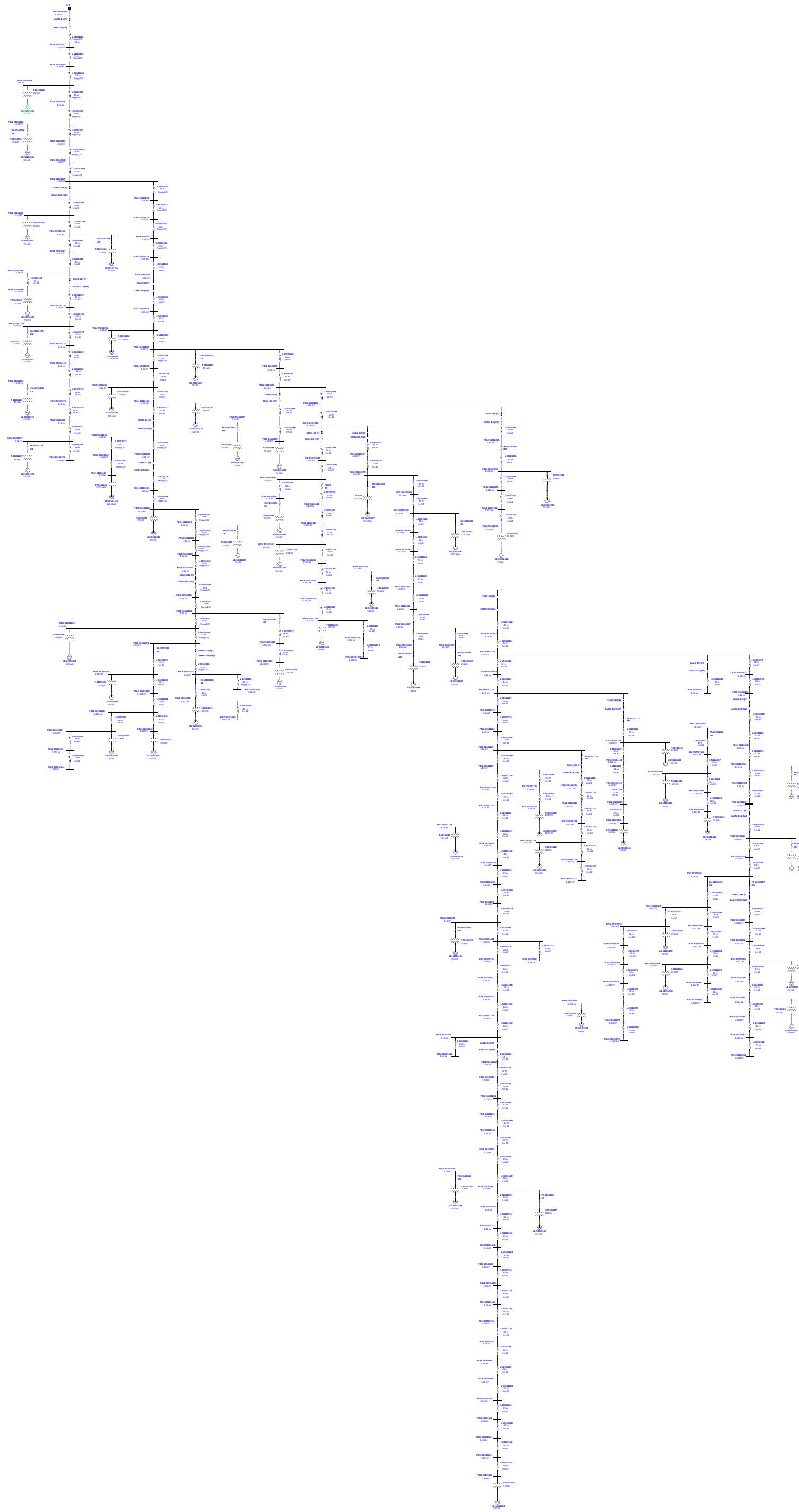
Option 3: Scenario A: All Feeders are Fed from One Step-up Transformer

Option 3: Scenario B: Each Two Feeders are Fed from One Step-up Transformer

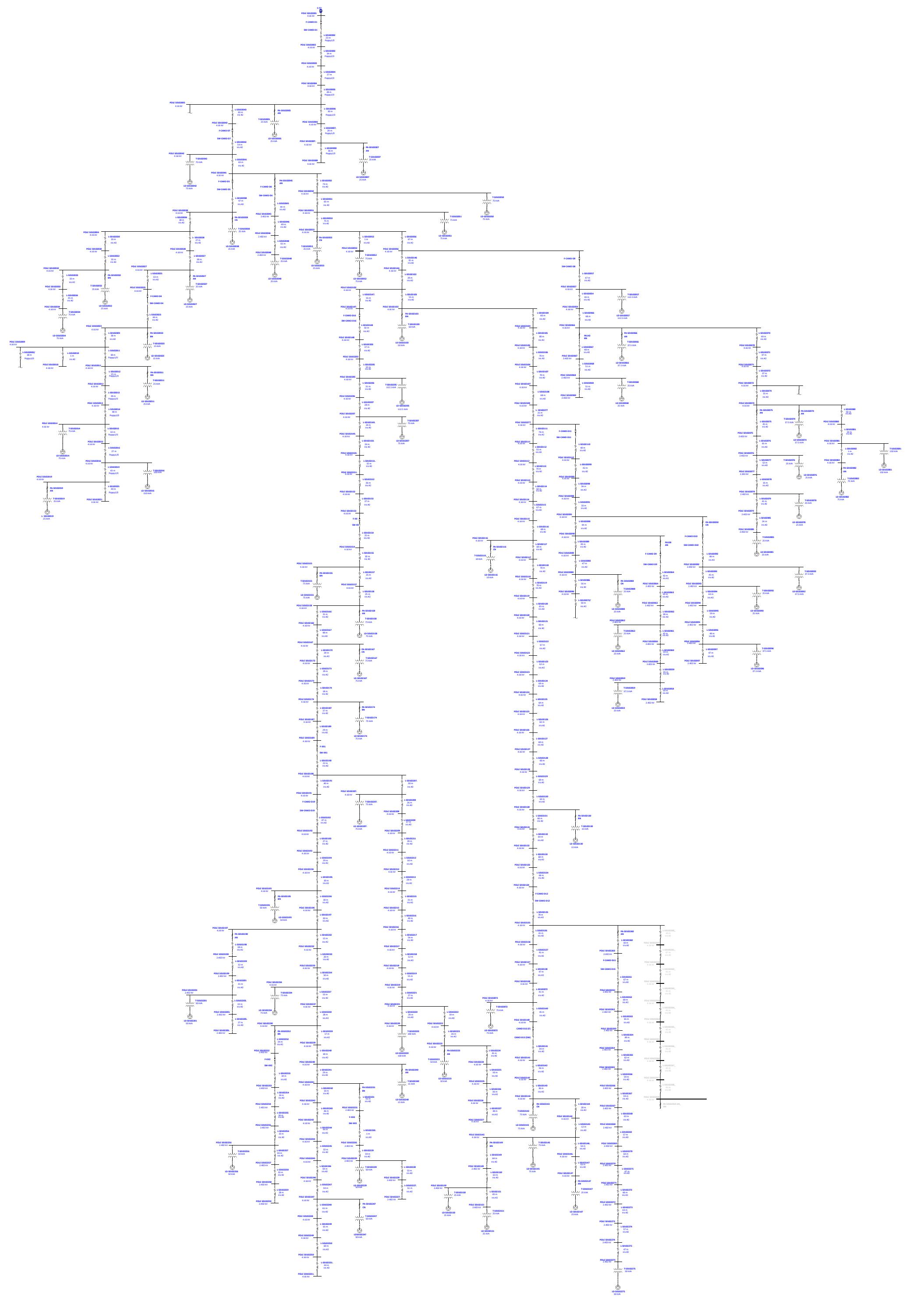
Appendix 1.D
Cambridge Bay Network ETAP Model – Option 3A

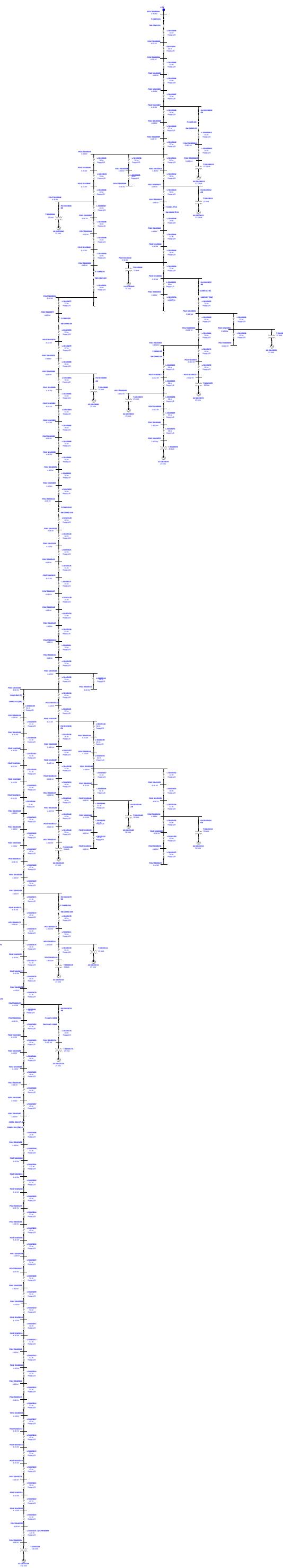
One-Line Diagram - OLV1 (Load Flow Analysis)

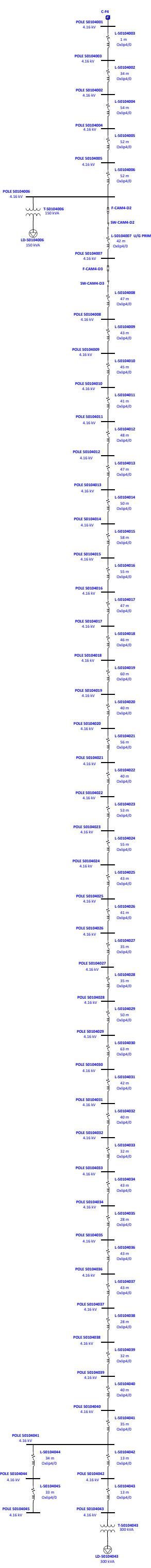




One-Line Diagram - OLV1=>F2 (Load Flow Analysis) - Ahmed.Abdelfattah(Project Editor)







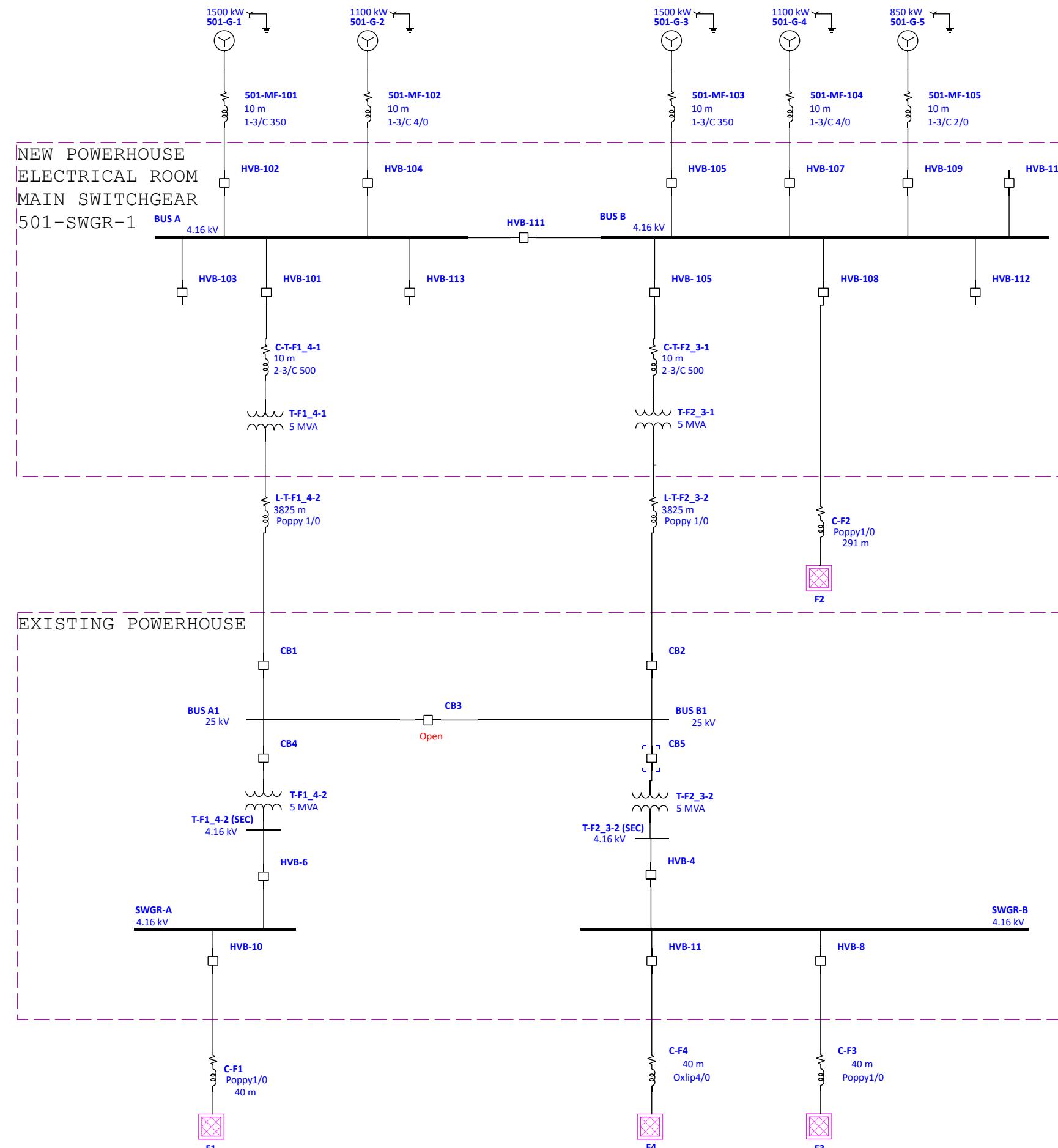
Option 3A: Scenario A: All Feeders are Fed from One Step-up Transformer

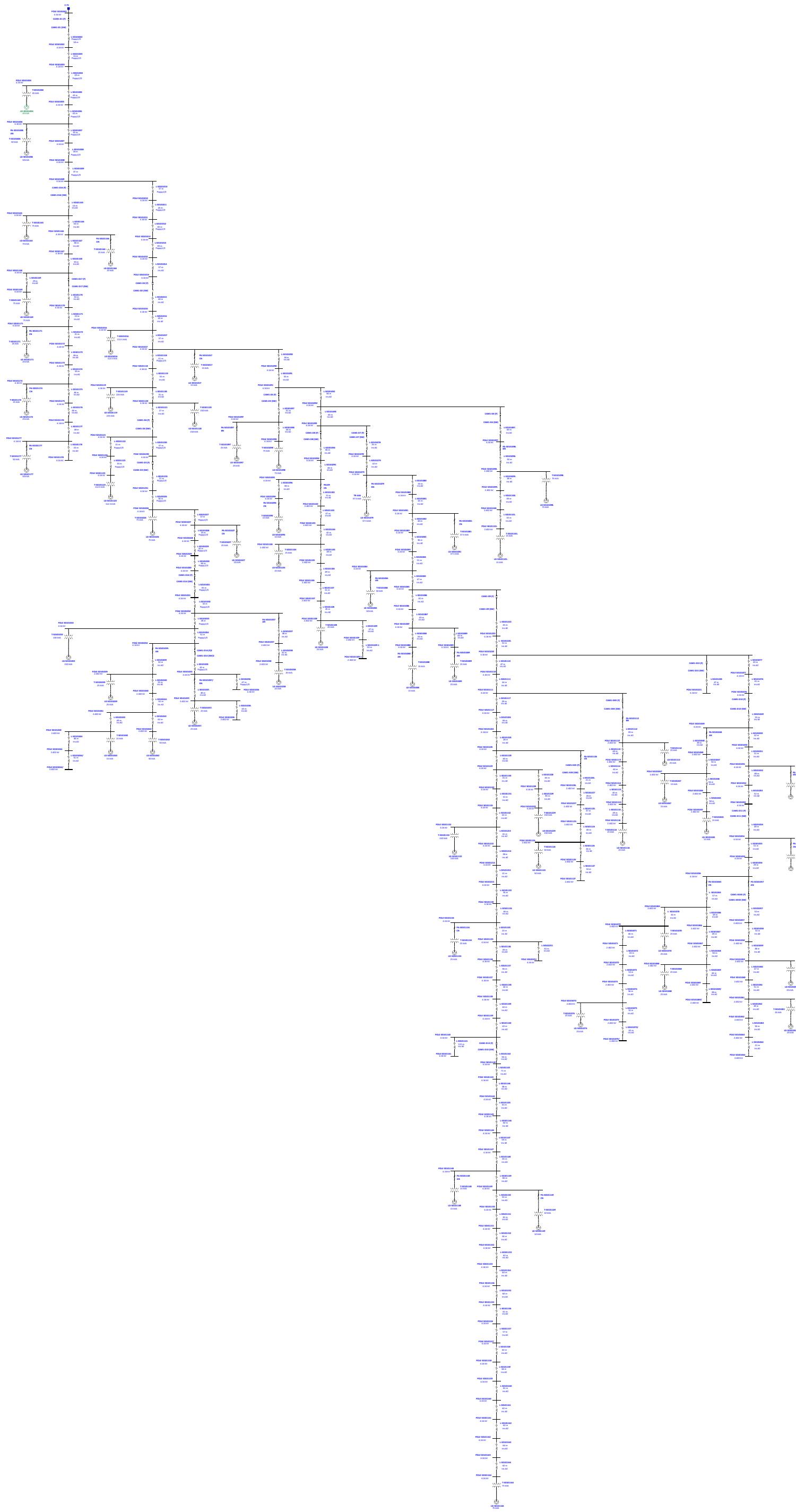
Option 3A: Scenario B: Feeder 1 is Fed from T-F1 4-2 Step-up Transformer and Feeders 2, 3, and 4 are Fed from T-F2 3-2 Step-Up Transformer

Appendix 1.E

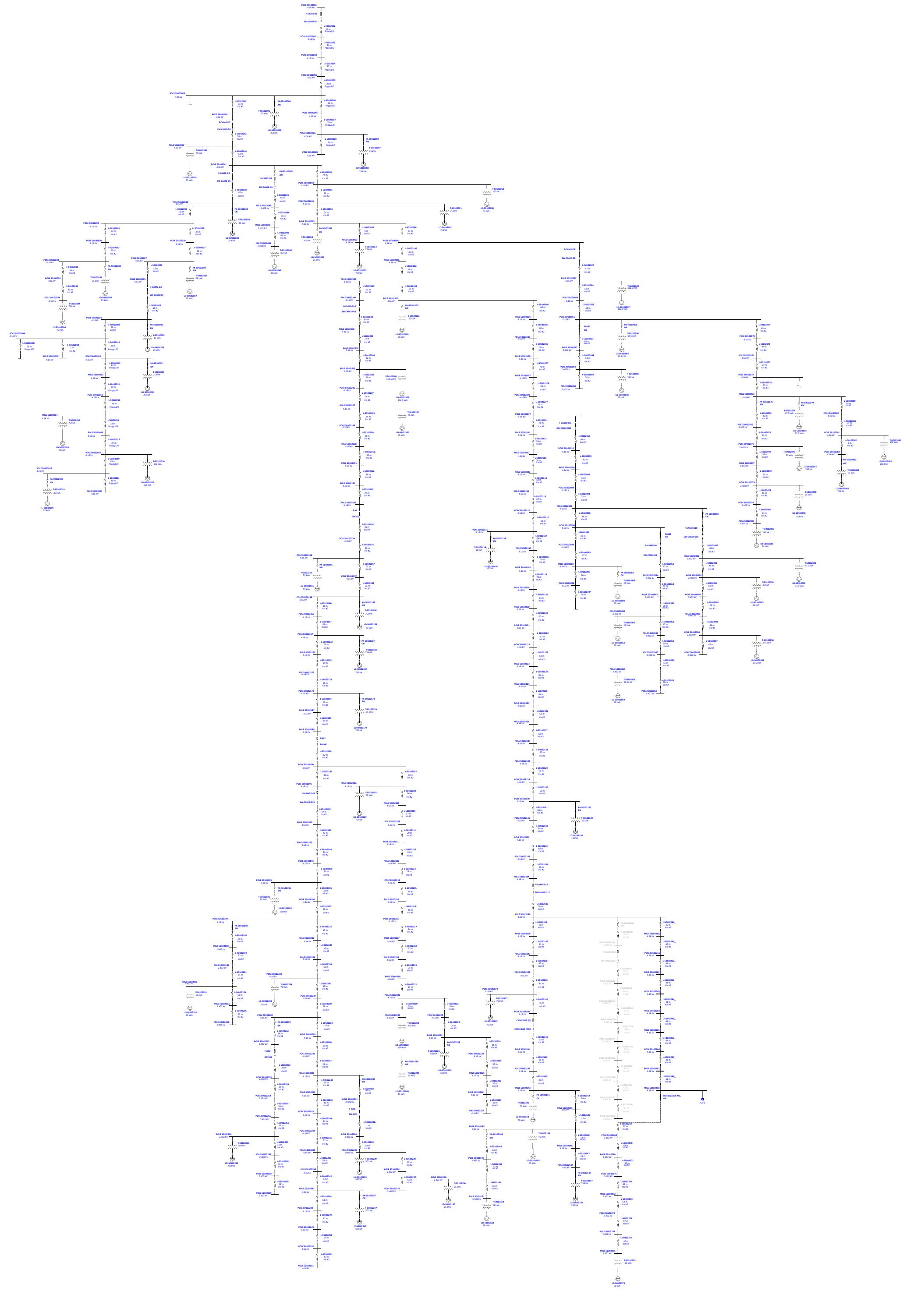
Cambridge Bay Network ETAP Model and Results – Option 3B

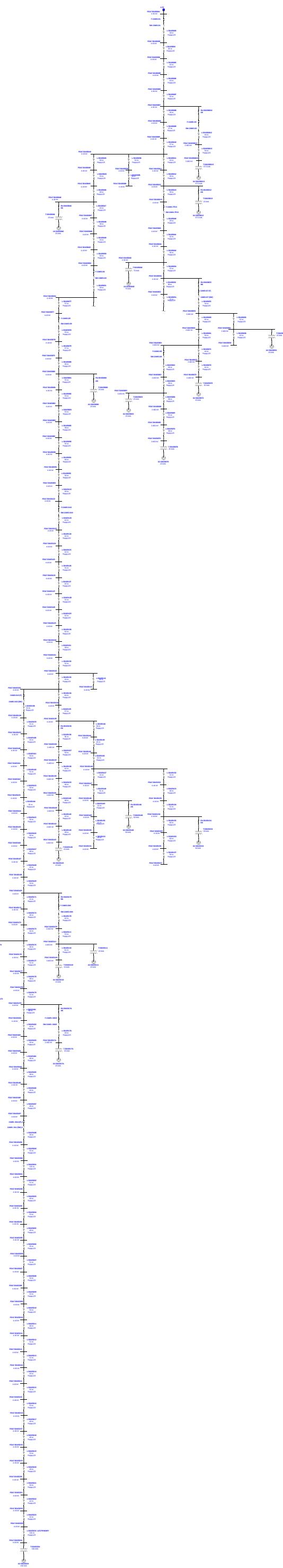
One-Line Diagram - OLV1 (Load Flow Analysis)

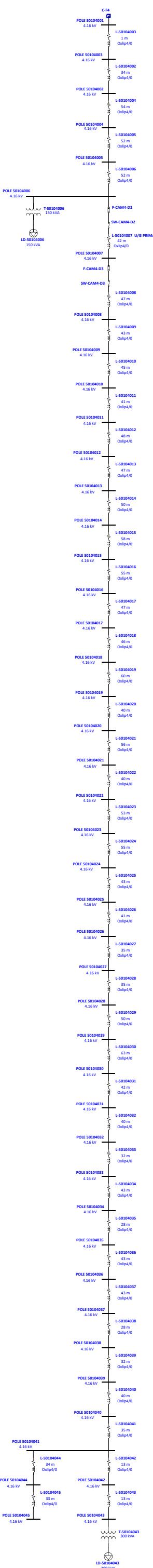




One-Line Diagram - OLV1=>F2 (Load Flow Analysis) - Ahmed.Abdelfattah(Project Editor)







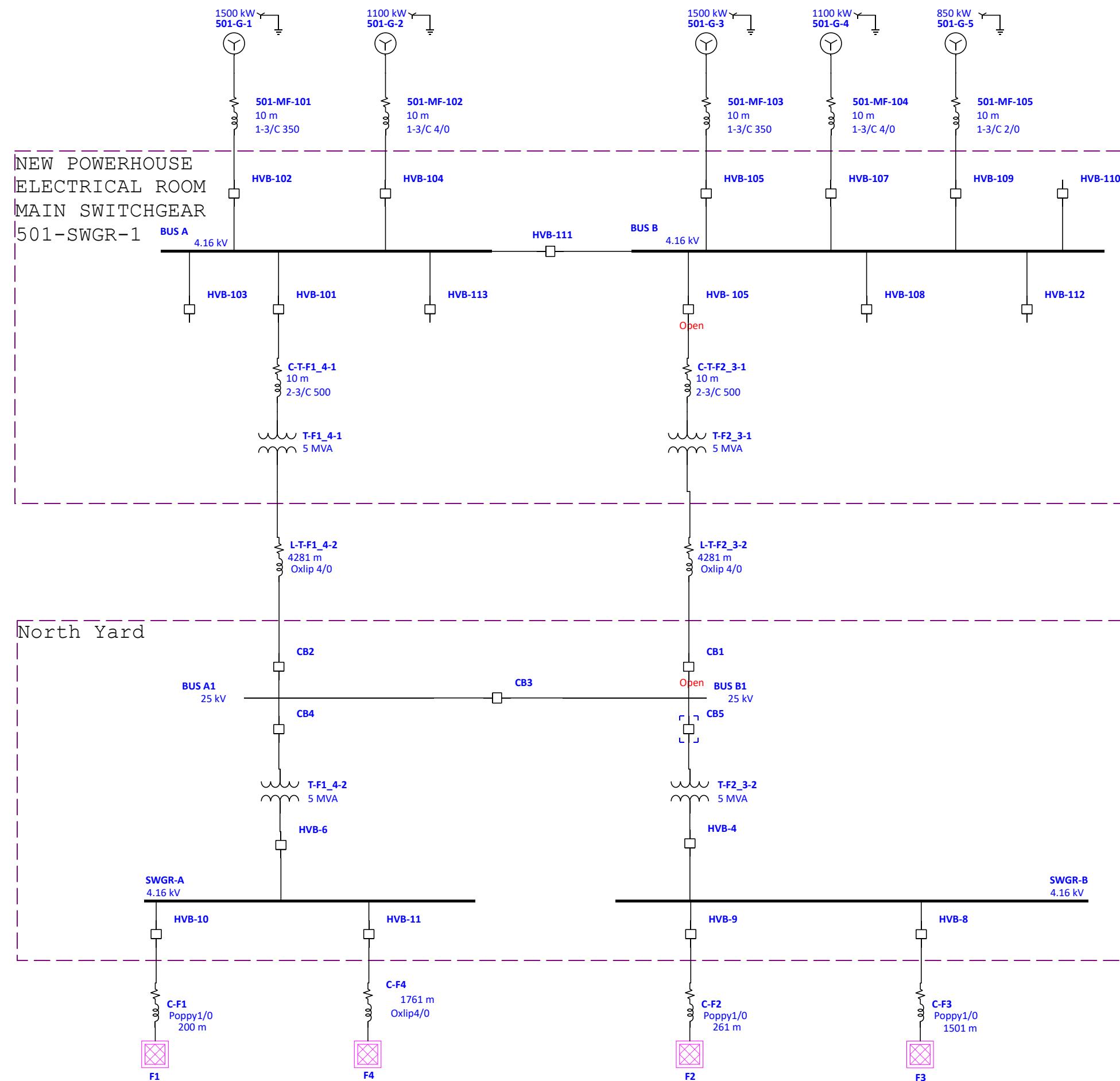
Option 3B: Scenario A: All Feeders are Fed from One Step-up Transformer

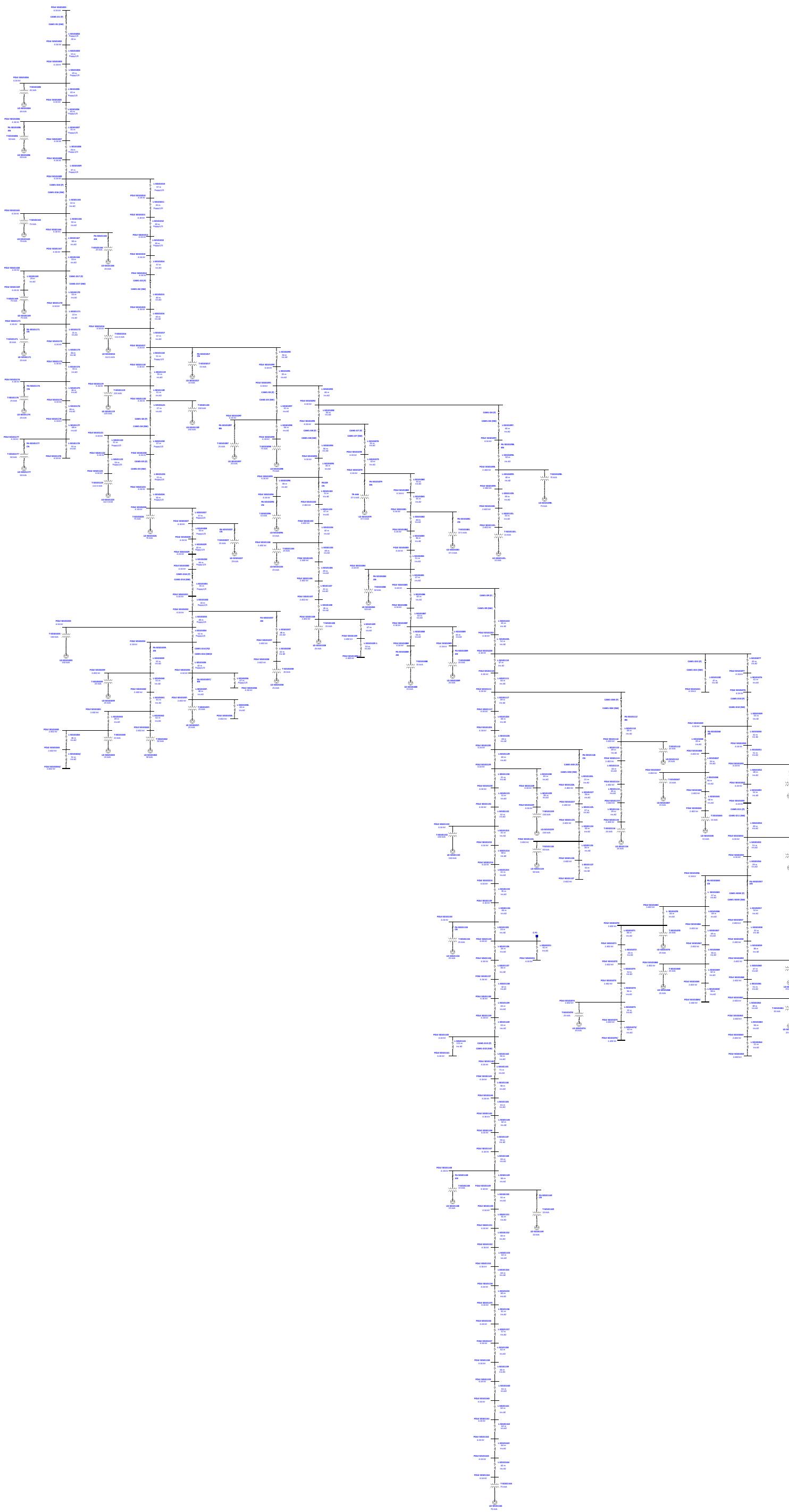
Option 3B: Scenario B: Feeder 1 is Fed from T-F1 4-2 Step-up Transformer and Feeders 3 and 4 are Fed from T-F2 3-2 Step-Up Transformer

Appendix 1.F

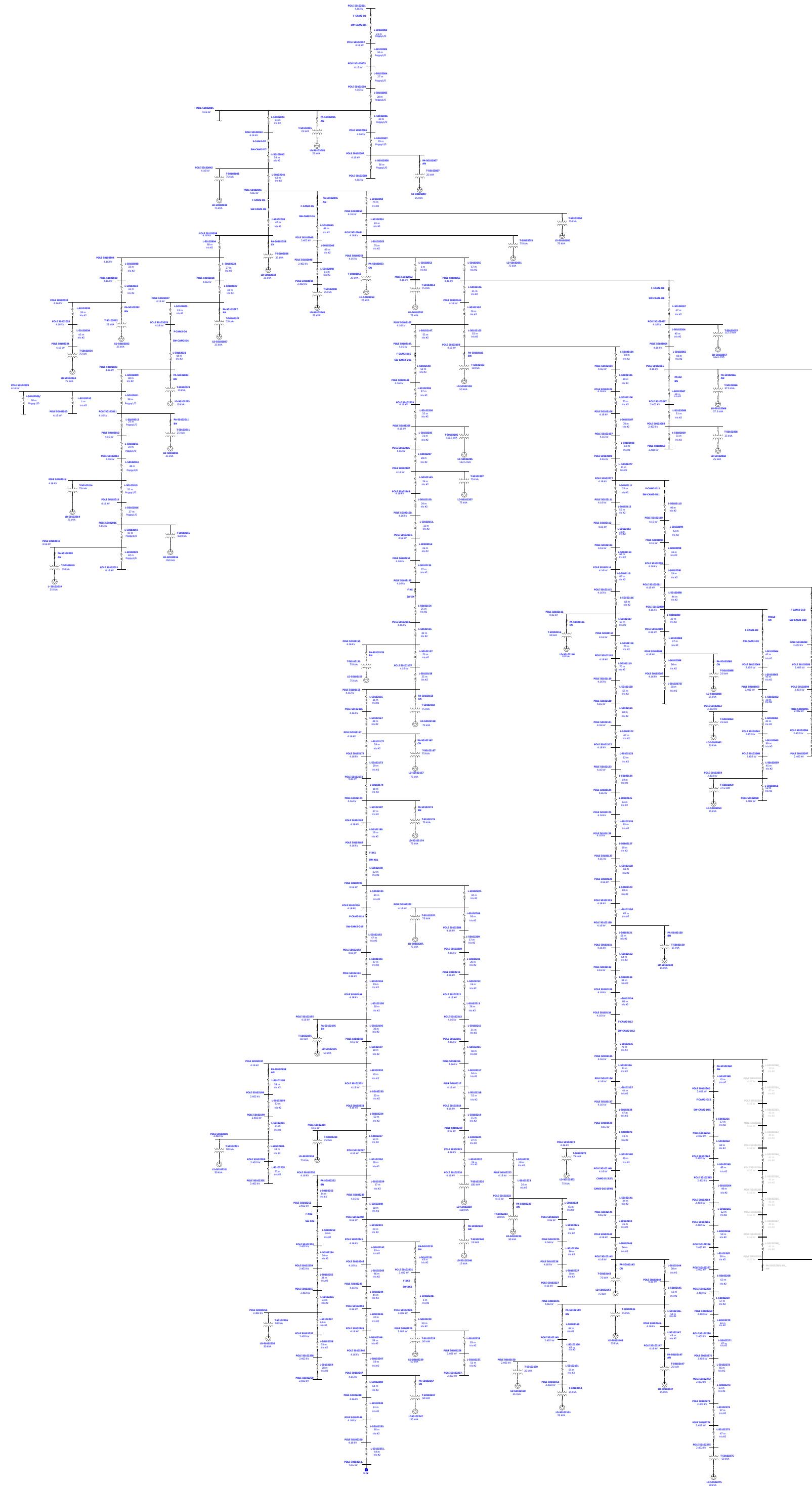
Cambridge Bay Network ETAP Model and Results – Option 4

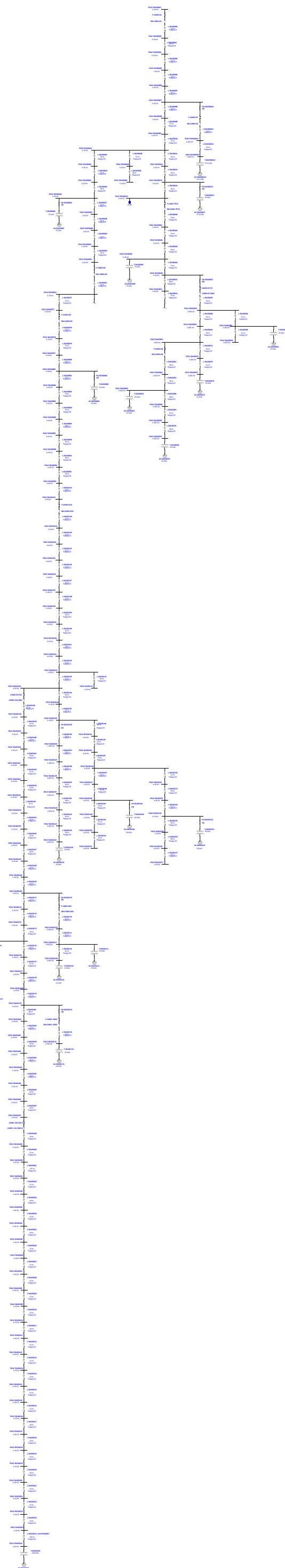
One-Line Diagram - OLV1 (Load Flow Analysis)

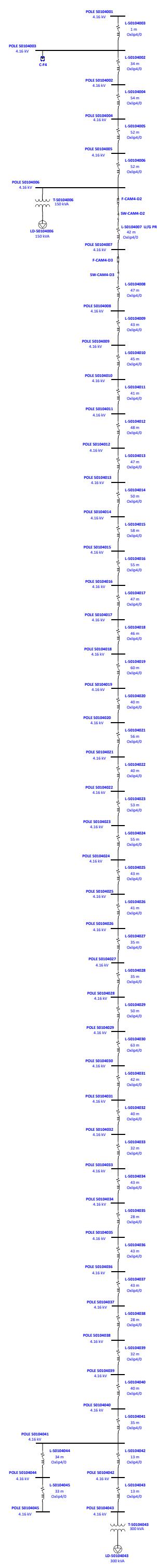




One-Line Diagram - OLV1=>F2 (Load Flow Analysis) - Ahmed.Abdelfattah(Project Editor)







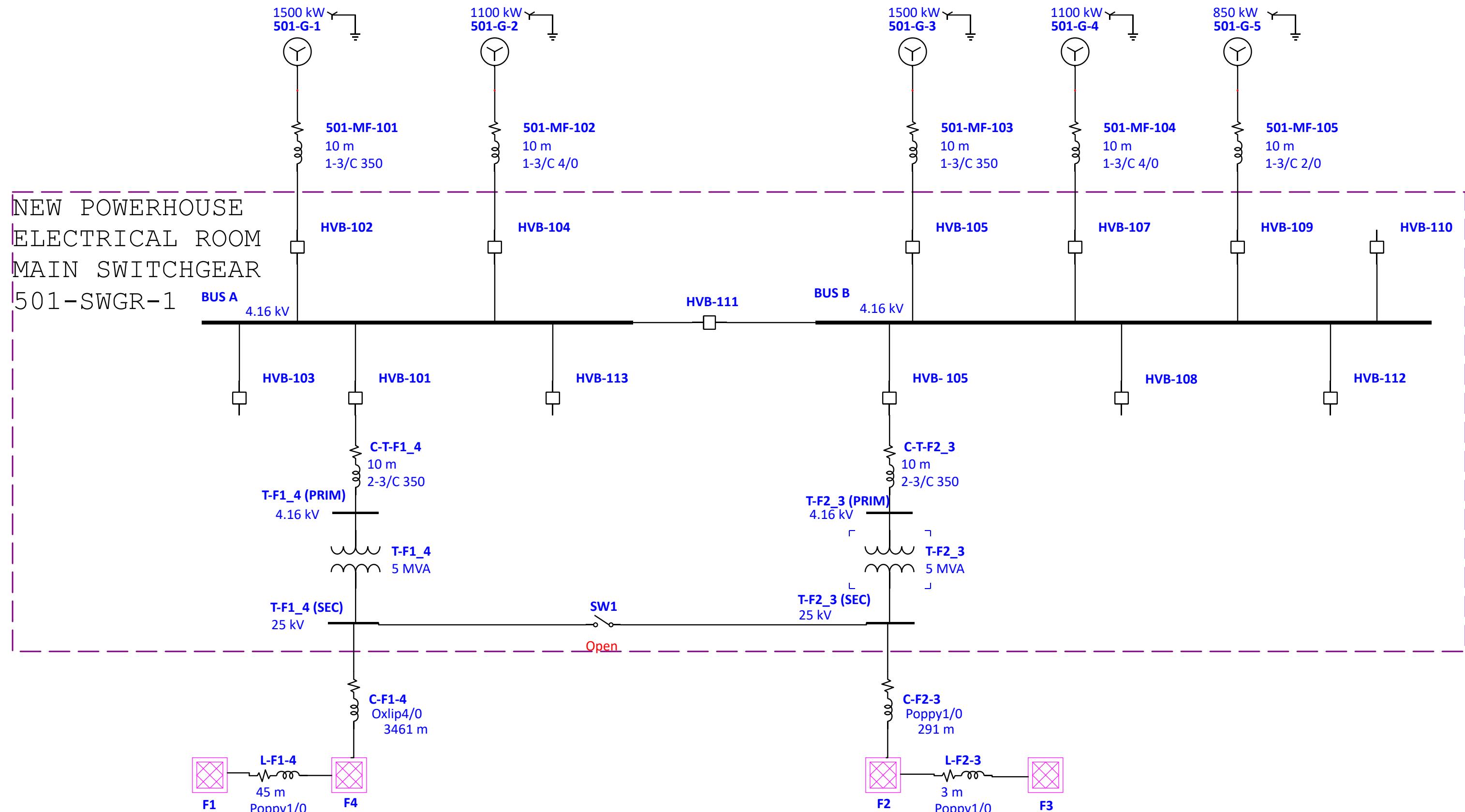
Option 4: Scenario A: All Feeders are Fed from One Step-up Transformer

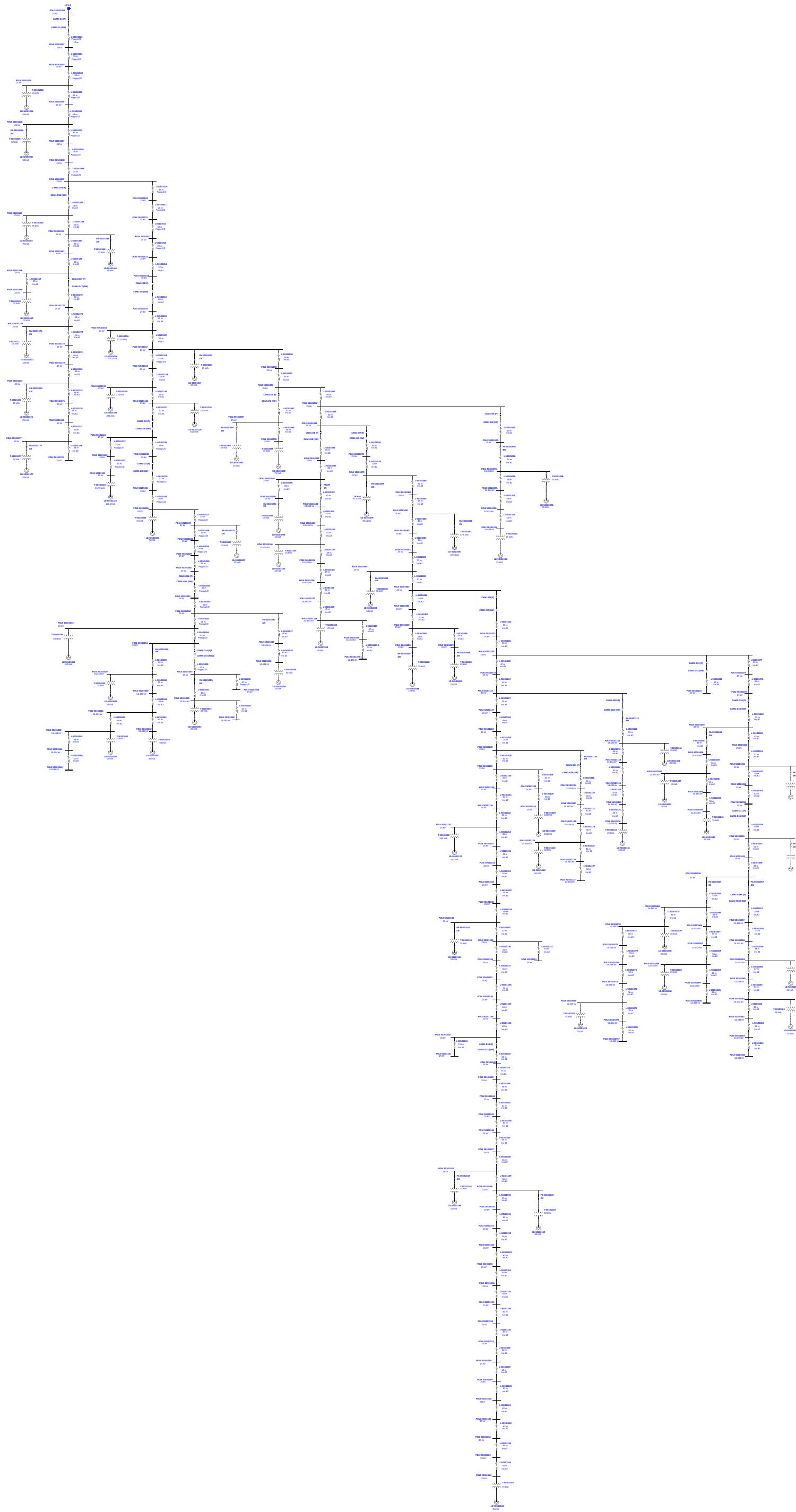
Option 4: Scenario B: Each Two Feeders are Fed from One Step-up Transformer

Appendix 1.G

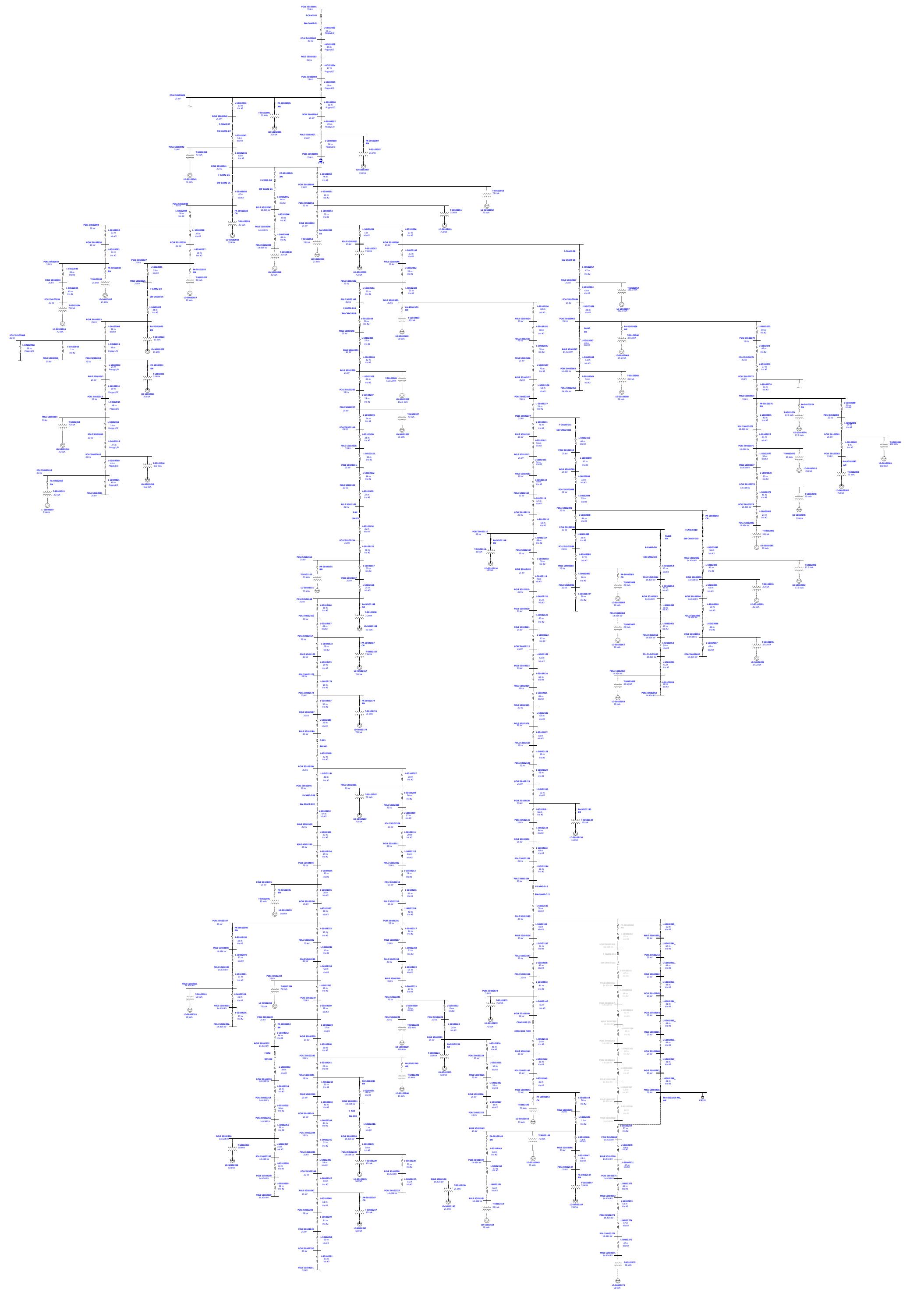
Cambridge Bay Network ETAP Model and Result – Option 5

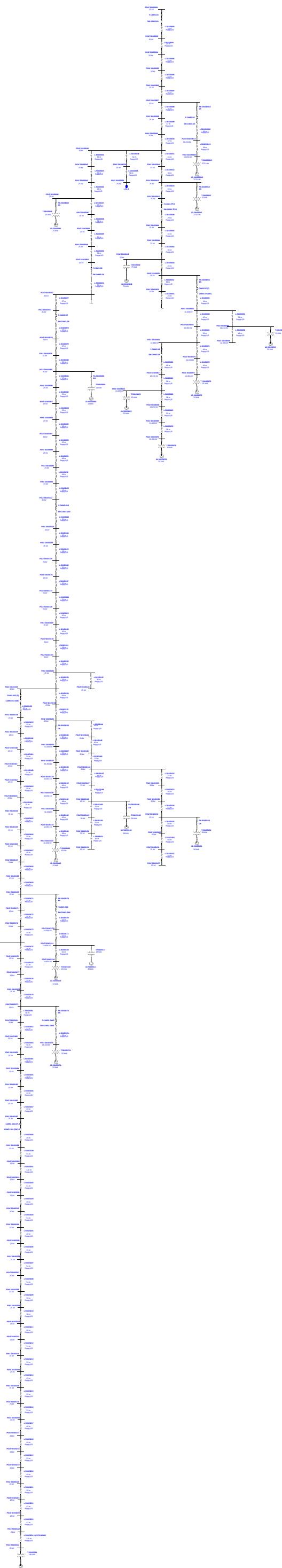
One-Line Diagram - OLV1 (Load Flow Analysis)

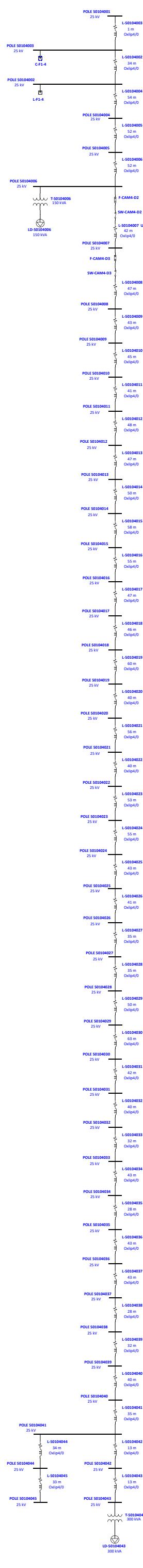




One-Line Diagram - OLV1=>F2 (Load Flow Analysis) - Ahmed.Abdelfattah(Project Editor)







Option 5: Scenario A: All Feeders are Fed from One Step-up Transformer

Option 5: Scenario B: Each Two Feeders are Fed from One Step-up Transformer

Year	F1			F2				F3				F4				
	Status	Min. Main Line Size L-F1-4	Transformer Taps		Status	Min. Main Line Size C-F2-3	Transformer Taps		Status	Min. Main Line Size L-F2-3	Transformer Taps		Status	Min. Main Line Size C-F1-4	Transformer Taps	
			T-F1_4	T-F2_3												
2026	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2027	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2028	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2029	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2030	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2031	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2032	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2033	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2034	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2035	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2036	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2041	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2046	Passed	1/0 AWG	0.00%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	0.00%	N/A
2051	Passed	1/0 AWG	-2.50%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	-2.50%	N/A
2056	Passed	1/0 AWG	-2.50%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	-2.50%	N/A
2061	Passed	1/0 AWG	-2.50%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	-2.50%	N/A
2066	Passed	1/0 AWG	-2.50%	N/A	Passed	1/0 AWG	N/A	0.00%	Passed	1/0 AWG	N/A	0.00%	Passed	4/0 AWG	-2.50%	N/A

Appendix 2

Cambridge Bay – Estimated Electricity Production



Cambridge Bay Community Diesel Power Plant

Technical Report

Greenhouse Gas Mitigation Assessment



Appendix C: Calculated power plant electricity generation after 2026



Estimated yearly electricity production for the new Cambridge Bay power plant

Year	Population	Population change	Estimated electricity produced (kWh/year)
2026	2,451	+55	15,407,427
2027	2,507	+57	15,763,605
2028	2,565	+58	16,128,017
2029	2,625	+59	16,500,853
2030	2,685	+61	16,882,308
2031	2,747	+62	17,272,581
2032	2,811	+64	17,671,877
2033	2,876	+65	18,080,403
2034	2,942	+66	18,498,373
2035	3,010	+68	18,926,005
2036	3,080	+70	19,363,523
2037	3,151	+71	19,811,155
2038	3,224	+73	20,269,136
2039	3,298	+75	20,737,703
2040	3,375	+76	21,217,103
2041	3,453	+78	21,707,585
2042	3,532	+80	22,209,405
2043	3,614	+82	22,722,827
2044	3,698	+84	23,248,117
2045	3,783	+85	23,785,550
2046	3,871	+87	24,335,408
2047	3,960	+89	24,897,977
2048	4,052	+92	25,473,551
2049	4,145	+94	26,062,430
2050	4,241	+96	26,664,923
2051	4,339	+98	27,281,344
2052	4,439	+100	27,912,015
2053	4,542	+103	28,557,265
2054	4,647	+105	29,217,432
2055	4,755	+107	29,892,860
2056	4,864	+110	30,583,902
2057	4,977	+112	31,290,919
2058	5,092	+115	32,014,280
2059	5,210	+118	32,754,364
2060	5,330	+120	33,511,556
2061	5,453	+123	34,286,252
2062	5,579	+126	35,078,858
2063	5,708	+129	35,889,786
2064	5,840	+132	36,719,461
2065	5,975	+135	37,568,315
2066	6,113	+138	38,436,793



Engineering Study Final Report

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The results presented in the report are at a conceptual level; no detailed engineering has yet been performed, nor has equipment been selected or an operational plan been defined.

Use of this Document acknowledges acceptance of the foregoing conditions.

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Appendices

Appendix 1	Cambridge Bay Network ETAP Model and Results
Appendix 2	Cambridge Bay – Estimated Electricity Production

Executive Summary

QEC is building a new power plant on the south-west side of Cambridge Bay to provide sufficient energy to this community. Due to the remote location of the new power plant, different approaches for connecting the existing community feeders to the new power plant were studied.

After studying the different options for the possibility of feeding the existing community feeders from the new power plant, as explained in Cambridge Bay Power Plant Feeder Distribution Line Study 2401E001ST Rev. C, QEC advised to investigate the feasibility to implement the following option (Referenced as Option 4 in the report):

- A new power plant will be constructed in the south-west part of Cambridge Bay community. The new power plant will comprise Five (5) 4.16kV generators, 4.16kV switchgear and Two (2) 4.16/25kV, 5MVA, step-up transformers.
- A new substation will be constructed at the North Yard on the north side of Cambridge Bay community. The new substation will comprise One (1) 25kV switchgear, Two (2) 25/4.16kV, 5MVA, step-down transformers, and Two (2) 4.16kV switchgears.
- The new substation will be connected to the new power plant via Two (2) 25kV transmission lines.

The above option is discussed in detail in Section 1.3. The single-line diagrams showing the network topology are included in Appendix 1.

The previous study showed that this option does not accommodate the load forecast up to the year 2066, and that the off-line tap changers of both step up and step down transformers need to be adjusted to mitigate the voltage drop due to future load increase. Therefore, an alternative approach for voltage drop mitigation was studied as part of the scope of this report. The alternative approach involves the use of Automatic Voltage Regulators (AVRs) that are strategically placed in order to maintain the voltage drop within the $\pm 3\%$ voltage limits while keeping the network losses at a minimum.

The study considers the estimated electricity production for the years from 2026 to 2066 as shown in Appendix 2.

The study recommends the use of AVRs in the following locations:

- Two (2), 4.16kV, 5MVA, AVRs, one on the primary side of each step-up transformer in the new power plant.
- Feeder 1: Two (2), 4.16kV, 2.5MVA, AVRs on the supply side of Poles 50101135 and 50101225.
- Feeder 2: One (1), 4.16kV, 3.5MVA, AVR on the supply side of Pole 50102135.
- Feeder 3: One (1), 4.16kV, 1MVA, AVR on the supply side of Pole 50103013.
- Feeder 4: One (1), 4.16kV, 0.8MVA, AVR on the supply side of Pole 50104003.

The current study considers that Feeder 2 is connected to the new power plant at Pole 50102260 which is the closest pole with three-phase lines. An alternative option is to connect Feeder 2 to the new power plant at Pole 50102268 which is closer to the power plant and replace the single-phase transmission lines between Poles 50102268 and 50102260 with three-phase. Although this option involves additional transmission lines to be installed, it will eliminate the need for an AVR for Feeder 2.

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Table 3 summarizes the study results.

Table 3: Study Results Summary

		Operating Scenario		Remarks
		A	B	
Main Power Plant	Min. Main Feeder Line Size	4/0 AWG	1/0 AWG	
	AVR Tap Setting	AVR-T-F1_4-1	-5%	-2.5%
		AVR-T-F2_3-1	-5%	-2.5%
Feeder 1	Min. Main Feeder Line Size	2/0 AWG	1/0 AWG	
	AVR Tap Setting	AVR-50101135	-6.25%	-5.625%
		AVR-50101225	-3.75%	-3.75%
Feeder 2	Min. Main Feeder Line Size	1/0 AWG	1/0 AWG	
	AVR Tap Setting AVR-50102135		-3.75%	-3.75%
Feeder 3	Min. Main Feeder Line Size	3/0 AWG	1/0 AWG	
	AVR Tap Setting AVR-50103013		-7.5%	-7.5%
Feeder 4	Min. Main Feeder Line Size	4/0 AWG	4/0 AWG	
	AVR Tap Setting AVR-50104003		-4.375%	-3.75%

Scenario A: Feeders 1, 3, and 4 are fed from one North Yard Switchgear incomer.

Scenario B: Feeders 1, 3, and 4 are fed from both North Yard Switchgear incomers.

1. Introduction

1.1 Background

QEC is building a new power plant on the south-west side of Cambridge Bay to provide sufficient energy to this community. Due to the remote location of the new power plant, different approaches for connecting the existing community feeders to the new power plant were studied. The previous study, Cambridge Bay Power Plant Feeder Distribution Line Study 2401E001ST, considered five (5) options and reviewed the associated load behaviour over the network including the voltage drop and active power losses.

QEC preferred Option 4 of the original study.

Option 4

Run two (2) x 25kV feeder circuit lines from the new power plant (with two (2) x 5MVA step-up transformers) to the North Yard location (with two (2) x 5MVA step-down transformers and 5kV switchgear).

- Install two (2) new 4.16/25kV, 5MVA, step-up transformers in the new power plant and connect the primary side of these transformers to the new main 5kV switchgear via cables.
- Install two (2) new 25/4.16kV, 5MVA, step-down transformers and Main-Tie-Main, 5kV, switchgear at the North Yard and connect the primary side of these transformers to the outgoing breaker of the new switchgear.
- Connect the incoming breakers of the new switchgear to the secondary side of the new step-up transformers via new transmission lines.
- Connect the existing community feeders to the 5kV switchgear at the North Yard via transmission lines. The tie-in location of each feeder is as below:
 - For Feeder 1: Pole 50101135
 - For Feeder 2: Pole 50102251
 - For Feeder 3: Pole 50103013
 - For Feeder 4: Pole 50104003

For this option, two operating scenarios are considered:

- All community feeders are fed from one step-up transformer. This is considered the worst-case operating scenario.
- Each two of the community feeders are fed from one step-up transformer. The distribution of the community feeders on each transformer was decided based on the peak demand load of the four feeders such that both transformers are equally loaded.

However further review of this option was required in order to satisfy the original criteria of the study which were:

- Minimize the voltage drop across the lines. The voltage drop should not exceed 3% from the generators to each individual consumer.

- Minimize the network active power losses.

1.2 Scope of Work

The previous study showed that Option 4 as originally assessed does not accommodate the load forecast up to the year 2066, and that the off-line tap changers of both step up and step down transformers need to be adjusted to mitigate the voltage drop due to future load increase. Therefore, an alternative approach for voltage drop mitigation was included as part of the scope. The alternative approach involves the use of Automatic Voltage Regulators (AVRs) that are strategically placed at different parts of the network in order to maintain the voltage drop within the $\pm 3\%$ voltage limits while keeping the network losses at a minimum. In addition, alternatives for tie-in of Feeder 2 were considered.

The estimated electricity production for the years from 2026 to 2066 used in the study is included in Appendix 2.

1.3 Tie-In Option

The Option 4 approach for tie-in of the community feeders is detailed below with modifications from the original approach in bold.

- Construct a new power plant at the south-west part of Cambridge Bay community. The new power plant will comprise Five (5) 4.16kV generators, **4.16kV switchgear** and Two (2) 4.16/25kV, 5MVA, step-up transformers.
- Construct a new substation at the North Yard on the north side of Cambridge Bay community. The new substation will comprise **One (1) 25kV switchgear**, Two (2) 25/4.16kV, 5MVA, step-down transformers, and **Two (2) 4.16kV switchgears**.
- Run two (2) x 25kV feeder circuit lines from the new power plant each line will connect the 25kV secondary side of the step-up transformer in the new power plant to the 25kV switchgear in the new substation.
- Connect the primary side of the step-up transformers to the 4.16kV switchgear in the new power plant via cables.
- Connect the 25kV switchgear in the new substation to the primary side of the step-down transformers via cables.
- Connect the secondary side of the step-down transformers in the new substation to the **4.16kV switchgear** via cables.
- Connect the existing community feeders to the new power plant and the new substation as below:
 - Feeder 1: Will be connected to the 4.16kV switchgear in the new substation at Pole 50101135.
 - **Feeder 2: Will be connected to the 4.16kV switchgear in the new power plant at Pole 50102135.**
 - Feeder 3: Will be connected to the 4.16kV switchgear in the new substation at Pole 50103013.
 - Feeder 4: Will be connected to the 4.16kV switchgear in the new substation at Pole 50104003.

Two operating scenarios are considered:

- **Community Feeders 1, 3, and 4 are fed from one step-up transformer. This is considered the worst-case operating scenario.**
- Community Feeders 1 and 4 are fed from one step-up transformer while community Feeder 3 is fed from the other step-up transformer. The distribution of the community feeders on each transformer was decided based on the peak demand load of the three feeders such that both transformers are equally loaded.

The single-line diagram showing the network topology is included under Appendix 1.

2. Discussion

As with the previous study, the solution discussed in this study uses the following criteria in order to provide recommended optimum locations of AVRs and select a tie-in location for Feeder 2:

- Minimize the voltage drop across the lines. The voltage drop should not exceed 3% from the generators to each individual consumer.
- Minimize the network active power losses.

2.1 Sources of Data

Network model and simulation parameters are set based on the following inputs:

- **ETAP Model:**

The ETAP model used is based on the model developed for QEC Penetration Study. The model of the power plant is updated to reflect the topology of the new plant.

- **One-line Diagrams:**

The Network model is built using the provided one-line diagrams. These diagrams are also used to obtain the connected load and phase connection of each customer.

- **Generation Forecast:**

QEC provided a table showing the estimated electricity produced over the years from 2026 to 2066 (See Appendix 2). These estimates are used for feeder sizing, voltage drop, and network losses calculations.

2.2 Assumptions

- The maximum demand factors of each feeder load in 2019 are calculated based on the load data reading provided by QEC. The estimated electricity production for subsequent years (Appendix 2) is used to calculate the maximum demand factor for these years.
- Normally open switches, interconnecting different feeders and used during the failure or maintenance of any of the feeder breakers, are not included in the model and the penetration study except for the options where each two feeders are combined.

- Since the specified AASC cables are not available in the standard ETAP library, AAC cables are used instead. The electrical and geometric characteristics of the selected cable are modified to match the AASC cable specifications provided by QEC.
- The boundary conditions for the voltage limits at all networks nodes (buses) are assumed to be $\pm 3\%$.
- The maximum transmission line size to be used is 4/0 AWG with a single conductor per phase.
- QEC advised that most of the loads are non-inductive and that the overall power factor for each feeder is in the order of 0.99. For the purpose of this study, all loads are assumed to have a 0.95 power factor for more conservative values of load currents.
- Based on overhead line conductor parameters provided by QEC, resistance, reactance, and susceptance values for overhead lines are calculated using ETAP considering the following conductor configuration on the pole structure:
 - Conductor height: 34 ft (unless otherwise indicated on the single-line diagrams).
 - Spacing between phases: 2 ft.
- Generator plant service loads are not considered in the analysis.
- Proposed AVR's have voltage adjustment limits of $\pm 10\%$ with steps of 0.625%. AVR impedances are included in the study based on their assumed values as provided by ETAP software.

2.3 Network Configuration

The new power plant for Cambridge Bay consists of two (2) 1500kW, two (2) 1100kW and one (1) 850kW generators with an output voltage of 4.16kV. Generator outputs are connected to a main 4.16kV switchgear with two (2) bus sections connected together via tie breaker such that one (1) 1500kW and one (1) 1100kW generators are connected to one bus section, and one (1) 1500kW, one (1) 1100kW, and one (1) 850kW generators are connected to the other bus section.

With the exception of Feeder #2, in order to improve customer power supply reliability, feeders are interconnected via a set of normally open switches. Any of these switches may be closed in the case when one of the feeder breakers is out of duty due to failure or for maintenance purposes. Since the case where both feeders are connected to one feeder breaker does not represent normal network operation and is used only for maintenance purposes, these configurations are not included in the model except where two feeders are combined into one feeder. For this case, only the tie switch is considered closed.

The network ETAP model is provided in Appendix 1.

2.4 Calculation Procedures

2.4.1 Load Parameters Calculations

The peak demand load for the year 2019 is obtained from the metering readings provided by QEC for this year and is used to calculate the maximum demand factor for the loads of each feeder as shown in Table 1.

Table 1: Maximum Demand (2019)

	Connected Load (kVA)	Max. Demand Load (kVA)	Max. Demand Factor (%)
Feeder 1	2537.5	989.625	39.00%
Feeder 2	3017.5	754.375	25.00%
Feeder 3	642.5	334.1	52.00%
Feeder 4	450	234	52.00%
Total	6647.5	2312.1	

The estimated electricity production (Appendix 2) is used to calculate the percentage growth of electricity demand which is, in turn, used to calculate the maximum demand for the successive years as shown in Table 2.

Table 2: Estimated Growth in Demand Load

Year	Population Demand Load Change (%)	Maximum Demand Factors			
		Feeder 1	Feeder 2	Feeder 3	Feeder 4
2019	-	39.00%	25.00%	52.00%	52.00%
2026	55.00%	60.45%	38.75%	80.60%	80.60%
2027	57.00%	61.23%	39.25%	81.64%	81.64%
2028	58.00%	61.62%	39.50%	82.16%	82.16%
2029	59.00%	62.01%	39.75%	82.68%	82.68%
2030	61.00%	62.79%	40.25%	83.72%	83.72%
2031	62.00%	63.18%	40.50%	84.24%	84.24%
2032	64.00%	63.96%	41.00%	85.28%	85.28%
2033	65.00%	64.35%	41.25%	85.80%	85.80%
2034	66.00%	64.74%	41.50%	86.32%	86.32%
2035	68.00%	65.52%	42.00%	87.36%	87.36%
2036	70.00%	66.30%	42.50%	88.40%	88.40%
2041	78.00%	69.42%	44.50%	92.56%	92.56%
2046	87.00%	72.93%	46.75%	97.24%	97.24%
2051	98.00%	77.22%	49.50%	102.96%	102.96%
2056	110.00%	81.90%	52.50%	109.20%	109.20%
2061	123.00%	86.97%	55.75%	115.96%	115.96%
2066	138.00%	92.82%	59.50%	123.76%	123.76%

As agreed with QEC, the study considers the load demand of the first 10 years (2026 to 2036) in one-year steps, and the following 30 years (2037 to 2066) in 5-year steps.

The above demand factors are used in the ETAP model.

The maximum demand load analysis of the four feeders based on the table above shows that:

- The maximum generation capacity for each bus section of the switchgear is 2500 kW. The peak demand load forecast for all the years exceeds 2500kW. Therefore, the switchgear bus-tie breaker needs to be closed such that the total load can be distributed among all the generators.
- Customer transformers connected to Feeders 3 and 4 need to be upgraded to 125% of their current ratings to accommodate the forecasted demand.

2.4.2 Design Constraints

The following design constraint are established by QEC:

- The total voltage drop from the generators to each customer load shall not exceed 3%.
- The maximum size of a transmission line is 4/0AWG with no more than one conductor per phase.
- Initial calculations are made with all transformer taps set at the zero-position. Voltage drop compensation is achieved using AVRs.

2.5 Results

Electricity production estimate for the years from 2026 to 2066 is used to calculate the demand load and demand factor for each feeder. These demand factors were applied to calculate the minimum feeder size that is required to achieve maximum voltage drop of 3% at the customer transformer using the tie-in option detailed under Section 1.3.

An iterative method is used to find the optimum connection locations for the AVR. The objective constraints used in this method is to:

- 1) Maintain the voltages at different poles within the $\pm 3\%$ voltage drop limits.
- 2) Minimize the active power losses in the network.
- 3) Minimize the number of AVRs to be used.

The results of this iterative method show that the AVR are best located near the heaviest loaded lines.

The study concludes that the tie-in configuration discussed in this study will provide the required energy to the community feeders up to the forecasted load for the year 2066 when using AVRs strategically located at different points of the network to compensate for potential voltage drops and to minimize network losses.

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Table 3: Study Results Summary

			Operating Scenario		Remarks
			A	B	
Main Power Plant	Min. Main Feeder Line Size		4/0 AWG	1/0 AWG	
	AVR Tap Setting	AVR-T-F1_4-1	-5%	-2.5%	
		AVR-T-F2_3-1	-5%	-2.5%	
Feeder 1	Min. Main Feeder Line Size		2/0 AWG	1/0 AWG	
	AVR Tap Setting	AVR-50101135	-6.25%	-5.625%	
		AVR-50101225	-3.75%	-3.75%	
Feeder 2	Min. Main Feeder Line Size		1/0 AWG	1/0 AWG	
	AVR Tap Setting AVR-50102135		-3.75%	-3.75%	
Feeder 3	Min. Main Feeder Line Size		3/0 AWG	1/0 AWG	
	AVR Tap Setting AVR-50103013		-7.5%	-7.5%	
Feeder 4	Min. Main Feeder Line Size		4/0 AWG	4/0 AWG	
	AVR Tap Setting AVR-50104003		-4.375%	-3.75%	

Scenario A: Feeders 1, 3, and 4 are fed from one North Yard Switchgear incomer.

Scenario B: Feeders 1, 3, and 4 are fed from both North Yard Switchgear incomers.

Table 4: Study Results Details

Year	Operating Scenario	Main Power Plant			Feeder 1			Feeder 2			Feeder 3			Feeder 4		
		Min. Main Feeder Line Size	AVR Tap Setting		Min. Main Feeder Line Size	AVR Tap Setting		Min. Main Feeder Line Size	AVR Tap Setting		Min. Main Feeder Line Size	AVR Tap Setting		Min. Main Feeder Line Size	AVR Tap Setting	
			AVR-T-F1_4-1	AVR-T-F2_3-1		AVR-50101135	AVR-50101225		AVR-50102135	AVR-50103013		AVR-50104003	AVR-50104003		AVR-50104003	AVR-50104003
2026	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.25%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.25%			
2027	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.25%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.25%			
2028	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.25%			
2029	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.25%			
2030	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.25%			
2031	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-5%	4/0 AWG	-1.875%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.125%	4/0 AWG	-1.875%			
2032	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-5%	4/0 AWG	-1.875%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.75%	4/0 AWG	-1.875%			
2033	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-1.875%	1/0 AWG	-1.875%	1/0 AWG	-5%	4/0 AWG	-2.5%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.75%	4/0 AWG	-1.875%			
2034	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-5%	4/0 AWG	-2.5%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.75%	4/0 AWG	-1.875%			
2035	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-5%	4/0 AWG	-2.5%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.75%	4/0 AWG	-1.875%			
2036	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-3.75%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-5.625%	4/0 AWG	-2.5%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-3.75%	4/0 AWG	-1.875%			
2041	A	1/0 AWG	-3.75%	-3.75%	1/0 AWG	-4.375%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-6.25%	4/0 AWG	-3.125%			
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-2.5%	1/0 AWG	-1.875%	1/0 AWG	-4.375%	4/0 AWG	-1.875%			

Year	Operating Scenario	Main Power Plant			Feeder 1			Feeder 2		Feeder 3		Feeder 4	
		Min. Main Feeder Line Size	AVR Tap Setting		Min. Main Feeder Line Size	AVR Tap Setting		Min. Main Feeder Line Size	AVR Tap Setting	Min. Main Feeder Line Size	AVR Tap Setting	Min. Main Feeder Line Size	AVR Tap Setting
			AVR-T-F1_4-1	AVR-T-F2_3-1		AVR-50101135	AVR-50101225		AVR-50102135		AVR-50103013		AVR-50104003
2046	A	1/0 AWG	-4.375%	-4.375%	1/0 AWG	-4.375%	-2.5%	1/0 AWG	-2.5%	1/0 AWG	-6.25%	4/0 AWG	-3.125%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.125%	-3.125%	1/0 AWG	-2.5%	1/0 AWG	-5%	4/0 AWG	-1.875%
2051	A	1/0 AWG	-4.375%	-4.375%	1/0 AWG	-5%	-3.125%	1/0 AWG	-2.5%	1/0 AWG	-6.875%	4/0 AWG	-3.125%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-3.75%	-3.125%	1/0 AWG	-2.5%	1/0 AWG	-5%	4/0 AWG	-2.5%
2056	A	3/0 AWG	-4.375%	-4.375%	1/0 AWG	-5%	-3.75%	1/0 AWG	-3.125%	1/0 AWG	-7.5%	4/0 AWG	-3.75%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-5%	-3.125%	1/0 AWG	-3.125%	1/0 AWG	-6.25%	4/0 AWG	-3.125%
2061	A	3/0 AWG	-5%	-5%	1/0 AWG	-5%	-3.75%	1/0 AWG	-3.125%	1/0 AWG	-7.5%	4/0 AWG	-3.75%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-5%	-3.125%	1/0 AWG	-3.125%	1/0 AWG	-6.875%	4/0 AWG	-3.125%
2066	A	4/0 AWG	-5%	-5%	2/0 AWG	-6.25%	-3.75%	1/0 AWG	-3.75%	3/0 AWG	-7.5%	4/0 AWG	-4.375%
	B	1/0 AWG	-2.5%	-2.5%	1/0 AWG	-5.625%	-3.75%	1/0 AWG	-3.75%	1/0 AWG	-7.5%	4/0 AWG	-3.75%

Scenario A: Feeders 1, 3, and 4 are fed from one North Yard Switchgear incomer.

Scenario B: Feeders 1, 3, and 4 are fed from both North Yard Switchgear incomers.

3. Conclusion and Recommendations

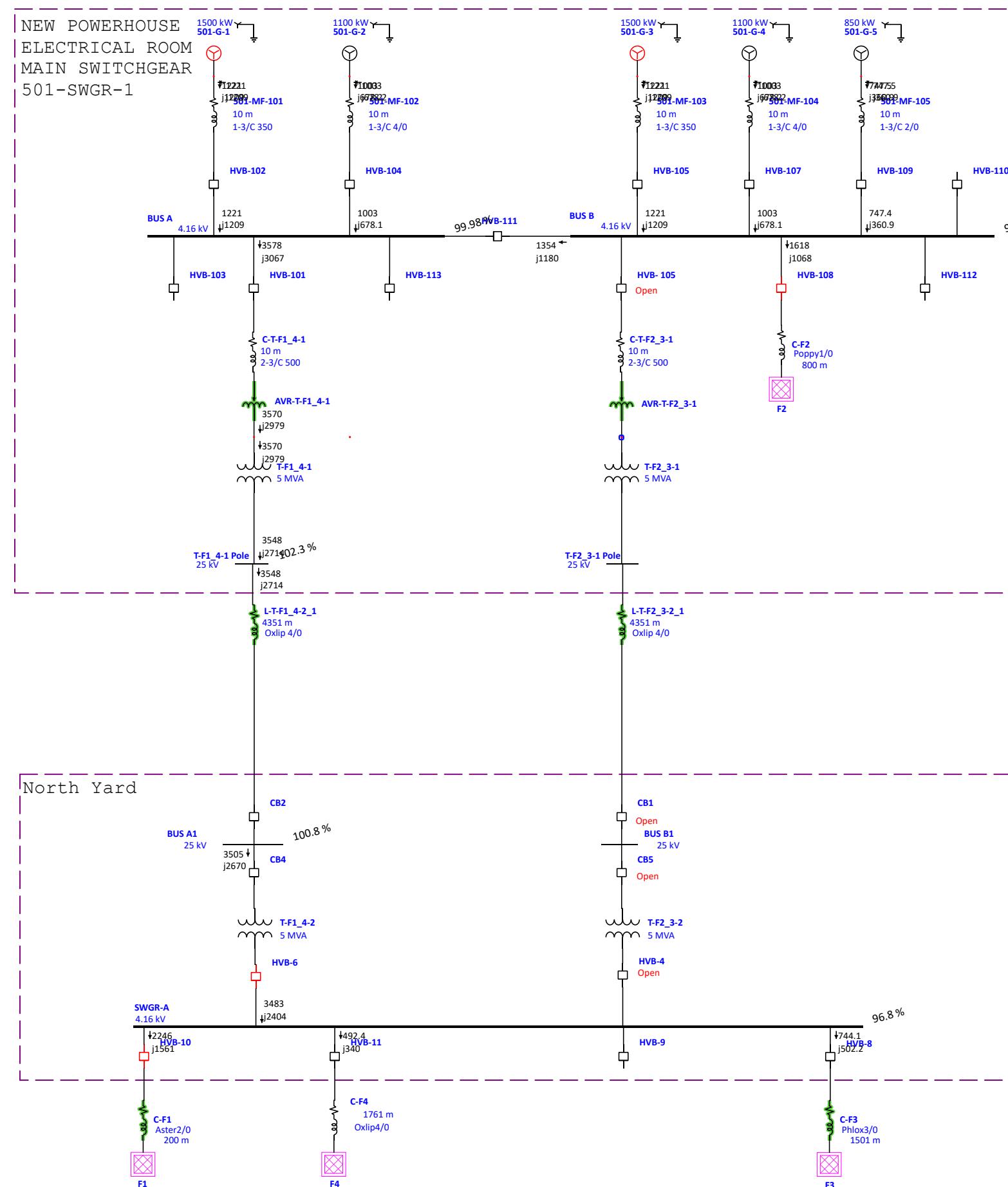
The tie-in configuration discussed in this study will provide the required energy to the community feeders up to the forecasted load for the year 2066 when using AVRs strategically located at different points of the network to compensate for potential voltage drops and to minimize network losses.

The current study considers that Feeder 2 is connected to the new power plant at Pole 50102135 which is the closest pole with three-phase lines. An alternative recommendation would be to connect Feeder 2 to the new power plant at Pole 50102268 which is closer to the power plant and replace the single-phase transmission lines between Poles 50102268 and 50102135 with three-phase. Although this option involves additional transmission lines, it would eliminate the need for an AVR for Feeder 2.

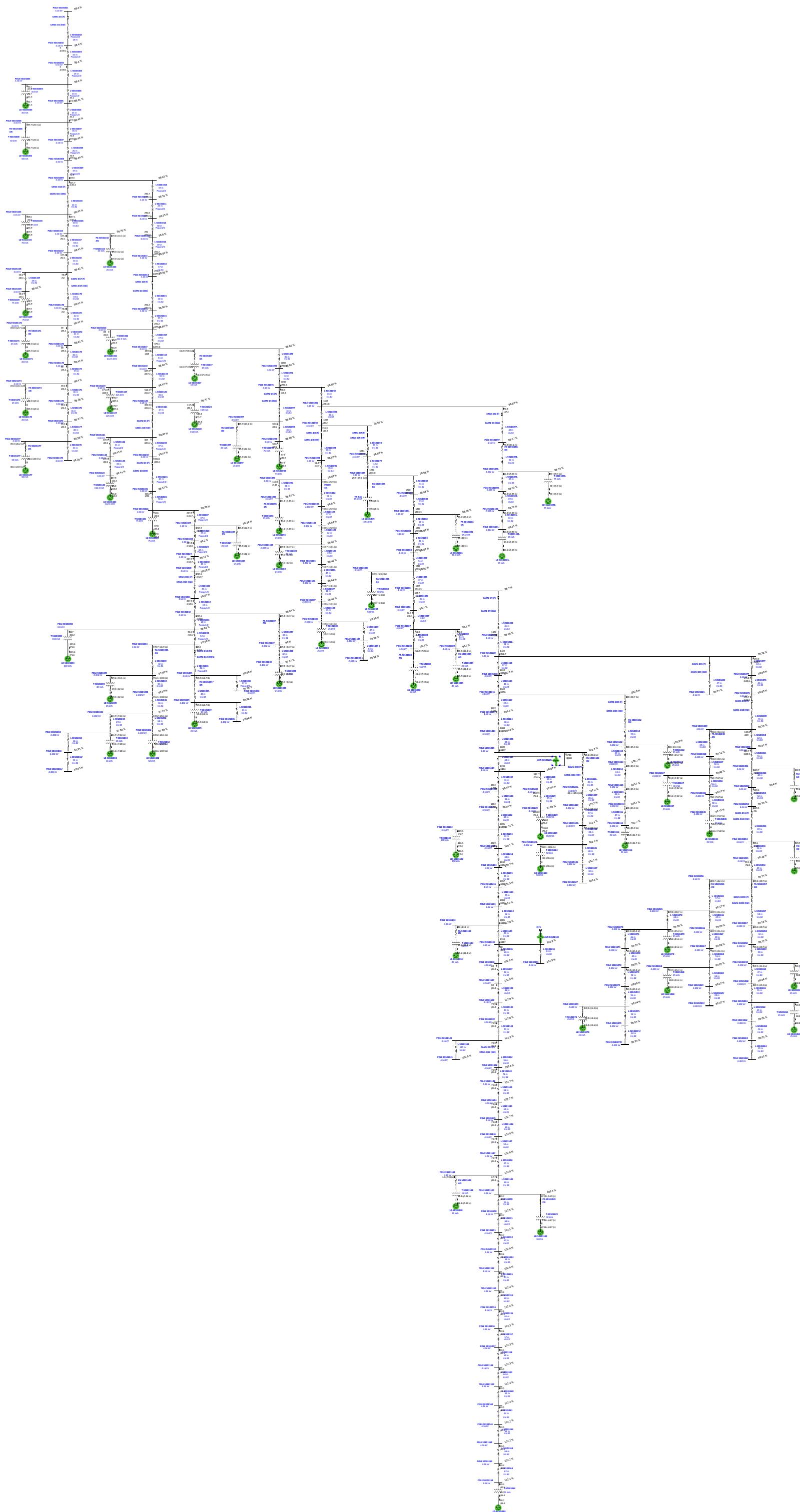
The study can be revisited upon the final selection of the AVRs to verify their connection locations based on their tap setting range and impedances.

Appendix 1
Cambridge Bay Network ETAP Model and Results

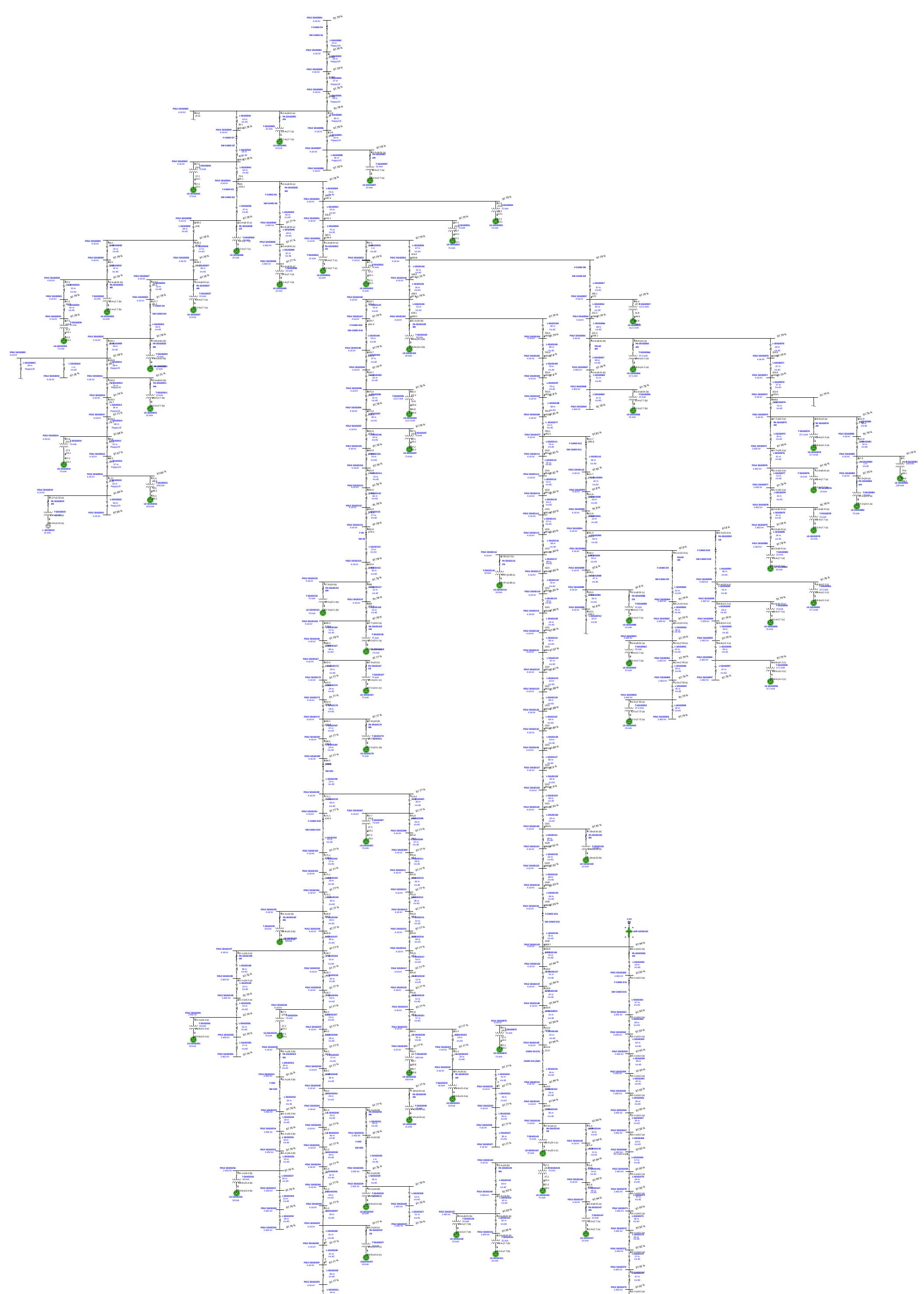
One-Line Diagram - OLV1 | Load Flow Analysis | LF



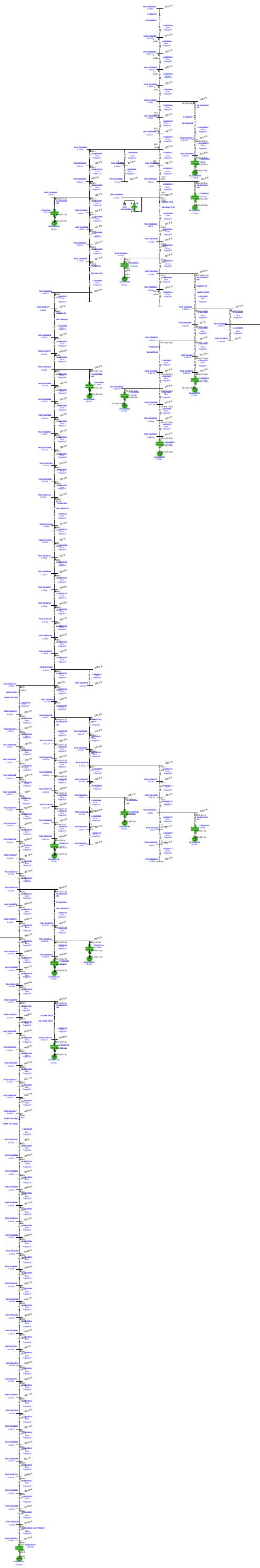
One-Line Diagram - OLV1->F1 | Load Flow Analysis | LF



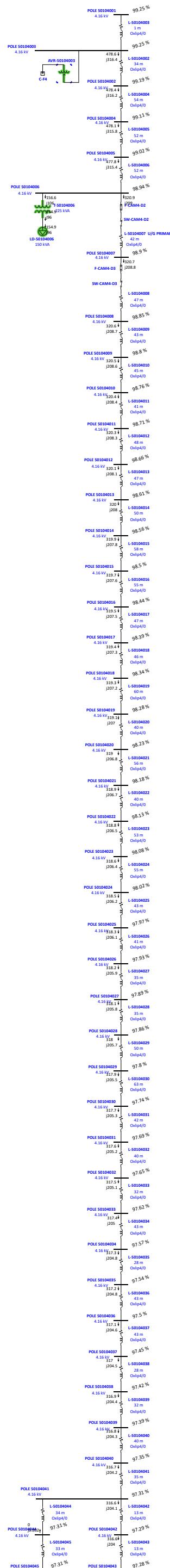
One-Line Diagram - OLV1->F2 | Load Flow Analysis | LF



One-Line Diagram - OLV1->F3 | Load Flow Analysis | LF



One-Line Diagram - OLV1->F4 | Load Flow Analysis | LF



Appendix 2
Cambridge Bay – Estimated Electricity Production



Cambridge Bay Community Diesel Power Plant

Technical Report

Greenhouse Gas Mitigation Assessment



Appendix C: Calculated power plant electricity generation after 2026



Estimated yearly electricity production for the new Cambridge Bay power plant

Year	Population	Population change	Estimated electricity produced (kWh/year)
2026	2,451	+55	15,407,427
2027	2,507	+57	15,763,605
2028	2,565	+58	16,128,017
2029	2,625	+59	16,500,853
2030	2,685	+61	16,882,308
2031	2,747	+62	17,272,581
2032	2,811	+64	17,671,877
2033	2,876	+65	18,080,403
2034	2,942	+66	18,498,373
2035	3,010	+68	18,926,005
2036	3,080	+70	19,363,523
2037	3,151	+71	19,811,155
2038	3,224	+73	20,269,136
2039	3,298	+75	20,737,703
2040	3,375	+76	21,217,103
2041	3,453	+78	21,707,585
2042	3,532	+80	22,209,405
2043	3,614	+82	22,722,827
2044	3,698	+84	23,248,117
2045	3,783	+85	23,785,550
2046	3,871	+87	24,335,408
2047	3,960	+89	24,897,977
2048	4,052	+92	25,473,551
2049	4,145	+94	26,062,430
2050	4,241	+96	26,664,923
2051	4,339	+98	27,281,344
2052	4,439	+100	27,912,015
2053	4,542	+103	28,557,265
2054	4,647	+105	29,217,432
2055	4,755	+107	29,892,860
2056	4,864	+110	30,583,902
2057	4,977	+112	31,290,919
2058	5,092	+115	32,014,280
2059	5,210	+118	32,754,364
2060	5,330	+120	33,511,556
2061	5,453	+123	34,286,252
2062	5,579	+126	35,078,858
2063	5,708	+129	35,889,786
2064	5,840	+132	36,719,461
2065	5,975	+135	37,568,315
2066	6,113	+138	38,436,793